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# **ENVIRONMENTAL TECHNOLOGY SERIES**

# Assessment of Sources of Air, Water, and Land Pollution

A Guide to Rapid Source Inventory Techniques and their Use in Formulating Environmental Control Strategies

Part One: Rapid Inventory Techniques in Environmental Pollution

BY

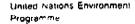
ALEXANDER P. ECONOMOPOULOS
DEMOCRITOS UNIVERSITY OF THRACE



WORLD HEALTH ORGANIZATION, GENEVA, 1993









World Health Organization



International Atomic Energy Agency



United Nations Industrial Development Organization

## Dear Recipient,

The World Health Organization is pleased to provide you with the latest revision to its rapid assessment manual, "Assessment of Sources of Air, Water, and Land Pollution." This document revises an earlier publication, "Management and Control of the Environment" (WHO/PEP/89.1) and was developed under WHO's Global Environmental Technology Network (GETNET). GETNET is a programme to enable authorities at the local, regional, and national levels to identify, assess, and take actions on their own to prevent or eliminate environmental problems which threaten public health.

In 1986, the World Health Organization teamed with three other United Nations agencies - United Nations Environment Programme (UNEP), United Nations Industrial Development Organization (UNIDO), and the International Atomic Energy Agency (IAEA) to form the Inter-Agency Project on Risk Management. The purpose of this programme is to develop an integrated approach to the identification, prioritization, and minimization of important industrial hazards in a given area. This publication represents WHO's contribution to the Inter-Agency Project.

We hope that this publication will be beneficial in identifying priorities for future efforts to reduce environmental pollution in your area. WHO is committed to continually updating the rapid assessment programme and to developing future improvements to the document such as training modules and simplified, computer programmes for use of the document.

Sincerely,

G. Ozolins, Manager

Prevention of Environmental Pollution

Division of Environmental Health

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Environmental management is often referred to as an art rather than as a science. The past twenty years has seen considerable progress toward revising this image. Numerous examples can be cited which show that proper planning can significantly reduce the impact of human activities upon the environment (Economopoulos, JAPCA 37:8, 1987). The difficulties in formulating sound environmental management programmes are especially pronounced in developing countries, and there is a need for practical tools that are suitable for widespread implementation and that permit the standardization of the critical initial stages of the planning process. This book attempts to address these requirements.

Some years ago, WHO published a book entitled Rapid Assessment of Sources of Air, Water and Land Pollution (WHO, offset publication No. 62, 1982), which focused primarily on the source inventory aspects of the management process. Translated into several languages, it has been widely distributed and the procedure described has been the subject of numerous training courses. The Rapid Assessment procedure has been found particularly useful in developing countries in the design of environmental control strategies and policies using relatively modest resources.

More recently, WHO updated and expanded the Rapid Assessment techniques by publishing a book entitled "Management and Control of the Environment" (WHO/PEP/89.1). This book strengthened the inventory portions, provided comprehensive lists of control options for each kind of air or water pollution source, and introduced some easy to use air and water quality models. This book, as well as its predecessor, has been found valuable in developing countries, and two of its reprints have already been exhausted.

In 1991, WHO initiated the Global Environmental Technology Network (GETNET), which had as its prime objective the strengthening, at the local level, of education and training materials on environmental pollution control technologies. This book, which succeeds a previous publication entitled "Management and Control of the Environment", is linked to the GETNET activities and will hopefully be widely used by developing countries to assess their environmental conditions and lead to making the environmental management process more of a science than an art.

The rapid assessment procedure is most useful in making an initial appraisal of the sources and levels of emissions from an area that has little or no previous pollution load data. It is also useful in selecting priority areas to conduct more extensive monitoring surveys; for conducting case studies as part of public health programmes directed at pollution control; and for formulating pollution control policies and regulations for national environmental health activities.

Part I of this book updates the rapid pollution assessment factors and introduces air, water and solid waste inventory and control models. It describes how to initiate a study, including how to organize study teams, how to define study areas, and how to collect, cross-check, organize and process field data so as to generate air, water and solid waste inventories, and, how to produce relevant reports to present to decision or policy makers. The necessary models and data for conducting air, water and solid waste inventories, for defining alternative control measures, and for assessing the pollution load reduction effectiveness of the latter are provided in Chapters 3 to 5. Study organization and implementation aspects are discussed in Chapter 6.

Part II of the book deals with environmental management problems and describes how to assess the current quality of air and water and how to identify land pollution problems; it also describes how to formulate alternative control strategies, how to evaluate their effectiveness and how to define high priority action programmes. The systems analysis approach, which sets the stage in the remainder of this book for the development of rational pollution abatement strategies, is presented in Chapter 7. Management approaches for urban and rural air pollution problems and selected air quality models are presented in Chapter 8, and for water pollution problems and selected water quality models in Chapter 9. Management approaches for municipal solid wastes and hazardous substances are discussed in Chapter 10.

While the focus of this new book is on the revision of the rapid assessment process, the model application techniques for air, water and solid wastes are greatly expanded. There is considerable discussion of various management approaches to consider once an environmental assessment of the area has been completed. The listing of all possible control and prevention strategies would, obviously, constitute an ambitious, if not impossible task. Accordingly, the management approaches described in Chapters 8 to 10 are to be regarded as suggestions for the development of an environmental control strategy for an area. Many of these techniques to reduce pollution have proven to be very powerful and should be given serious consideration in problem analysis and strategy synthesis. The user of this book should make use of the expanded tools and data for conducting or updating their emission inventories and then give serious consideration to the approaches suggested herein. WHO, through the GETNET and its many experts from all fields of environmental technology in over 65 countries, can provide assistance to developing countries in interpreting the results of the rapid assessment and in the selection of management approaches.

Work on this book started before its predecessor, "Management and Control of the Environment", was published, mainly in the form of research addressing the lack of suitable models, for the purposes of the present methodology. The content was discussed at a consultation held in Geneva in June 1991. The first draft was reviewed during a meeting held in Athens in July 1992. Mr. G. Ozolins, Manager, and Mr. D. L. Calkins, Scientist, both from Prevention of Environmental Pollution, Environmental Health Division, WHO Geneva, provided the necessary impetus for the writing of this book and their support and advice throughout the preparation period is gratefully acknowledged.

Thanks are also due to Mr. G. Ozolins, Dr. D. Mage, and Mr. D. Calkins, from the Prevention of Environmental Pollution, Environmental Health Division, WHO Geneva, for reviewing the source inventory and the section on air pollution management and for drafting most of the preface; to Dr. R. Helmer, from the Environmental Health Division, WHO Geneva, for reviewing the water pollution management; to Mr. P. Economopoulos, from the Association of Communities and Municipalities of Attika Region, for his valuable contribution to, and review of, the section on solid wastes management; and, to Mr. E. Giroult, from the Environmental Health Division, WHO Geneva, for reviewing the section on solid wastes management.

CHAPTER 1

INTRODUCTION

#### 1. Introduction

Environmental pollution affects the air we breathe, the water we drink and the food we consume. It also affects the production of food, the general quality of our surroundings and may pose a risk to our health and well-being. Control of environmental pollution is necessary in almost all communities and countries to protect the health of the population. The important question to be answered in each situation, is which pollutants should be controlled, in what way, and to what extent.

This book recommends the systems analysis approach and the simplification of analysis procedures in environmental management, both of which can be particularly effective in the analysis of existing problems and in the synthesis of control strategies:

The systems analysis approach, which is introduced in Chapter 7 of Part Two, is systematically followed in Sections 8.1, 9.1, and 10.1 dealing with the management of the air, water and land pollution problems. The essence of this approach lies in the analysis of existing problems and the identification of the most critical ones, in the setting of definite pollution control objectives and in the development of effective strategies to meet those objectives. The above requires the capability to conduct source inventories, to assess the impact of the released loads into the receivers, to define major control alternatives and to analyze their environmental, economic, and implementation consequences.

The systems analysis approach offers the important practical advantages of high cost-effectiveness and fast implementation, and its results can be impressive indeed. It creates however, particularly demanding analysis requirements, which have to be simplified and addressed through special tools and procedures, if it is to be practical and widely used.

The simplification of analysis procedures down to practical, and yet meaningful levels, while maintaining at the same time a highly integrated environmental management approach in relation to air, water and land pollution, has been the major challenge in the writing of this book.

The environmental management requirements were established through the following procedure: complex problems were decoupled into a series of much simpler ones; inventory and control models, as well as ambient quality models, capable of providing solutions in an effective and practical manner, were carefully selected and/or developed; the most important control measures were classified in categories and existing relevant data and information about their cost/effectiveness and implementation aspects were documented; and, finally, a coherent approach for the collection of the required information from the study area, the analysis and evaluation of the existing problems and the synthesis of truly effective management strategies was formulated, field-tested, and described.

The selection of analysis tools defines to a large extent, on the one hand the magnitude of resources required (manpower, skills, study duration, etc.), and on the other hand the reliability of the management results. The need thus arises for the screening of available models for the purpose of carefully balancing issues such as the accuracy and the reliability of predictions against the importance and relevance of results, ease-of-use and data requirements, or inter-model-compatibility. As ready, off-theshelf, models meeting the above requirements did not always exist, some models had to be adapted and expanded (e.g. the ECE CORINAIR model for traffic fuel consumption and air emission calculations), while several new models had to be developed (e.g. the air, water and solid wastes inventory and control models presented in Sections 3.2.2, 4.2.2 and 5.2.2, as well as all air quality models presented in Section 8.2).

For most developing nations, where environmental problems are often and available resources scarce, environmental management approaches based on the best available control technology tend to be too expensive, while those relying on the imposition of selective controls through local inspectorate decisions and public opinion feedback, tend to be unworkable (lack of inspector skills and other infrastructure requirements, long response times, etc, see Section 7.2.) The alternative systems analysis approach for environmental management, followed in this book, is believed to be better suited for developing nations as it offers a practical procedure for formulating costeffective strategies, targeted at selected critical problems, as well as detailed action programmes, which facilitate strategy implementation. It is thus hoped that the described procedure can contribute to better health and environmental quality protection, to conservation of valuable resources, and to unobstructed development in a rational and sustainable manner.

Designed as a work-book, this publication contains all the information required to analyze the current situation and to develop adequate management approaches, and additional information, such as conversion factors that facilitate the task. However, the measures derived through the recommended procedure, especially the complex and expensive ones, suitable should not be regarded as final or as for direct implementation, but rather as promising, high potential candidates which require further examination through more detailed feasibility studies.

Making assessments of environmental pollution and devising control strategies should not be viewed as a one-off effort, but rather as an on-going process. After an inventory of pollution loads has been made in a given area or country, it will need to be kept up-to-date and its accuracy improved. Similarly, control strategies will need to be reviewed as to their effectiveness and cost, while the efficiency of implemented measures will need to be monitored and compared with predictions, so as to provide quidance for the future. Assignment of these follow-up responsibilities to a specific government department is necessary, but the involvement of other government experts who would provide data and support to the total effort should be encouraged and stimulated. Examples of the latter are environmental and public health specialists, meteorologists and hydrologists, regional and country wide

planning specialists, statisticians with knowledge of industrial and other economic activities, etc. This network of experts could, in a spirit of fruitful cooperation, develop into a highly competent planning body with far reaching impact.

The environmental management techniques described in this book can be used at different levels: municipal or local, provincial or state, and national. At the local and regional level, the management results can be used for addressing the pollution problems in an effective way. At the national level, management plans from various regions can be combined and used in the formulation of a national environmental management policy, which offers notable advantages such as:

- Rationalization of allocated government funds for protection of the environment through clear national priorities;
- Improved implementation through appropriate distribution of relevant responsibilities among the central and local authorities. As a general rule, the implementation of relatively simple measures affecting numerous small local sources can best be handled by local authorities, while that of complex measures affecting larger areas, by central government services. An example of a measure suitable for the implementation by local authorities is Inspection Maintenance of central heating furnaces, and of measures suitable for implementation by central government are the changes in the fuel type or quality, or the setting of vehicle emission standards. Competent central government control and coordination is highly desirable in relation to the formulation, implementation and followup of national environmental plans;
- Valuable input can be offered in the formulation of other government plans and policies, in fields such as land planning, or the rational balancing of industrial and economic development against environmental quality.

# **CHAPTER**

2

## SOURCE INVENTORY TECHNIQUES

- 2.1 Alternative Source Inventory Approaches
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  - 2.1.2 Waste Monitoring Programmes
  - 2.1.3 Modeling of Pollution Source and Control Systems
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#### 2.1 Alternative Source Inventory Approaches

#### 2.1.1 Purpose and Objectives

The reliable assessment of the air, water and land polluting loads generated by each source, or by groups of similar sources, in the study area is essential for the identification of the nature, magnitude and origin of the existing pollution problems, as well as for the formulation of rational pollution abatement strategies.

Established methods to provide such information include direct monitoring of waste discharges, computer simulation of source and associated control systems, as well as the rapid assessment technique. In the sections that follow, these methods are described, their advantages and drawbacks outlined, and their possible combined use, so as to maximize the accuracy of the inventory results in a cost effective manner, discussed.

#### 2.1.2 Waste Monitoring Programmes

The direct monitoring of waste sources through sampling and analysis is an obvious approach and one of the earliest and most widely used. This method is indispensable in many cases, especially when the waste discharges from large sources need to be kept under close surveillance, or when environmental services need to verify compliance with the applicable liquid effluent and air emission standards.

The major advantage of the direct waste monitoring method is the accuracy of the inventory results. In the context of environmental management studies however, which are of prime importance here, this method may be extremely time consuming and resource intensive, and even impractical for large and complex study areas. For example:

Monitoring of the effluents from a leather tannery plant requires careful sampling as well as analysis to determine the concentration of a number of pollutants. As the effluent volume and composition changes significantly during the weekly production cycles, a fair number of samples need to be taken representing all major production phases, while the corresponding effluent rates must be determined. It is rather obvious that the resource requirements for the particular plant are high and could soon become prohibitive for a study area with numerous sources.

Monitoring of the exhaust emissions from a road vehicle is even more difficult as the rate depends on parameters such as vehicle speed, engine loading, engine and catalyst warm up status, and is thus continuously changing. In addition, a significant part of the emissions, the evaporative ones, are not released via the tail pipe, and the bulk of them not even while the vehicle is running. In cases like this, the on-line measurement of the emissions even

from a single vehicle is difficult, and obviously impractical from an entire fleet.

Based on the above discussion, source monitoring can improve the accuracy of inventories and should be pursued to the extent possible. However, priorities must be set, so as to have all important sources adequately covered. As the latter often account for the bulk of the released loads, accurate monitoring of their wastes contributes substantially to the accuracy of the overall inventory programme. For the same reasons, time and resource constraints that are always present should not lead to a superficial coverage of many sources, and especially to the collection and analysis of few random samples from each source, as the inventory results obtained this way are generally unreliable and highly unpredictable.

#### 2.1.3 Modeling of Pollution Source and Control Systems

The use of mathematical models, which simulate the behavior of certain sources, such as external and internal combustion sources, cement kilns, lime kilns etc, along with the performance of the attached control systems, constitutes one of the most advanced methods for reliably assessing not only the current emissions, but also the impact of possible design and operating modifications.

The disadvantages of the modeling approach include the practical difficulty of developing such models for the great variety of existing sources and control systems, and also the demand for the collection of often hard-to-find process and control system design and operating data during the source survey visits.

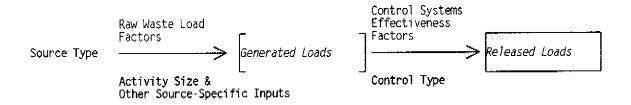
In reality the limited availability of models and the associated difficulties in assembling the required input data during field surveys restrict the application of the modeling approach during source inventory studies. In this book such models are used for predicting the emissions from Light Duty Gasoline Power (LDGP) cars, the flue gas volume from external combustion sources, as well as the drop in the temperature of flue gases passing through stacks. This selected use was deemed necessary for enhancing the accuracy of the air emission inventory results, as well as for generating inputs which are required for the application of air quality models. It should be noted that the sources concerned (LDGP cars and external combustion sources) are important contributors to air pollution problems, particularly in urban areas where they usually play a dominant role.

Validation of certain models under the local circumstances through balanced source monitoring programmes can be particularly beneficial and in some cases necessary, especially when large-scale measures are to be implemented. Verification using the emission model for LDGP cars is highly recommended if local measurements, or infrastructure allowing the generation of local monitoring measurements, exist. On the other hand, certain models such as the flue gas volume model do not need verification because they rely on stoichiometric relations.

#### 2.1.4 The Rapid Assessment Procedure

The rapid assessment methodology provides a particularly effective way of assessing air, water and solid wastes generated by each source, or groups of similar sources, within the study area. In addition, it permits convenient assessment of the effectiveness of alternative pollution control options.

This method is based on the documented, and often extensive, past experience of the nature and quantities of pollutants generated from each kind of source, with and without associated control systems, and, as Figure 2.1.4-1 illustrates, it makes constant use of this experience for predicting the anticipated loads from a given source.



Legend:

Bold: Field survey data Italic: Model output

Illustration of the rapid assessment approach for estimating the air, water and Figure 2.1.4-1 land pollution loads.

The advantages offered by the Rapid Assessment approach include convenience of use, which makes it possible to conduct integrated source inventories of air, water and land pollution sources in highly complex situations within only a few weeks time and with modest resources. Moreover, despite the simplicity of the method, the end result is often considered more reliable than that from direct source monitoring programmes in cases where shortcuts have to be taken (see also Section 2.1.2 above). Another significant advantage is the possibility of estimating conveniently the effectiveness of alternative control schemes in terms of their polluting load reduction potential. The latter constitutes a major input into the process of formulating rational control strategies.

A major disadvantage of the Rapid Assessment approach is the statistical validity of its inventory predictions. More specifically, the predictions from any given source need to be considered in many cases only as indicative as there is significant variation in normalized emissions between similar sources. Consequently, measures adopted immediately following Rapid Assessment need to be viewed as preliminary, subject to

subsequent, more detailed, analysis prior to implementation strategies.

#### 2.1.5 Combined Approaches

The source inventory approach in this book combines the Rapid Assessment method (see Section 2.1.4) with the selective (and streamlined) use of the modeling method (see Section 2.1.3). The end objective of the above combination is to enhance the accuracy of predictions while maintaining the overall simplicity of use.

Source inventory data and information, which can easily be generated for any study area, can be used for more effective planning of waste and ambient air and water quality monitoring programmes, in cases where extra resources are available and such information is desirable. Indeed:

Through the source inventory procedure described in this book, one can obtain information about the nature (polluting parameters of major interest) and the magnitude of the polluting loads released from each source. In most situations, a few large sources account for the bulk of the released loads (e.g. among 140 tanneries in a study area, the largest plant was found to account for 40 % of the total discharged loads, while the largest five plants contributed about 80 % to the total discharges) and these few dominant sources can be easily identified. Waste monitoring could then be restricted, at least in the initial phases, to the dominant sources, for it is often preferable to have reliable monitoring data from, for example 80 % of the discharges than shortcut data of unpredictable quality from 100 % of the discharges.

Based on the above, a carefully planned combination of the Rapid Assessment and the monitoring approaches could maximize the accuracy of the inventory results within the constraints of available resources.

Data and information from the Rapid Assessment methodology could be used, possibly along with the air and water quality models, for planning more effective ambient monitoring programmes. Information about the important parameters to be measured and about the critical location of the stations can easily be generated and could be a valuable input into the planning process of monitoring networks.

# 2.2 Screening and Classification of the Pollution and Waste Generating Activities

There are often many types of pollution-generating activities in a study area, and dealing with all of them in the context of an environmental management study, is not practical, nor even feasible. As discussed in Section 2.3 below, the objective of an effective source inventory approach is to assess on an individual basis the very large sources (such as power plants, steel mills, and municipal waste water outfalls) expected to have major impact on the environment of the study area. Other major sources of pollution to be considered are service stations, dry cleaners etc., which collectively have an appreciable impact on the environment.

While almost all industrial activities cause some pollution and produce some waste, relatively few industries (without appropriate air pollution control and waste treatment facilities) are responsible for the bulk of the air, water and land pollution loads generated in a given study area. Careful selection of the major pollution and waste-producing industries can greatly simplify the preparation of the assessment, while still covering most of the pollutants and wastes produced.

Table 2.2-1 presents a list of the industrial sources and processes that account for much of the industrial pollution and waste loads in almost any study area. The table also gives the corresponding Standard Industrial Classification (SIC) numbers (UN 1980, 1989) and indicates whether a specific industry or process is included in the appropriate air, water and solid waste inventory and control models of Sections 3.2, 4.2, and 5.2 respectively. The list could be used in the initial phases of the inventory work as a check list to identify the existing major industrial operations in the study area. The identification of industries to be included in the survey is very important and should be prepared with great care since it forms the basis for the remainder of the work to be completed.

List of activities included in the air, water, and solid waste inventory and control models, classified under the SIC system, UN (1989). Table 2.2-1

			Emissions <sup>a</sup>	Effluents <sup>a</sup>	Soli Wastes
0	Act	vities not Adequately Defined			
		Consumer Solvent Use Surface Coating	*		
ì	Agr	culture, Hunting, Forestry & Fishi	ng		
	11	Agriculture and Hunting 111 Agriculture and Livestock Production	*	*	
	12	Forestry and Logging 121 Forestry	*		
1	Min	ing and Quarrying			
	21	Coal Mining	*		
	22	Crude Petroleum & Natural Gas Pro	duction *		
	23	Metal Ore Mining	*		
	29	Other Mining	*		
;	Mani	ufacturing			
	31	Manufacture of Food, Beverages &	Tobacco		
		311/2 Food Manufacturing			
		3111 Slaughtering, preparing and pre	serving meat *	*	
		3112 Manufacture of dairy products		*	
		3123 Canning and Preserving Fruits 8	_	*	
		3114 Canning, preserving & Processin	7	74 Ju	
		3115 Manufacture of vegetable & anim	ıal oils & fats **	*	
		3116 Grain mill products 3117 Bakery products	•-	*	
		3117 Bakery products 3118 Sugar factories and refineries		*	
		3121 Food products not elsewhere cla	secified *	*	
		3122 Alfalfa dehydrating	*		
		313 Beverage Industries		.31.	
		3131 Distilling, rectifying and blem	ding spirits	*	
		3132 Wine industries	*	*	
		3133 Mait liquors and malt	*	*	
		3134 Soft drinks		~	

Table 2.2-1 (Continued)

	. Emis:	sions <sup>a</sup>	Effluents <sup>a</sup>	S Was
32	Textile, Wearing Apparel & Leather			
	321 Manufacture of Textiles			
	3210 Manufacture of textiles		*	
	322 Manufacture of Wearing Apparel, Except Footwear			
	3211 Spinning, weaving and finishing textiles	*		
	3214 Carpet and rug manufacture			
	323 Manufacture of Leather and Products of Leather			
	3231 Tanneries and leather finishing		*	
34	Paper & Paper Products, Printing & Publi.	shing		
	341 Manufacture of Paper and Paper Products	*	*	
	342 Printing Publishing and Allied Industries	*		
35	Manufacture of Chemicals, & Chemical, Petroleum, Coal, Rubber & Plastic Produc	t s		
	351 Manufacture of Industrial Chemicals	_		
	3511 Basic industrial chemicals except fertili		*	
	3512 Manufacture of fertilizers and pesticides		*	
	3513 Resins, Plastics & fibers except glass	*	*	
	352 Manufacture of Other Chemical Products			
	3521 Manufacture of paints, varnishes & lacque	:rs *	.b.	
	3522 Manufacture of drugs and medicines		*	
	3523 Manufacture of soap & cleaning preparatio	.1-	*	
	3529 Chemical products not elsewhere classifie	d *	*	
	353 Petroleum Refineries	_	*	
	354 Manufacture of Misc. Products of Petroleum and Co	al ~	•	
	355 Manufacture of Rubber Products		*	
	3551 Tyre & tube industries		•	
36	Non-metallic Mineral Products, Except Products of Petroleum & Coal			
	361 Manufacture of Pottery, China and Earthenware	*		
	362 Manufacture of Glass and Glass Products	*	*	
	369 Manufacture of Other Non-Metallic Mineral Product	5		
	3691 Manufacture of structural clay products	*		
	3692 Cement, Lime and Plaster	*		
	3699 Products not elsewhere classified	*		
37	Basic Metal Industries			
	371 Iron and Steel Basic Industries	*	*	
	372 Non-ferrous Metal Basic Industries	*	*	
38	Fabricated Metal Products, Machinery & E		.1.	
	381 Fabricated Metal Products, Except Machinery	*	*	
	384 Manufacture of Transport Equipment			

Table 2.2-1 (Continued)

			Emissions <sup>a</sup>	Effluents <sup>a</sup>	Solid Wastes <sup>a</sup>
4	Elec	ctricity Gas and Water		,	
	41	Electricity, Gas and Steam 4101 Electricity light & power	*	*	*
6	Who	lesale and Retail Trade			
	61	Wholesale Trade	*		
	62	Retail Trade	*	*	
	63	Restaurants and Hotels			
		631 Restaurants, Cafes, and other Eating & Drink	king	*	
		632 Hotels, Rooming Houses, Camps and Other Lodg	ging	*	
7	Trai	asport, Storage and Communication			
	71	Transport and Storage			
	<i>,</i> +	711 Land Transport	*		
		712 Water Transport	*		
		713 Air Transport	*	*	
		719 Services Allied to Transport			
		7192 Storage and warehousing	*	*	-1-
					*
9	Com	munity, Social and Personal Services			
	92	Sanitary and Similar Services	*	*	*
	93	Social and Related Community Service	s	*	
		931 Education Services		*	
		932 Medical, Dental and Other Health Services		_	*
	94	Recreational & Cultural Services		*	
	95	Personal and Household Services	*		
		952 Laundries, Laundry Services and Cleaning	*		

An asterisk in the column below indicates that the relevant industry or process is included in the appropriate air, water or solid waste inventory and control models of Sections 3.2.2, 4.2.2 and 5.2.2 respectively.

#### 2.3 General Description of the Rapid Assessment Procedure

As discussed in Section 2.1.4, and as shown in Figure 2.1.4-1, the calculation of the released loads from a given source is based on the use of appropriate waste load factors, which reflect the existing relevant experience from the measured performance of similar sources. Each waste load factor,  $e_j$ , is defined as the normalized released load of pollutant j expressed in kg/(unit of activity) of the particular source under consideration.

Sections 3.2.1, 4.2.1, and 5.2.1 present the rationale for the selection of the most appropriate "unit of activity" for each kind of source. Basically, the selected "activity unit" must bear a close and proportional relationship to the pollutant loads generated; it must also offer convenience during field-work (available field activity data must be commonly expressed in terms of the selected unit). The former makes the waste load factors,  $e_j$ , independent of the source size and activity level, and allows it to be expressed mathematically in the following form, as a function of several parameters:

The dependence of the waste factors ej on parameters such as those included in Equation (2.3-1) above, cannot be expressed in a continuous function form due to the discreet nature of most parameters (e.g. the type of control systems employed), and the lack of sufficient information in relation to the remaining ones. A discreet functional form yielding a series of waste factor values, each valid under a specific set of common and important parameter combinations, is used instead.

The above leads into the tabular constructs for the air, liquid and solid waste inventory and control models, which are presented in Sections 3.2.2, 4.2.2 and 5.2.2 and described in Sections 3.2.1, 4.2.1 and 5.2.1 respectively. These models introduce the impact of all major parameters into the assessment of the load released, while providing at the same time a precise definition of the data requirements from the field surveys. Sections 3.2.4, 4.2.4, and 5.2.4 elaborate on the latter.

Based on the above, the air, liquid and solid waste models presented in Sections 3.2.2, 4.2.2 and 5.2.2 provide values for the waste load factors, as well as guidance for the data to be collected from the study area. The applicable waste load factors along with the collected data can then be introduced into (blank photocopies of) the Working Tables, which are given in Section 3.2.3, 4.2.3 and 5.2.3.

In the above Working Tables the activity level of each source must be expressed in (1000 units/year). This activity value can then be multiplied directly by the waste load factors, which are always expressed in (kg/unit), to yield the released loads for all pollutants of major interest, expressed in (tons/year). The Working Tables provide room for listing not only the waste load factors and the source type and activity data, but also the computed inventory results. The latter can also be added together to provide partial or overall totals, e.g. for the loads released from a particular industry and/or for the loads released within the entire study area. This way, the field survey data are organized and documented in a concise manner, along with the applicable factors and the source inventory results.

Sections 3.2.4, 4.2.4 and 5.2.4 provide examples on how the air, liquid and solid waste inventory and control models of Sections can be used, along with the Working Tables of Sections 3.2.3, 4.2.3 and 5.2.3, to define the data requirements, to list the field survey results and to compute the released loads.

An important practical question, which often arises during source inventory studies, is when one should collect field data and compute the released loads for each source individually, and when one is justified to do so for a group of similar sources jointly. The answer is obvious for the relatively few large sources (e.g. an electric power plant), for which calculations on an individual basis are required, as well as for groups of numerous small sources of similar type and with similar controls (e.g. space heating furnaces), for which joint calculations are necessary. In the latter case the combined overall activity (e.g. the total heating oil consumed by the space heating furnaces in 1000 tons/year) is entered in the Working Tables and the overall waste loads produced jointly from all such sources are computed.

Between the very large individual sources and the groups of numerous but very small sources, there is a grey area, for which the decision on how to proceed must be based on careful judgment as it may significantly affect both the amount of work involved and the accuracy of the results. As a general rule, when numerous small to medium size sources exist within our study area or sub-area, one should try first to classify them into one or more groups, for which common sets of waste load factors apply, and calculate their combined waste load releases. This has some distinct advantages, since data about the combined overall activity are often easily available from government sources and industrial associations, etc (see Section 6.3.3) and these data are often reliable. Moreover, the entire assessment procedure is greatly simplified and a clearer overall picture is obtained. The classification however of the small sources in groups of similar type, and especially the distribution of the known overall activity among the groups, is not always straightforward and some pertinent information from knowledgeable persons is usually required.

As an example let us assume that in a study area 140 tanneries are operating, one of which is known to be large, half a dozen of them to be of medium size, and the rest small. A sensible inventory approach would be to visit the large and the biggest of the medium-size tanneries so as to calculate their effluent loads on an individual basis. For the remaining ones, one should try to obtain data about their collective output (i.e. tons of hides processed annually) as well as information about the process used (e.g. chrome or vegetable tanning) and the kinds of control systems employed (e.g. no control or primary sedimentation). On the basis of this information one could then form a number of groups, each of which comprises tanneries of the same process and of the same effluent controls. Assume for example that the information collected indicated that about 80 % of the hides are chrome tanned and that no controls are used as the effluents are discharged directly into the sewerage system. Under such circumstances two groups need to be considered, one comprising all production lines employing tanning, and a second one comprising the remaining production lines employing vegetable tanning. The collective activity of the former is 80 % of the known total for all small plants, while the collective activity of the latter accounts for the remaining 20 %.

#### 2.4 Validity of Waste Load Factors

The waste load factors listed in the inventory and control models of Sections 3.2, 4.2, and 5.2 relate, as we have seen, to major production or other industrial activity sectors. These factors have been obtained from a multitude of different books, documents, and scientific articles gathered from different parts of the world. They have subsequently been evaluated and cross checked before being inserted into the models. Particular attention has been given to the reliability of the factors, as this is directly related to the validity of inventory results. There are however, certain limitations associated with the use of factors, which must be considered:

For any given activity, the waste load factors vary from source to source, and this variation is sometimes very significant. Such variations are often the results of different operating practices, but may also reflect differences in the design and layout of the equipment. The factors provided are selected to represent as much as possible, average or typical conditions. As a result it can be expected that the waste load predictions on any individual source basis may occasionally differ significantly from the actual waste loads generated. Overall load predictions for several similar plants, e.g. the total polluting loads in the effluents of many tanneries operating in a given area should however, be reasonably accurate.

The accuracy of the factors provided is not uniform as it depends the nature of the source, on the pollutant generating mechanisms, and on the extent of the characterization and measurement studies done. As an example, the SO<sub>2</sub> emission factors from external and internal combustion sources can be considered very accurate since they are stoichiometrically related to the sulfur content of the fuel. No other emission factors for combustion sources bear such a close relationship to a well defined and known parameter (the sulfur content) and they are thus

less accurate. Furthermore, some of them, are based on relatively few measurements and exhibit wider variation.

The question often arises as to the validity of factors across different countries, especially those derived in industrialized countries when applied to developing countries. For example, because of differences in source inspection and maintenance, or because of differences in the size of a "typical" plant, somewhat higher factors could be justified. However, extensive use of the Rapid Assessment procedure (WHO, 1982), for over a decade in many parts of the world has shown that this is not a significant problem.

The general conclusion so far is that the application of the Rapid Assessment procedures should generally be expected to produce acceptable accuracy for the management purposes intended. The accuracy could be improved in cases where information about local factors is available and assessments should be derived from these whenever possible. Such refinements, along with the increase in the number of experienced personnel, are expected to improve results and in turn, the quality of environmental management.

#### 2.5 Bibliography

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## CHAPTER

3

# AIR EMISSION INVENTORIES AND CONTROLS

- 3.1 Compilation of Air Emission Inventories Under Present and/or Strategy Target Conditions:
- 3.2 Model for Compiling Air Emission Inventories and Assessing the Effectiveness of Applicable Controls
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- 3.3 Model for the Exhaust and Evaporative Emissions from LDGP Vehicles Under Specific Driving, Climatic and Gasoline Volatility Conditions
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- 3.5 Model for the Temperature Drop through Stacks
  - 3.5.1 Introduction
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  - 3.5.3 Example
- 3.6 Bibliography

# 3.1 Compilation of Air Emission Inventories Under Present and/or Strategy Target Conditions

This chapter presents four models, two of which can be used for computing the air emission loads generated under present and strategy target conditions, while the remaining two can be used to calculate the flue gas volume from external combustion furnaces, as well as the gas temperatures at the stack exit point, as a function of the inlet gas temperature. The output from the latter models, along with the inventory results, are necessary for assessing the impact of point sources on the air quality, as well as for formulating appropriate mitigation strategies (see Chapter 8).

Among the inventory models provided in this chapter, that of Section 3.2.2 represents a general one applicable to all sources of interest in the study area. This model provides five columns listing the emission factors (see Section 3.2.1 below) for the "conventional" pollutants TSP,  $SO_2$ ,  $NO_X$ , CO, and VOC, as well as a sixth column reserved for other important substances, as the case may be, for each source considered. The procedural aspects for the calculation of the air emission loads are presented in Section 2.3 and demonstrated through an example in Section 3.2.4. In this model, the particularly important source category of Light Duty Gasoline Powered (LDGP) cars, is covered through a simplified procedure, allowing the computation of the typical annual emissions in urban areas with temperate climate under typical driving patterns.

The model in Section 3.3 focuses on the computation of the LDGP car emissions and supplements the above general model by providing a more elaborate computational procedure, which allows the user to derive emission factors adapted to local driving habits and to the prevailing annual or seasonal climatic conditions. The use of this model is described in Sections 3.3.2.1 and 3.3.3.1 and is demonstrated through examples in Sections 3.3.2.2 and 3.3.3.2.

To conclude this discussion on the source inventory, some remarks are warranted in relation to the procedure followed for the computation of road traffic emissions and justification of the particular emphasis placed on this source category:

The importance of road traffic emissions in urban areas stems from their dominance in terms of the emitted loads, the low level of their release, and from their adverse spatial distribution (the highest emission densities are generally encountered in the highest population density areas). As a result, the impact of road traffic emissions on urban air quality and on the health of the general population is significant.

Assessment of the emissions from LDGP cars, by far the most important category of road vehicles, presents particular difficulties as these emissions are highly variable and dependent on a number of parameters, such as the age and size distributions of the vehicles in the fleet, the severity and the period of enactment of the emission standards legislation, local driving patterns, and local annual or seasonal climatic conditions.

From the published data and information about the LDGP car emission factors, those from the U.S. EPA (1989) and from the Commission of the European Communities (1989) stand out clearly for their completeness. The U.S. EPA data reflect a situation not representative of developing countries since most of the U.S. fleet now uses catalytic converter technologies (strict measures have been imposed since 1980) and comprises vehicles of unusually large size. The CEC legislation on the other hand followed the evolution of engine design, and the periodically updated emission standards closely reflected the improvements obtained from the progress in the conventional (non catalytic) engine design technologies. Only from 1993 will catalytic technologies become mandatory through CEC regulations. Furthermore, the European fleet comprises a relatively high proportion of small vehicles, which are more suitable for the congested European city traffic conditions.

Based on the above, the CEC data appear to be representative for most countries and are used in this book. Nonetheless, the use of local factors, if available, is encouraged, especially for countries where the local car production is not export oriented and/or without reasonably strict vehicles emission standards, as higher emissions than the computed ones may be anticipated.

From the analysis of the CEC data, two models have been derived and are presented here. A simple one, which is suitable for computing typical annual emissions in congested urban areas with temperate climate, has been streamlined and incorporated in the general emission load model of Section 3.2.2. A specific model, allowing users to derive more accurate factors on the basis of local driving habits and on the prevailing annual or seasonal climatic conditions, is presented in Section 3.3.

The flue gas volume model presented in Section 3.4, allows convenient assessment of the actual gas volume from external combustion sources as a function of the easily measured (or assumed) CO2 concentrations. This information is required for estimating the ambient concentrations from point sources through the application of dispersion models (see Section 4.2.1). As the majority of point sources, for which air quality models are applied are industrial or utility boilers, the present model should cover a significant part of the gas volume data requirements.

The stack temperature drop model presented in Section 3.5 allows convenient computation for the stack-gas exit temperature, as a function of the stack-gas inlet temperature and other variables (physical stack height and diameter, and flue gas volume). It should be noted that although the flue gas exit temperature is a key variable for the use of air quality models, only the stack gas inlet temperature is usually known from literature and/or from direct measurements. The present model holds for both insulated and non-insulated stacks and addresses the input requirements of the air quality models by properly interfacing the raw data which are normally available from field surveys.

# 3.2 Model for Compiling Air Emission Inventories and Assessing the Effectiveness of Applicable Controls

#### 3.2.1 Introduction

The quantities of emissions released into the atmosphere from any industrial or other activity depend, in general, on a number of parameters. Thus, the emission E of pollutant j could be expressed in a mathematical form as follows:

The source type defines the kind of pollution generating activity in somewhat broad terms, e.g. cement manufacturing, vehicle traffic, external fuel combustion. More precise definition is provided through other parameters as discussed below. Obviously, the source type is a parameter which is closely related to the type and quantity of pollutants emitted.

Through the source type parameter alone it is possible to simplify very substantially the source inventory and the air pollution management tasks by excluding right from the start numerous activities with relatively minor air pollution potential.

The unit of activity, referred to simply as unit hereafter, defines an acceptable way of expressing the activity of a given source. Suitably defined units can be used to provide a measure of the services offered (e.g. the mileage of the vehicles in relation to the traffic in a study area, or the aircraft landing and take off cycles in relation to an airport), of the raw materials consumed (e.g. the fuel oil burned by an industrial boiler) or of the products manufactured (e.g. the quantity of cement produced by a cement manufacturing plant).

Selection of the most suitable unit for each type of activity is important, as the unit must have a direct relation to the pollutant loads emitted, and must offer convenience in obtaining the required data during the field work. For example, the activity of an industrial boiler could be characterized by the quantity of fuel used, or by the quantity of steam generated. The former is directly related to pollutant emissions, while the latter only indirectly (other parameters such as the overall thermal efficiency of the boiler are involved). Moreover, in practice is it easier to obtain reliable data on fuel consumption (both on a

plant, as well as on a regional basis) than on the quantities of steam generated. Hence, a unit related to fuel consumption would then be appropriate for characterizing the activity of the boiler.

In some cases alternative units are provided to facilitate the field work. For example, in the case of road vehicles, units related to the distance driven or the fuel consumed can be used.

Source size, although a key parameter, is only indirectly related to the normalized emissions rate (emission loads per unit activity). In general, economies of scale allow better design and operation, as well as stricter emission controls for larger size units. Moreover, for industrial sources, selection of the particular process to be used is often dictated by plant size. It is for these reasons that emission standards are generally significantly stricter for large plants.

In the context of the present methodology the effects of plant size on the normalized emission loads can be taken into consideration only in cases where the source size affects the process selection. In some important cases however, as in the calculation of emissions from vehicle traffic, separate vehicle size categories are considered.

- Process or design particularities are very much related to the kinds and to the quantities of pollutants emitted from industrial sources. For example, different kinds of kilns in the production of lime and cement, or different types of furnaces in the metallurgical industry result in greatly varying emission rates.
- Source age and technological sophistication are important parameters, as they often significantly affect the emission loads. The aging of a source causes higher emissions as systems tend to fail more frequently and their operation tends to depart from the new equipment specifications. In addition, older systems do not take full advantage of technological innovations, which tend to yield environmentally friendlier performance. Naturally, the technological sophistication does not only depend on the age of the source alone, but also on the environmental legislation, as well as on enforcement aspects.

A well known example of the impact exerted by the age of the source and the severity of legislation on emissions is in the case of motor vehicles. Continuing improvements in engine design over the past 20 years have resulted in the production of vehicles with progressively diminishing emissions. Age aspects of light duty passenger cars are dealt with here in detail as they play a dominant role in urban air pollution.

Source maintenance and operating practices is another parameter significantly affecting emission loads. Fortunately, for the vast majority of industrial sources, proper maintenance and operation is also intimately related to production quality and costs and for this reason is usually practiced to acceptable standards. For smaller sources however, improper maintenance and operation is the rule rather than the exception, despite the associated economic losses.

A particularly important example of the impact of improper maintenance on emissions is in the case of internal and external combustion sources (industrial or domestic boilers and motor vehicles). Proper maintenance practices for certain of these sources are described in our emissions model, as they offer potent control alternatives for urban air pollution problems, along with significantly lower fuel consumption and economic savings as well.

The type and the quality of the raw materials used is in may cases intimately related to the types and to the quantities of pollutants emitted. In industrial processes the type and the quality of raw materials available often dictate the process to be used and the emission loads released by them. However, the most important, and perhaps the most striking impact, is in the case of internal and external combustion sources, where the type and the quality of fuel used exert a dominant impact on the urban air quality. Based on the above, it is not surprising that possible improvements in the type and in the quality of the fuel used, offer some of the most potent air pollution management options. In our emissions model the general subject of the raw materials type and quality is treated with particular attention due to its significant practical importance.

The type, design, and age of the control systems employed determine the removal efficiencies of the source emissions and are thus intimately related to the loads eventually released into the atmosphere. It should be noted that all parameters discussed so far in this section are associated with the generation of emissions and their reduction at source level. Only this one deals with the reduction of the emissions once they have been generated by the source.

The type of the control system employed defines by itself the capabilities and limitations (and hence the control efficiency range) for the source under consideration. Analytical design characteristics allow a better insight and a more accurate assessment of the control system efficiency, but relevant data are difficult to collect in practice and difficult to use. The age of the control system affects the emissions due to the progressive downgrading of the performance with time, but, most importantly, due to the generally more relaxed design specifications of the past. Old age of equipment tends thus to be associated with lower design efficiencies.

In our inventory model the type of control system is used as the leading parameter for assessing the control system performance. The age of the control system is an additional parameter, which is used in selected cases. Detailed assessments on the basis of specific design characteristics are however not addressed, as typical design practices are assumed.

The ambient conditions may significantly affect the rate of emissions. For example, wind velocity and/or rainfall affect the TSP emissions from roads and material storage facilities, while temperature affects considerably the road traffic emissions. The impact of the ambient conditions has been incorporated in our emissions model for selected sources.

The above discussion leads into the important practical question of how the emission load  $E_j$  could be expressed as a direct and explicit function of all the parameters that may affect it for all pollutants j of interest.

The first step in this direction is to define the emission factor  $\mathbf{e_i}$  for pollutant j, through the following relation:

$$e_j = \frac{E_j, kg/yr}{Source activity, Units/yr}$$
 (3.2.1-2)

The emission factor ej is normally expressed as kg/unit and is assumed to be independent of the source size and the source activity (or production) level. The basis for this important assumption is the way the activity units are selected. Indeed, as discussed above, a key criterion in the selection of the activity units is their direct and proportional relation to the emission loads generated. From the above and from Equation (3.2.1-1) we obtain:

(3.2.1-3) $e_i = f'(Source type,$ Process or design particularities, Source age and technological sophistication, Source maintenance and operating practices, Type and quality of the raw materials used, Type, design and age of the control systems employed, Ambient conditions, etc.)

The emission factor ej is used extensively hereafter, as the key objective of the air emissions model is to define the value of e<sub>i</sub> for every significant source and for every pollutant of interest j.

The dependence of the emission factors  $e_j$  on the parameters discussed above and listed in Equation (3.2.1-1), cannot, in most cases, be expressed in a continuous function form due to the discreet nature of most parameters (e.g. type of fuel or type of control equipment used), and to the frequent lack of sufficient information in relation to the remaining parameters. A discreet functional form yielding a series of emission values, each valid under a specific set of common and important parameter combinations, is used instead.

The discreet rather than the continuous nature of the emission factor values leads into the tabular construct of the model in Section 3.2.2, into which the source types are organized on the basis of the UN Standard Classification of Industries and Services. Under each activity listed, all important individual sources are included (e.g. under Gypsum manufacturing, the Rotary Ore Dryers, the Raw Mills and the Calciners are included); for each such source all major alternative processes are listed (e.g. in Gypsum manufacturing and under Calciners, the Flash and the Continuous Kettle Calciners are listed); and for each such process all major control alternatives are provided (e.g. in Gypsum manufacturing, under Calciners and under the Continuous Kettle Calciners the Uncontrolled, the Fabric Filter and the Electrostatic Precipitator control alternatives are provided). For each such combination of parameters the applicable emission factors are given for the pollutants of interest.

The impact of the raw materials type and quality is either expressed directly through a relation (e.g. in the case of the SO2 and TSP emission factors in several external combustion activities), indirectly through the listing of alternative processes (the process selection often depends on the raw materials available), or is described in the footnotes. Similar provision is made for the remaining parameters, whenever their impact becomes important. The impact of the ambient conditions (as well as of the local driving patterns) for light duty passenger cars is examined separately in Section 3.3 because of its particular importance for urban pollution.

The tabular structure and the form of Section 3.2.2 constitutes a rather elaborate air emissions model by introducing the impact of all major parameters into the assessment of the air emissions releases, and by providing a precise definition of the data requirements from field surveys. The model of Section 3.2.2 is thus a valuable tool for source inventory studies, not only for computing the emissions, but also for providing guidance on the data to be collected during the field survey work, as well as for organizing and presenting such data in a concise manner (see also Sections 3.2.3 and 3.2.4 below).

In addition, the model in Section 3.2.2 should be a valuable tool in air pollution management studies as it provides a clear picture of the existing sources and emissions and, along with it, a fairly comprehensive list of the available alternative process modifications and control equipment options for each activity and each source therein, as well as identification of the parameters that exert a particular influence on the emissions and quantification of relevant changes (e.g. quantification of the impacts from possible changes in the types and qualities of the fuel used). The above constitute key elements in the analysis of air pollution problems and the formulation of effective control strategies for any given urban or industrial area.

Finally, the model in Section 3.2.2 is useful in Environmental Impact Assessment Studies as it provides, in a convenient form, quantification of the impacts of alternative process and emission control system selections for most sources and activities of interest.

#### Model for Air Emission Inventories and Controls 3.2.2

≀ SIC#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U —————	kg/
MAJOR	DIVISION O. <u>ACTIVITIES NOT AD</u>	EQUATELY DEFINED						
	Consumer Solvent Use <sup>1</sup>	(Person)*(year)					4.2	
	Surface Coating							
	Paint	tn consumed					560	
	Varnish	tn consumed					500	
	Lacquer	tn consumed					770	
	Ename 1	tn consumed					420	
	Primer (Zinc Chromate)	tn consumed					660	
IOLAM	R DIVISION 1. AGRICULTURE, HUNT	ING, FORESTRY AND FIS	HING					
111	Agricultural and Livestock Prod	uction						
	Open Burning of Agricultural Ma	terials						
	Field Crops	tn	11.0			58	9.0	
		1000 m <sup>2</sup> of land	5.0			26	4.0	
	Vine Crops	tn	3.0			26		
		1000 m <sup>2</sup> of land	1.7			15		
	Weeds	. tn	8.0			42		
		1000 m <sup>2</sup> of land	5.8			30	3.2	
	Orchard Crops	tn	3.0			26	4.0	
		1000 m <sup>2</sup> of land	1.0			9	1.4	
	Forest Residues	tn	8.0			70	9.0	
		1000 m <sup>2</sup> of land	12.6			110	14.0	
121	Forestry							
	Charcoal Manufacturing	<b>.</b>	175		10	172	157	
	Uncontrolled	tn 			12 12			
	Afterburners	tn	23		12	34	Δī	
MAJO	R DIVISION 2. MINING AND QUARK	<u>/ 1ng</u>						
210	Coal Mining							
	Coal Cleaning							
	Coal Drying							
	Fluidized Bed Dryer				0 07		0.05	
	Uncontrolled	tn of dried coa!		0.22			0.05	
	Cyc ione	tn of dried coal	6	0.22	0.07		0.05	

The listed factor includes evaporation losses from the use of polishes, waxes, deodorants etc. and tts value is related to the standard of living of people in the study area. A lower value than the listed one may be is more appropriate for areas with low standard of living.

## Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS			UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/U	VOC kg/U		kg/U
	Wet Scrubber	tn o	f ·	dried coal	0.05	0.13	0.07		0.05		
	Flash Orier										
	Uncontrolled	tn o	f .	dried coal	8						
	Cyc lone	tn o	f	dried coal	5						
	Wet Scrubber	tn o	f	dried coal	0.2						
	Multilouvered Orier										
	Uncontrolled	tn o	f	dried coal	13						
	Cyc lone	tn o	f	dried coal	4						
	Wet Scrubber	tn a	f (	dried coal	0.05						
220	Crude Petroleum and Natural Gas F	roduct	io	n							
	Desulfurization of Natural Gas <sup>2</sup>			1000 m <sup>3</sup>	1	4.2(1-	e)H <sub>2</sub> S				
				1000 m <sup>3</sup>	1	6.6(1-	e)S				
				tn of gas	1	7.1(1-	e)H <sub>2</sub> S				
				tn of gas	2	0(1-e)	S				
2302	Non-Ferrous Ore Mining										
2302	Non-Ferrous Ore Mining Metallic Mineral Processing (Low	/ Moist	ΔŤ	e Ore)							
2302	-	/ Moist	ШŤ(	e Ore)							
2302	Metallic Mineral Processing (Low	/ Moist	ШŤ	e Ore)							
2302	Metallic Mineral Processing (Low Uncontrolled	/ Moist	ШŤ	e Ore) tn	0.2						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing	/ Moist	Uť		0.2 0.6						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary	/ Moist	ůř:	tn							
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary	/ Moist	ut:	tn tn	0.6						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary	/ Moist	ШŤſ	tn tn	0.6						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding	/ Moist	ur	tn tn tn	0.6 1.4						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge	/ Moist	ÚŤſ	tn tn tn	0.6 1.4 1.2						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept	/ Moist	ur	tn tn tn tn	0.6 1.4 1.2 14.4						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept		<b>Ú</b> ተና	tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8						
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept Drying Fabric Filter or Scrubbers		ur	tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8 1.5					РЬ	0.15
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept Drying Fabric Filter or Scrubbers		Uť	tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8 1.5					Pb Pb	0.15 0.006
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept Drying Fabric Filter or Scrubbers  Leadbearing Ore Crushing and Grin Pb Ores		Uť	tn tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8 1.5						0.006
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept Drying Fabric Filter or Scrubbers  Leadbearing Ore Crushing and Grin Pb Ores Zn Ores		Uť	tn tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8 1.5					РЬ	0.006 0.006
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept Drying Fabric Filter or Scrubbers  Leadbearing Ore Crushing and Grin Pb Ores Zn Ores Cu Ores		ure	tn tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8 1.5					Pb Pb	0.006 0.006 0.06
2302	Metallic Mineral Processing (Low Uncontrolled Crushing Primary Secondary Tertiary Dry Grinding Gravity Discharge Air Swept Drying Fabric Filter or Scrubbers  Leadbearing Ore Crushing and Grin Pb Ores Zn Ores Cu Ores Pb-Zn Ores		Uti	tn tn tn tn tn tn	0.6 1.4 1.2 14.4 9.8 1.5					Pb Pb Pb	0.15 0.006 0.006 0.06 0.06

<sup>(</sup>a) "e" is fractional efficiency of sulfur recovery plants with typical values as follows: for uncontrolled 2-stage sulfur recovery plant: from 0.920 to 0.950 for uncontrolled 3-stage sulfur recovery plant: from 0.950 to 0.975 for uncontrolled 4-stage sulfur recovery plant: from 0.960 to 0.990 for controlled sulfur recovery plant : from 0.990 to 0.999

<sup>(</sup>b) " $H_2S$ " is the mole percent of  $H_2S$  in natural gas (1 mole %  $H_2S$  = 0.966 weight %  $H_2S$  or 0.856 weight % Sulfur), while "S" is the weight percent of sulfur in the natural gas.

Model for Air Emission Inventories and Controls - Cont'd

SIC# PROCESS	UNIT	(U)	TSP kg/U	SO <sub>2</sub> kg/U ——	NO <sub>X</sub> kg/U	CO kg/U ——	VOC kg/U ───	kg/∪
2901 Stone Quarrying, Clay and Sand Pits							•	
Sand and Gravel <sup>3</sup>		tn	0.134					
Stone Quarrying and Processing <sup>4</sup> Uncontrolled								
Wet Quarry Drilling		tn	0.4					
Blasting		tn	?					
Batch Drop								
Truck Unloading		tn	0.17					
Truck Loading								
Conveyor		tn	0.17					
Front End Loader		tn	29.					
Conveying		tn	1.7					
Drying		ţn	17.5					
Crushing								
Primary+Secondary Crushing								
Dry Materials		tn	0.14					
Wet Materials		tn	0.009					
Tertiary Dry Materials		tn	0.93					
2902 Chemical and Fertilizer Mineral Min	ing							
Phosphate Rock Processing								
Drying or Calcining								
Drying								
Uncontrolled		tn	2.9					
Low Pres Venturi Scrubber		tn	0.29					
High Pres Venturi Scrubber		tn	0.06					
Calcining								
Uncontrolled		tn	7.7					
Low Pres Venturi Scrubber		tn	0.77					
High Pres Venturi Scrubber	,	tn	0.16	ı				
Product Grinding								
Uncontrolled		tn	1.5	1				
Fabric Filter		tn	0.01					
Transfer and Storage		ŧn	1					
Open Storage Piles		tn	20	1				

Emissions from the material hauling are not included as they can be computed separately (see factors listed in group 711).

Emission factors apply in cases where granular materials are found in near-surface alluvial deposits and in processing operations involving initial dry screening followed by wet processing for screening and silt removal to produce washed sand and gravel. In situations where silt is removed by air blowing, a significant portion of the raw material may be blown in the air resulting in very high dust emissions.

 $\label{thm:model} \mbox{Model for Air Emission Inventories and Controls - Cont'd}$ 

SIC# PROCESS	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/IJ	NO <sub>x</sub> kg/U	C0 kg/U	VOC kg/U		kg/U
MAJOR DIVISION 3. MANUFACTURING								
DIVISION 31. MANUFACTURE OF FOOD. BEVERA	GES AND TOBACCO							
3111 Meat Smokehouses								
Uncontrolled	tn	0.15			0.3	0.18		
Low Voltage ESP or Afterburner	tn	0.05			0.0	0.075		
3114 Fish Processing (Canning & Manufactur	re of by-product	:s)						
Steam Tube Driers	tn	2.5					H <sub>2</sub> S	0.05
Direct Fired Driers	tn	4.0					H <sub>2</sub> S	0.05
3116 Grain Mills								
Feed Mills, Uncontrolled	tn	4.9						
Wheat Milling								
Uncontrolled	tn	38.0						
Cyclones & Fabric Filters	tn	0.8						
Durum Milling, Uncontrolled	tn	3.0						
Rye Milling.								
Uncontrolled	tn	38.0						
Cyclones & Fabric Filters	tπ	0.8						
Oat Milling, Uncontrolled	tn	1.25						
Rice Milling, Uncontrolled	tn	2.97						
Soybean Milling, Uncontrolled	tn	11.73						
Dry Corn Milling, Uncontrolled	tn	6.25						
Wet Corn Milling, Uncontrolled	tn	6.24						
3121 Starch Manufacturing								
Uncontrolled	ţn	4.0						
Controlled <sup>5</sup>	tn	0.01						
3122 Alfalfa Dehydrating								
Primary Cyclone								
No Secondary Controls	tn	5						
Medium Energy Wet Scrubber	tn	0.5						
Meal Collector Cyclone								
No Secondary Controls	tn	2.6						
Fabric Filter	tn	0.03						
Pellet Cooler Cyclone								
No Secondary Controls	tn	3						
Fabric Filter	tn	0.03						
3133 Beer Brewing	tn of cereal	4.0				1.3		
m <sup>3</sup> of beer	0.8				0.25			

TSP emissions from the various corn cleaning, grinding, and screening operations can be controlled by centrifugal gas scrubber.

12

#### Model for Air Emission Inventories and Controls - Cont'd

SIC# PROCESS	UNIT (U)		_	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U	ر kg/V
3133 Wine Production	m <sup>3</sup> of wine					0.35	
DIVISION 32. TEXTILE, WEARING APPAREL & I	LEATHER INDUSTRIE	Es					
321 Textile Fabric Printing	tn of fabric					142	
3211 Cotton Ginning Uncontrolled Cyclones, in-line filters etc	tn of cotton tn of cotton	7.0 4.48					

#### DIVISION 33. MANUFACTURE OF WOOD & WOOD PRODUCTS, INCLUDING FURNITURE

#### 331 Manufacture of Wood and Wood and Cork Products, Except Furniture

Plywood Veneer Fugitive Emissions tn of logs 0.187 Log Debarking & Sawing th of logs 0.167 m<sup>2</sup> of plywood 0.05 Plywood Cutting & Sanding Sawdust Handling tn of Sawdust 0.5 1000m<sup>2</sup> Dryers

DIVISION 34. MANUFACTURE OF PAPER AND PAPER PRODUCTS. PRINTING AND PUBLISHING

#### 341 Manufacture of Paper and Paper Products

Sulfate (Kraft) Pulping						
Bigester, Brown Stock Washer Multiple Effe	ct Evapo	rator				
Uncontrolled	tn				H <sub>2</sub> \$	0.58
					Merc	1.15
Recovery Boiler						
Recovery Boiler & Direct Contact Evapor.	ator					
Uncontrolled	tπ	90.	3.5	5.5	H <sub>2</sub> S	6
					Merc	1.5
Venturi Scrubber	tn	24.	3.5	5. <b>5</b>	H <sub>2</sub> S	6
					Merc	1.5
Venturi+Auxilliary Scrubber	tn	7.5	3.5	5.5	H <sub>2</sub> S	6.
•					Merc	1.5
923	tn	1.	3.5	5.5	H <sub>2</sub> \$	6.
					Merc	1.5
ESP+Auxilliary Scrubber	tn	1.5	3.5	5.5	H₂S	6.
					Merc	1.5
Recovery Boiler Without Direct Contact	Evapora:	tor				
Uncontrolled	tn	115.		5.5	H₂S	0.05
FSP	tn	1.		5.5	ห_้ร	0.05

Model for Air Emission Inventories and Controls - Cont'd

Mesh Pad       tn 0.5 0.1       5.5       H <sub>2</sub> S 0.1         Merc 0.15         Scrubber       tn 0.1       5.5       H <sub>2</sub> S 0.1         Merc 0.15         Lime Kiln       Uncontrolled       tn 28. 0.15       0.05       H <sub>2</sub> S 0.25         Merc 0.1         Scrubber or ESP       tn 0.25       0.05       H <sub>2</sub> S 0.25         Merc 0.1	SIC# PROCESS		UNIT	(U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U		kg/U
Uncontrolled	Smelt Dissolving	Tank									
Mesh Pad				tn	3.5	0.1		5.5		-	0.1
Scrubber	Mesh Pad			tn	0.5	0.1		5.5		H <sub>2</sub> S	0.1
Lime Kiln  Uncontrolled  tn 28. 0.15 0.05 H <sub>2</sub> S 0.25  Mero 0.1  Scrubber or ESP  tn 0.25 0.05 H <sub>2</sub> S 0.25  Mero 0.1  Miscellaneous Sources  tn Merc 0.25  Sulfite Pulping  Digester Blow Pit or Dump Tank  Uncontrolled  tn 335.  Mg0 Base System  Process Changes  Process Changes  Scrubber  tn 0.5  Process Changes+Scrubber  tn 0.1  All Exhausts through  Recovery Systems  Process Changes tn 0.2  NH <sub>3</sub> Base System  Process Changes tn 12.5  Process Changes tn 0.2  Na Base System  Process Changes+Scrubber  tn 0.2  Na Base System  Process Changes+Scrubber  tn 0.2  Na Base System  Mg0 Base System  Mg0 Base System  Mg1 Base System  Mg0 Base System  Mg1 Base System  Mg2 Base System  Ng3 Base System  Ng4 Base System  Ng5 Base System  Ng6 Base System  Ng7 Base System  Ng8 Base System  Ng9 Base System  Scrubber  tn 0.2  Na Base System  Scrubber  tn 0.2  Na Base System  Scrubber  tn 0.2  Na Base System  Scrubber  tn 0.1  Calcium Base System	Scrubber			tn	0.1			5.5		H <sub>2</sub> S	0.1
Merc   0.1	Lime Kiln									METO	0.15
Scrubber or ESP	Uncontrolle	d		tn	28.	0.15		0.05		_	0.25
Miscellaneous Sources tn Merc 0.25  Sulfite Pulping Digester Blow Pit or Dump Tank Uncontrolled tn 335. Mg0 Base System Process Changes tn 2.0 Scrubber tn 0.5 Process Changes+Scrubber tn 0.1 All Exhausts through Recovery Systems tn 0.0 NH3 Base System Process Changes+Scrubber tn 0.2 Na Base System Process Changes+Scrubber tn 0.2 Na Base System Process Changes+Scrubber tn 1. Calcium Base System tn 33.5 Recovery System Mg0 Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5 NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5 Na Base System Sodium Carbonate Scrubber tn 2. 1. Acid Plant6 NH3 Base System Scrubber tn 0.2 Na Base System tn 0.2 Na Base System tn 0.2 Na Base System tn 0.1	Scrubber or	ESP		tn	0.25			0.05		H <sub>2</sub> S	0.25
Digester Blow Pit or Dump Tank Uncontrolled tn 335.  Mg0 Base System Process Changes tn 2.0 Scrubber tn 0.5 Process Changes+Scrubber tn 0.1 All Exhausts through Recovery Systems tn 0.0  NH3 Base System Process Changes+Scrubber tn 0.2  Na Base System Process Changes+Scrubber tn 0.2  Na Base System Process Changes+Scrubber tn 1. Calcium Base System tn 33.5  Recovery System Mg0 Base System Mg0 Base System Multicyclone+Venturi Scrub tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant6  NH3 Base System Scrubber tn 0.2  Na Base System Scrubber tn 0.2  Na Base System Scrubber tn 0.1 Calcium Base System	Miscellaneous Sou	rces		tn							0.25
Uncontrolled tn 335.  Mg0 Base System  Process Changes tn 2.0  Scrubber tn 0.5  Process Changes+Scrubber tn 0.1  All Exhausts through  Recovery Systems tn 0.0  NH3 Base System  Process Changes+Scrubber tn 0.2  Na Base System  Process Changes+Scrubber tn 0.2  Na Base System  Process Changes+Scrubber tn 1.  Calcium Base System tn 33.5  Recovery System  Mg0 Base System  Mg0 Base System  Multicyclone+Venturi Scrub tn 1. 4.5 0.5  NH3 Base System  NH3 Absorption+Mist Elim tn 0.35 3.5  Na Base System  Sodium Carbonate Scrubber tn 2. 1.  Acid Plant6  NH3 Base System  Scrubber tn 0.2  Na Base System  Scrubber tn 0.2  Na Base System  Scrubber tn 0.1  Calcium Base System	Sulfite Pulping										
MgO Base System       2.0         Process Changes       tn       2.0         Scrubber       tn       0.5         Process Changes+Scrubber       tn       0.1         All Exhausts through       Recovery Systems       tn       0.0         NH3 Base System       tn       0.2         Process Changes       tn       12.5         Process Changes+Scrubber       tn       0.2         Na Base System       tn       1.         Calcium Base System       tn       33.5         Recovery System       MgO Base System       tn       1.4.5       0.5         NH3 Base System       tn       0.35       3.5         NB Base System       tn       0.35       3.5         Na Base System       tn       2.1         Acid Plant 6       NH3 Base System       tn       0.2         Na Base System       tn       0.2         Na Base System       tn       0.1         Calcium Base System       tn       0.1         Calcium Base System       tn       0.1	Digester Blow Pit	or Dump Tank									
Process Changes Scrubber Scrubber Process Changes+Scrubber All Exhausts through Recovery Systems Process Changes Process Changes Process Changes Process Changes Process Changes Process Changes Process Changes+Scrubber Process Changes Proces	Uncontrolled			tn	3	35.					
Scrubber tn 0.5 Process Changes+Scrubber tn 0.1 All Exhausts through Recovery Systems tn 0.0 NH3 Base System Process Changes tn 12.5 Process Changes+Scrubber tn 0.2 Na Base System Process Changes+Scrubber tn 1. Calcium Base System tn 33.5 Recovery System MgO Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5 NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5 Na Base System Sodium Carbonate Scrubber tn 2. 1. Acid Plant6 NH3 Base System Scrubber tn 0.2 Na Base System Scrubber tn 0.1 Calcium Base System	MgO Base System	म									
Process Changes+Scrubber All Exhausts through Recovery Systems The content of the	Process Char	nges		tn		2.0					
All Exhausts through Recovery Systems tn 0.0  NH3 Base System Process Changes tn 12.5 Process Changes+Scrubber tn 0.2  Na Base System Process Changes+Scrubber tn 1.  Calcium Base System tn 33.5  Recovery System Mg0 Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant6  NH3 Base System Scrubber tn 0.2  Na Base System Scrubber tn 0.2  Na Base System Scrubber tn 0.1  Calcium Base System	Scrubber			tn		0.5					
Recovery Systems tn 0.0  NH3 Base System Process Changes tn 12.5 Process Changes+Scrubber tn 0.2  Na Base System Process Changes+Scrubber tn 1.  Calcium Base System tn 33.5  Recovery System MgO Base System Multicyclone+Venturi Scrub tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant6  NH3 Base System Scrubber tn 0.2  Na Base System Calcium Base System NH3 Base System Scrubber tn 0.1  Calcium Base System	Process Cha	nges+Scrubber		tn		0.1					
NH3 Base System Process Changes Process Changes+Scrubber Tn 1.  Calcium Base System Mg0 Base System Mg0 Base System Multicyclone+Venturi Scrub. Tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim. NH3 Absorption+Mist Elim. Tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber Tn 2. 1.  Acid Plant6  NH3 Base System Scrubber Tn 0.2  Na Base System Th 0.2  Na Base System Th 0.1  Calcium Base System Th 0.1  Calcium Base System	All Exhaust:	s through									
Process Changes tn 12.5 Process Changes+Scrubber tn 0.2 Na Base System Process Changes+Scrubber tn 1. Calcium Base System tn 33.5 Recovery System MgO Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5 NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5 Na Base System Sodium Carbonate Scrubber tn 2. 1. Acid Plant <sup>6</sup> NH3 Base System Scrubber tn 0.2 Na Base System Calcium Base System Calcium Base System	Rec	overy Systems		tn		0.0					
Process Changes+Scrubber tn 0.2  Na Base System Process Changes+Scrubber tn 1.  Calcium Base System tn 33.5  Recovery System MgO Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant6  NH3 Base System Scrubber tn 0.2  Na Base System Calcium Base System  NH3 Base System Scrubber tn 0.1  Calcium Base System	NH <sub>3</sub> Base System	m									
Na Base System Process Changes+Scrubber tn 1. Calcium Base System tn 33.5  Recovery System MgO Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant 6  NH3 Base System Scrubber tn 0.2  Na Base System Calcium Base System  Calcium Base System	Process Chai	nges		tn		12.5					
Na Base System Process Changes+Scrubber tn 1. Calcium Base System tn 33.5  Recovery System MgO Base System Multicyclone+Venturi Scrub. tn 1. 4.5 0.5  NH3 Base System NH3 Absorption+Mist Elim. tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant 6  NH3 Base System Scrubber tn 0.2  Na Base System Calcium Base System  Calcium Base System	Process Chai	nges+Scrubber		tn		0.2					
Calcium Base System  Recovery System  MgO Base System  Multicyclone+Venturi Scrub.  NH3 Base System  NH3 Absorption+Mist Elim.  NB Base System  Sodium Carbonate Scrubber  Acid Plant6  NH3 Base System  Scrubber  Scrubber  Th 0.2  Na Base System  Calcium Base System  Th 0.2  Na Base System  Th 0.2  Na Base System  Th 0.2  Na Base System  Th 0.1  Calcium Base System											
Recovery System  MgO Base System  Multicyclone+Venturi Scrub.  NH <sub>3</sub> Base System  NH <sub>3</sub> Absorption+Mist Elim.  Na Base System  Sodium Carbonate Scrubber  Acid Plant <sup>6</sup> NH <sub>3</sub> Base System  Scrubber  The O.2  Na Base System  Calcium Base System	Process Chai	nges+Scrubber		ţn		1.					
Recovery System  MgO Base System  Multicyclone+Venturi Scrub.  NH <sub>3</sub> Base System  NH <sub>3</sub> Absorption+Mist Elim.  Na Base System  Sodium Carbonate Scrubber  Acid Plant <sup>6</sup> NH <sub>3</sub> Base System  Scrubber  The O.2  Na Base System  Calcium Base System	Calcium Base S	ystem		tn		33.5					
Multicyclone+Venturi Scrub. tn 1, 4.5 0.5  NH <sub>3</sub> Base System  NH <sub>3</sub> Absorption+Mist Elim. tn 0.35 3.5  Na Base System  Sodium Carbonate Scrubber tn 2, 1.  Acid Plant <sup>6</sup> NH <sub>3</sub> Base System  Scrubber tn 0.2  Na Base System tn 0.1  Calcium Base System	Recovery System										
NH <sub>3</sub> Base System  NH <sub>3</sub> Absorption+Mist Elim. tn 0.35 3.5  Na Base System  Sodium Carbonate Scrubber tn 2. 1.  Acid Plant <sup>6</sup> NH <sub>3</sub> Base System  Scrubber tn 0.2  Na Base System tn 0.1  Calcium Base System	MgO Base System	TI									
NH <sub>3</sub> Absorption+Mist Elim. tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant <sup>6</sup> NH <sub>3</sub> Base System Scrubber tn 0.2  Na Base System tn 0.1  Calcium Base System	Multicyclone	e+Venturi Scrub.		tn	1.	4.5	0.5				
NH <sub>3</sub> Absorption+Mist Elim. tn 0.35 3.5  Na Base System Sodium Carbonate Scrubber tn 2. 1.  Acid Plant <sup>6</sup> NH <sub>3</sub> Base System Scrubber tn 0.2  Na Base System tn 0.1  Calcium Base System	NH <sub>3</sub> Base System	п									
Na Base System Sodium Carbonate Scrubber tn 2. I. Acid Plant <sup>6</sup> NH <sub>3</sub> Base System Scrubber tn 0.2 Na Base System tn 0.1 Calcium Base System				tn	0.35	3.5					
Acid Plant <sup>6</sup> NH <sub>3</sub> Base System  Scrubber tn 0.2  Na Base System tn 0.1  Calcium Base System											
Scrubber tn 0.2 Na Base System tn 0.1 Calcium Base System		onate Scrubber		tn	2.	1.					
Scrubber tn 0.2 Na Base System tn 0.1 Calcium Base System	NH₃ Base System	ग									
Na Base System tn 0.1 Calcium Base System				tn		0.2					
Calcium Base System											
A 11											
		-		tn		4.					

<sup>6.</sup> Necessary in pulp mills with insufficient or nonexistent recovery systems.

IC#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/U	<b>VOC</b> kg/U —————	kg/l
342	Printing and Publishing and Allie	d Industries					,	
	Graphic Arts							
	Small Applications 7	(Capita)*(year)					0.4	
	Major Printing Lines <sup>8</sup>							
	Web Offset							
	Publications							
	Printing Line							
	Uncontrolled	tn of ink					240	
	Incineration	tn of ink					12	
	Printed Product	tn of ink					160	
	Newspapers							
	Printed Product	tn of ink					50	
	Web Letterpress							
	Publications							
	Printing Line							
	Uncontrolled	tn of ink					240	
	Incineration	tn of ink					12	
	Printed Product	tπ of ink					160	
	Newspapers	tn of ink					Q	
	Rotogravure							
	Printing Line							
	Uncontrolled	tn of ink					712	
	Carbon Adsorption	tn of ink					230	
	Incineration	tn of ink					249	
	Printed Product	tn of ink					38	
	Flexography							
	Printing Line							
	Uncontrolled	tn of ink					712	
	Carbon Adsorption	tn of ink					285	
	Incineration	tn of ink					285	
	Printed Product	tn of ink					38	
	Publication Gravure Printing <sup>9</sup>							
	Uncontrolled	tn of ink					1480	
	Controlled (Old Presses)	tn of ink					370	
	Controlled (New Presses)	tn of ink					220	

<sup>7. (</sup>a) Large sources contribute most of the emissions for graphic arts operations.

<sup>(</sup>b) The listed factor is expressed in kg/year/capita, it provides an overall estimate for the numerous small sources which are difficult to be identified separately, and can be used only in the case of developed countries.

<sup>8.</sup> The VOC emission factors for the plant operations (dryer and other print-line components) are listed separately from these for the printed product, as the former are subject to controls.

<sup>9. (</sup>a) Control devices can be of the solvent recovery (carbon adsorption) and of the solvent destruction type (thermal or catalytic exidation) type, the former being more common.

<sup>(</sup>b) The 75% overall control level represents 84% capture efficiency and 90% control efficiency (the U.S. EPA guideline recommendation for old existing presses). The 85% overall control level represents the Best Demonstrated Control Technology for new plants.

# $\label{thm:model} \mbox{Model for Air Emission Inventories and Controls - Cont'd}$

1				
SIC#	PROCESS	UNIT (U) TSP SO <sub>2</sub> NO <sub>x</sub> CO	VOC	
		kg/U kg/Ū kg/U kg/U	kg/U	kg/U

### DIVISION 35. MANUFACTURE OF CHEMICALS & OF CHEMICAL, PETROLEUM, COAL, RUBBER & PLASTIC PRODUCTS

#### 351 Manufacture of Industrial Chemical

#### 3511 Basic Industrial Chemicals Except Fertilizers

Phthalic Anhydride							
Oxidation of o-xylene Process							
Main Process Stream							
Uncontrolled	tn	69	4,7	151			
Scrubber & Incinerator	tn	3	4.7	6			
Incinerator	tn	4	4.7	8			
Incinerator+Steam Generator	tn	4	4.7	8			
Pretreatment							
Uncontrolled	tn	6.4					
Scrubber & Incinerator	tn	0.3					
Incinerator	tn	0.4					
Distillation							
Uncontrolled	tn	45.			1.2		
Scrubber & Incinerator	tn	2.			<0.1		
Incinerator	tn	2.			<0.1		
Oxidation of naphthalene							
Uncontrolled	tn	28.		50			
Incinerator	tn	6.		10			
Scrubber	tn	0.3		50			
Pretreatment							
Uncontrolled	tn	2.5					
Incinerator	tn	0.5					
Scrubber	tn	0.1					
Distillation							
Uncontrolled	tn	19.			5		
Incinerator	tn	2.			1		
Scrubber	tn	0.2			<0.1		
Chlor-Alkali Production							
Mercury Cell Process							
Air Blowing the Cell Brine	tn					C1 <sub>2</sub>	2.5
Blow Gases from Liquefaction							
Uncontrolled	tn					¢١ <sub>2</sub>	50
Water Absorber	ţn					$c_{12}$	5
Caustic or Lime Absorber	tn					C1 <sub>2</sub>	0.5
Loading of Chlorine							
Storage & Tank Car Vents	tn					¢1 <sub>2</sub>	8.25
Diaphragm Cell Process							
Blow Gases from Liquefaction							
Uncontrolled	tn					c1 <sub>2</sub>	30
Water Absorber	tn					c1 <sub>2</sub>	3
Caustic or Lime Absorber	ŧn					C1 <sub>2</sub>	0.5

Model for Air Emission Inventories and Controls - Cont'd

<b>:#</b>	PROCESS	UNIT (U)	TSP kg/U	50 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U ——	VOC kg/U		kg/U
	Loading of Chlorine								
	Storage & Tank Car Vents	tn						c۱ <sub>2</sub>	8.25
ļ	Hydrochloric Acid (by-product prod	cess10							
	Uncontrolled	tn						HC 1	3.0
	Final Scrubber	tn						HC 1	0.2
1	Hydrofluoric Acid from fluorospar	& H <sub>2</sub> SO <sub>4</sub>							
	Spar drying, transfer & silos	<b>4</b>							
	Uncontrolled	tn	70.5						
	FFs. Covers, Additives	tn	1.3						
	Tail Gas								
	Uncontrolled	tn		22.5				HF	13
	511551171511754							\$iF4	15.0
	Caustic Scrubber	tn		0.3				HF	0.1
	0000010 0010000							SiF4	0.1
	Sulfuric Acid <sup>11</sup>								
	Without Acid Mist Controls								
	From Recovered S	tn of 100% H <sub>2</sub> SO <sub>4</sub>	;	7(100-6	e)			$so_3$	0.29
	From Bright Virgin S	tn of 100% H <sub>2</sub> SO <sub>4</sub>		7(100-				SO <sub>3</sub>	0.8
	From Dark Virgin S	tn of 100% H <sub>2</sub> SO <sub>4</sub>		7(100-				$SO_3$	1.6
	Sulfide Ores	tn of 100% H <sub>2</sub> \$0 <sub>4</sub>		7(100-c				so <sub>3</sub>	2.1
	Spent Acid	tn of 100% H <sub>2</sub> SO <sub>4</sub>		7(100-				s0 <sub>3</sub>	1.1
	ESP or Mist Eliminator	tn of 100% H <sub>2</sub> SO <sub>4</sub>		7(100-				\$0 <sub>3</sub>	0.0
	Nitric Acid from Catalytic oxidat	ion of NH <sub>2</sub>							
	Weak Acid Tail Gas	<b>V</b>							
	Uncontrolled	tn of 100% acid			22.0				
	Catalytic NO <sub>x</sub> Reduction								
	with Natural Gas	tn of 100% acid			0.2				
	with Hydrogen	tn of 100% acid			0.4				
	with 25% NG 75% H <sub>2</sub>	tn of 100% acid			0.5				
	Extended Absorption	tn of 100% acid			1.0				
	High Strength Acid Plant	tn of 100% acid			5.0				
	Phosphoric Acid								
	Wet Process <sup>12</sup>								
	Uncontrolled	tn of P <sub>2</sub> 0 <sub>5</sub>	5.5 <sup>13</sup>					۴ <sub>2</sub>	59.
	Controlled	tn of P <sub>2</sub> O <sub>5</sub>	3.0					F <sub>2</sub>	0.

<sup>10.</sup> With chlorine added to an organic compound such as benzene, toluene and vinyl chloride.

<sup>11. &</sup>quot;e" is the process conversion efficiency of  $SO_2$  into  $SO_3$ . Typical values for single absorption plants are 95 to 98% and for double absorption plants about 99.7%. For single absorption plants equipped with alkaline  $SO_2$  absorbers, a value of 99.7% should be also used.

<sup>12.</sup> The wet process is used predominantly in the production of fertilizers.

Phosphate rock is assumed to be delivered dried or calcined to the plant. If drying or calcining takes place, the added TSP emissions must be computed (see SIC No 2902).

Model for Air Emission Inventories and Controls - Cont'd

PROCESS	UNIT (U)	TSP kg/U ——	50 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	00 kg/U	VOC kg/U		kg/U
Thermal Process								
Controlled	tn of $P_2O_5$	1.0						
Lead Oxide & Inorganic Pigments								
Lead Oxide Production								
Barton Pot (After FF)	tn	0.32					РЬ	0.22
Calcining Furnace								
Uncontrolled	tn	7					РЬ	7.6
Scrubber	tn	1.23					Pb	1.23
Cyclone + FF	tn	0.07					Pb	0.07
Pigment Production							1	0.07
Red Lead								
Uncontrolled	tn	0.5					Pb	0.5
Scrubber	tn	0.088					Pb	0.088
Cyclone + FF	tn	0.005					Рb	0.005
White Lead								0.000
Uncontrolled	tп	0.28					РЬ	0.28
Scrubber	tn	0.05					Pb	0.05
Cyclone + FF	tn						РЬ	0.003
Chrome Pigments Production							,	*
Uncontrolled	tn	0.065					Pb	0.065
Scrubber		0.011					Pb	0.011
Cyclone + FF		0.001					Pb	0.001
Ammonia Production <sup>14</sup>								
With Natural Gas as Fuel	tn	0.072	0 022	2 7	7.97	4.73	NH <sub>3</sub>	2.1
With Distillate Oil as Fuel	tn	0.450			8.02	4.94	NH <sub>3</sub>	2.1
Sodium Carbonate (Soda Ash) Production								
Natural Process (Recovery from natur		5						
Predryer - Rotary steam heated	, ,							
Uncontrolled	tn	1.55						
Venturi Scrubber	tn	0.03						
Calciner								
Gas Fired - Uncontrolled	tn	184						
Coal Fired - Uncontrolled	tn		0.007					
Cyclone & ESP		.975-0,						
Bleacher - Rotary gas fired	2.1.2							
Uncontrolled	tn	155						
Cyclone & ESP	tn	0.02						

<sup>14.</sup> The natural gas feedstock is assumed to be desulfurized. If natural gas desulfurization takes place, the additional  $SO_2$  emissions need to be considered (see SIC No 2200). Loading of storage tanks and ships may be an additional source of significant  $NH_3$  emissions if proper controls are not applied.

<sup>15.</sup> Significant TSP emissions, which may arise from crushing and dissolving operations, elevators, conveyor transfer points, product loading and storage piles, have not been included.

Model for Air Emission Inventories and Controls - Cont'd

IC# PROCESS U	NIT (U)	TSP kg/U	SO <sub>2</sub> kg/V	NO <sub>x</sub> kg/U	CO kg/U ——	<b>VOC</b> kg/U		kg/U
Dryer								
Rotary steam tube								
Uncontrolled	tn	33						
Venturi Scrubber	tr	0.4						
Fluid bed steam tube								
Uncontrolled	tn	73						
Cyclone+Venturi Scrubber	tr	0.09						
Synthetic (Solvay) Process <sup>16</sup>								
Uncontrolled	tn	25					$NH_3$	2
Controlled	tr	0.25						
Calcium Carbide Production17								
Coke Dryer								
Uncontrolled	tn	1.	1.5					
Controlled	tn	0.13	1.5					
Electric Furnace								
Circular Charging Conveyor								
Controlled	tn	0.17						
Furnace Main Stack								
Uncontrolled	tr	12.	1.5					
Controlled	tr	0.39	1.5					
Tap fume vents								
Controlled	tn	0.07						
Furnace Room vents								
Uncontrolled	tr	13.						
Controlled	tr	0.07						
Primary and Secondary Product Crushing								
Controlled	tn	0.57						
Adipic Acid (from cyclohexane or cyclohexano	1)							
Raw Material Storage	tn					3.3		
Cyclohexane Oxidation								
Uncontrolled (after scrubber)	tn				58	20		
Carbon Adsorber	tr				58	1		
Flaring	tr				Ź	6		
CO boiler	tn				0.5	0.0		
Thermal Incinerator	tn				0.0	0.0		
Nitric Acid Reaction								
Uncont'led (after $NO_{ imes}$ absorber)	tr			27				
Scrubber, Flaring or Combustion	tr			8				
Thermal Reduction 18	tr			0.5				

<sup>16.</sup> Significant fugitive TSP emissions from limestone handling and processing operations, product drying operations, and dry solids handling (conveyance and bulk loading) have not been included.

Controls devices for TSP used are Fabric Filters of Wet Scrubbers. The CO generated from 17. closed furnaces is either used as fuel for other processes of Flared.

In the thermal reduction, the offgases containing the  $\mathrm{NO}_{\mathrm{X}}$  are reacted with excess fuel in a 18. reducing atmosphere.

Model for Air Emission Inventories and Controls - Cont'd

I SIC#P	ROCESS	UNIT	(U)	T\$P kg/U	\$0 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/U	VOC kg/U		kg/ប
	Refining, Drying, Cooling, Storing									
	Controlled (Fabric Filter)		tn	0.5		0.3		0.3		
Lea	d Alkyl Manufacture									
	Electrolytic Process		tn						Рb	0.5
	Sodium/Lead Alloy Process									
	Process Vents									
	Tetraethyl Lead Production									
	Uncontrolled		tn						PЬ	2.0
	Low Energy Wet Scrubber		tn						Рb	0.25
	High Energy Wet Scrubber		tn						Рb	0.06
	Fabric Filter		tn						Рþ	0.02
	Tetramethyl Lead Production									
	Uncontrolled		tn						Pb	75.0
	Low Energy Wet Scrubber		tn						Pb	9.4
	High Energy Wet Scrubber		tn						Рb	2.25
	Fabric Filter		tn						Pb	0.75
	Sludge Pits									
	Uncontrolled		tn						Pb	0.6
	Low Energy Wet Scrubber		tn						Pb	0.08
	High Energy Wet Scrubber		tn						Pb	0.002
	Fabric Filter		tn						Pb	0.001
	Recovery Furnace									
	Uncontrolled		tn						РЬ	28.0
	Low Energy Wet Scrubber		tn						Pb	3.5
	High Energy Wet Scrubber		tn						Pb	0.84
	Fabric Filter		tn						Pb	0.28
Ma	leic Anhydride by Oxidation of Benzene									
	Uncontrolled		tn				680	87		
	Carbon Adsorption		tn				680	87		
	Thermal or Catalytic Incineration		tn				3.4	0.4		
Ter	rephthalic Acid									
	Uncontrolled		tn				19	19.8		
	Carbon Adsorption		tn				19	2.0		
	Thermal Oxidation		tn				1.0	1.0		
3512 Mar	nufacture of Fertilizers and Pesticides	;								
Ure	ea Production (from NH <sub>3</sub> & CO <sub>2</sub> ) <sup>19</sup>									
	Solution Formation & Concentration									
	(1,, -4,11-4		4	0.0105					NH.	9 12

<sup>19.</sup> Emission sources are generally controlled with wet scrubbers due to easy recycling of the dissolved Urea collected. Emissions from the bagging operations are controlled by Fabric Filters. Emissions from the solution synthesis and concentration operations, from the solids screening and coating are small and are generally not controlled.

Uncontrolled

tn 0.0105

NH<sub>3</sub> 9.12

Model for Air Emission Inventories and Controls - Cont'd

# PROCESS	(U) TINU	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U ——		kg/L
Solids Formation								
Non Fluidized Bed Prilling								
Uncontrolled	tn	1.85					$NH_3$	0.43
Wet Scrubber	tn	0.032					NH <sub>3</sub>	0.43
Fluidized Bed Prilling								
Agricultural Grade								
Uncontrolled	tn	3.1					NH <sub>3</sub>	1.46
Wet Scrubber	tπ	0.39					NH <sub>3</sub>	1.46
Animal Feed Grade								
Uncontrolled	tn	1.8					$NH_3$	2.07
Wet Scrubber	tn	0.24					NH <sub>3</sub>	1.04
Drum Granulator								
Uncontrolled	tn	120.					NΗ <sub>3</sub>	1.07
Wet Scrubber	tn	0.115					NНЗ	1.07
Rotary Drum Cooler <sup>20</sup>								
Uncontrolled	tn	3.72					NH <sub>3</sub> 0	. 0256
Wet Scrubber	tn	0.1						
Bagging - Uncontrolled	tn	0.095						
Ammonium Nitrate (from HNO <sub>3</sub> & NH <sub>3</sub> ) High Density Prilling Process								
Uncontrolled	tn	5.8					ин <sub>3</sub> нио <sub>3</sub>	37.8 0.52
Wet Scrubbing	tn	0.74					3	
Low Density Prilling Process								
Uncontrolled	tn	86.9					NH <sub>3</sub> HNO <sub>3</sub>	18.8 0.52
Wet Scrubbing	tn	1.2					J	
Rotary Drum Granulator Process								
Uncontrolled	tn	157.5					NH <sub>3</sub>	48
							HNO <sub>3</sub>	0.52
Wet Scrubbing	tn	0.43						
Pan Granulators Process								
Uncontrolled	tn	23.1					NH <sub>3</sub>	17.8 0.52
Wet Scrubbing	tn	0.33					HNO <sub>3</sub>	υ. υ.
Ammonium Sulfate <sup>21</sup>								
Rotary Driers								
Uncontrolled	tn	23.00				0.74		
Wet Scrubbers	tn	0.12				0.11		
Fluidized Bed Dryers								
Uncontrolled	tn	109.00				0.74		
Wet Scrubbers	tn					0.11		

Required only for Pan granulation and for some agricultural grade prills. 20.

Produced as a caprolactam By-product, as a coke oven By-product, or synthetically by reacting 21. ammonia with sulfuric acid.

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS -	UNIT	(U)	TSP kg/U	80 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/U	VOC kg/U		, kg/U 
	Ammonium Phosphates (from H <sub>3</sub> PO <sub>4</sub> & Anhydrou Controlled	ıs NH <sub>3</sub>	tn	0.15					F <sub>2</sub> NH <sub>3</sub>	0.04 0.07
									3	0.07
	Normal Superphosphates (from Phosphate roo	k & F	1 <sub>2</sub> SO <sub>4</sub> )							
	Controlled to d	of Pro	duct	0.76					F <sub>2</sub>	0.36
	tn of P <sub>2</sub> (	) <sub>5</sub> cor	tent	4.20					F <sub>2</sub>	2
	Triple Superphosphates (from Phosphate Roc Run-of-the-Pile	:k & F	1 <sub>3</sub> P0 <sub>4</sub> )	22						
	Controlled the	of Pro	duct	0.04					F <sub>2</sub>	0.04
	tn of P <sub>2</sub> (	) <sub>S</sub> cor	itent	0.10					F <sub>2</sub>	0.1
	Granular	-							•	
	Controlled the	of Pro	duct	0.10					F <sub>2</sub>	0,056
	tn of P <sub>2</sub> (	5 cor	ntent	0.26					F <sub>2</sub>	0.14

3513 Manufacture of Synthetic Resins, Plastic Materials and Man-Made Fibbers Except Glass

Styrene-Butadiene Copolymer (Rubber)		
Emulsion Crumb Product		
Monomer Recovery		
Uncontrolled	tn	2.6
Absorber or Flaring	tn	0.26
Blend/Coagulation Tank & Dryers	tn	2.93
Emulsion Latex Product	tn	8.55
Polypropylene & Copolymers		
Uncontrolied	tn 1.5	0.35
Vapor Recovery and/or Flares	tn 0.2	0.03
Polyvinyl Chlorides & Copolymers		
Uncontrolled	tn 17.5	8.5
Vapor Recovery and/or Flares	tn 1.7	0.8
Rayon Manufacturing - Viscose Process	tn	H <sub>2</sub> S 50.4
		CS <sub>2</sub> 251
Cellulose Acetate, Filter Tow	tn	112
Cellulose Acetate & Triacetate (yarn)	tn	199

<sup>22. (</sup>a) Emissions from the reactor, den and granulator are controlled by scrubbers using recycled gypsum pond water.

<sup>(</sup>b) Emissions from the dryer, cooler, screens, mills, product transfer systems & storage buildings are controlled by cyclones for the removal of dust, before they are sent to wet scrubbers.

<sup>(</sup>c) Fabric Filters are used in the preliminary ground rock handling activities.

Model for Air Emission Inventories and Controls - Cont'd

IC∌	PROCESS	UN1 	IT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U	kg/
	Polyesters (e.g. Dacron), Melt S	Snun							
	Staple		tn	25.2			,	0.6	
	Yarn		tn	0.03				0.05	
	Acrylic, Dry Spun							•	
•	Uncontrolled		tn					40	
	Controlled <sup>23</sup>		tn					32	
	Modacrylic, Dry Span		tn					125	
	Acrylic and Modacrylic, Wet Spun	<b>.</b>	tn		•			6.75	•
	Acrylic, Inorganic Wet Spun				1				
	Homopolymer								
	Capolymer Capolymer		tn					20.7	
	copo (Aust.		tn			-	•	2.75	•
	Nylon 6, Melt Spun								
	Staple		tn	0.01				3.93	
	Yarn	٠	tn		•	•		0.45	
	Nylon 66, Melt Spun						:		
	Uncontrolled		tn	0.5				2.13	
	Catalytic Incinerators etc		tn	0.1				0.31	
	Polyolefin, Melt Spun		tn	0.01		,		5	
	Spandex (polyurethane fibber)								
	Dry Spun		tn					4.23	
	Reaction Spun		tn					138	
,	Vinyon, Dry Spun	v ,	tn					150	
		:						:	
52	Manufacture of Other Chemical Pro	oducts					,	•	
521	Manufacture of Paints. Varnishes	and Lacquere						,	
		wile rechaely							
ı	Paint Manufacture								
	Uncontrolled		tn	10.0				15	
	Afterburners	. *	tn.	1.0		,		0.15	
,	Varnish Manufacture								
,						1			
	Uncontrolled Afterburners	•	tn				•	185	
			tn					1.9	

Scrubbers and Condensers are used in the spinning cells and in the dryers. Carbon adsorption 23. is used in tank vents and in mixing and filtering operations. Distillation columns are also used to recover solvent from condenser, scrubber and wash water.

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS	UNIT (	U) 	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U		kg/U
3523	Manufacture of Soap and Cleaning Prepa	rations								
	Spray-Dried Detergents									
	Uncontrolled	1	tn	45.0						
	Cyclones	1	tn	7.0						
	Cyclones & Spray chamber	1	tn	3.5						
	Cyclones & Packed Scrubber	1	tn	2.5						
	Cyclones & Venturi Scrubber	1	tn	1.5						
	Cyclones & Wet Scrubber	•	tn	0.544						
	Cyclones & Wet Scrubber & ESP	•	tn	0.023						
3529	Manufacture of Chemical Products not E	lsewhere Cla	ass	ified						
	Carbon Black									
	Main Process Vent									
	0il Furnace Process									
	Uncontrolled		tn	3.27	0.0	0.28	1400	75	H <sub>2</sub> S	30
	Flare		tn	1.35	25.0		122.	1.85	H <sub>2</sub> S	1.0
	CO Boiler & Incinerator		tn	1.04	17.5	4.65	0.88	0.99	H <sub>2</sub> S	0.11
	Thermal Process		tn	O.	٥.		0.	٥.	_	
	All Other Systems									
	Fabric Filters		tn	0.37	0.27	0.4	0.	0.73		
	Printing Ink									
	Uncontrolled		tn	1.0				235		
	Scrubber/Condenser & Afterburner		tn				•	23.5		
	Trinitrotoluene									
	Batch Process									
	Nitration Reactors									
	With Fume Recovery		tn			12.5			HNO <sub>3</sub>	0.5
	With Acid Recovery		tn			27.5			ниоз	46.0
	Nitric Acid Concentrators		tn			18.5			so <sub>3</sub>	3.7
	Sulfuric Acid Concentrators									
	ESP		tn		7.	20.			so <sub>3</sub>	26.
	ESP & Scrubber		ŧπ		0.	20.			so <sub>3</sub>	1
	Red Water Incinerator									
	Uncontrolled		tn	12.5		13.				
	Wet Scrubber		tn	0.5	1.	2.5				
	Sellite Exhaust		tn		29.5				so <sub>3</sub>	2.4
	Continuous Process									
	With Fume Recovery		tn	0.13		7.5			HNO <sub>3</sub>	
	With Acid Recovery		tn	0.13	0.12	5.0			HNO <sub>3</sub>	0.0
	Nitrocellulose		tn		34.7	14.			нио <sub>з</sub> so <sub>3</sub>	19.0 0.24

SIC#	the state of the s	UNIT (U)	TSP SO <sub>2</sub> NO <sub>x</sub> kg/U kg/U kg/U		
•	er e				
353	Petro leum Refineries				
	No. 2	•			
	Petroleum Refining <sup>24</sup>				
	Misc Operations <sup>25</sup>	m <sup>3</sup> of crude			0.4
	Fluid Catalytic Cracking (FC	C)			0.4
	Uncontrolled		0.695 1.413 0.204	39.2	0.63
	CO Boiler	m <sup>3</sup> of FCC feed	0.695 1.413 0.204	00.	0.00
	ESP.18 CO Boiler	m <sup>3</sup> of FCC feed	0.126 1.413 0.204		
	Desulfürization of				
	Sour Gas <b>26</b>	kg of Sulfur in Gas	2(100-e)/100		
	64 0 <b>kg</b>	of Sulfur Recovered			
	Rail Tank & Tank Trucks Fill		-,,,-		
	Gasoline Loading		to the production		٠.
	Splash Loading	m <sup>3</sup> of Gasoline			1.43
		tn of Gasoline	•		1.94
	Submerged Loading <sup>27</sup>	•			,
	** Normal Service (B)	m <sup>3</sup> of Gasoline			0.59
	91 1. P. 92 184.	tn of Gasoline			0.80
	Vapor Balance Serv	m <sup>3</sup> of Gasoline			0.98
	was the first state of the	tn of Gasoline			1.33
	*Vapor Controlled (* )	m <sup>3</sup> of Gasoline			0705
	7.54	th of Gasoline		•	0.07
	Jet Naphtha Loading $\mathbb{R}^n$			•	
	'Splash' Loading 💎 💥 🔻	m <sup>3</sup> of Gasoline			0.43
	51 - 1 - 2. St.	tn of Gasoline			0.58
	Submerged Loading	_		* ;	, 41
	Normal Service	m <sup>3</sup> of Naphtha			0.18
		tn of Naphtha			0.24
	Vapor Balance Serv	m <sup>3</sup> of Naphtha			0.30
		tn of Naphtha	4	41	0.40 -
	Loading of Barges	_			
	Gasoline	m <sup>3</sup> of Gasoline		.`	0.41
		tn of Gasoline			0.55

Emissions due to fuel burning are not accounted for and should be computed separately (see 24. SIC No 410).

<sup>25.</sup> VOC emissions from typical sources within a refinery, such as storage tanks, API separators, blowdowns, fugitive sources etc are included. The listed factor is based on detailed VOC emissions estimates in several refineries.

<sup>&</sup>quot;e" is the percent efficiency of the sulfur recovery plant. Typical values are for 2-stage plant controlled 92-95%, for 3-stage plant uncontrolled 95-97.5%, 4-stage plant uncontrolled 96-99%, and for controlled plant 99-99.9%.

In the Vapor Balance Service the cargo truck retrieves the vapors displaced during the underground tank filling in service stations (see below, SIC 620). This operation increases the VOC concentration in the air within the empty truck and causes higher VOC emissions when the -0) truck is filled. It should be noted in this regard that most of the VOC emissions reduction achieved through the balanced vapor filling of the service stations submerged tanks is offset in by the mesultant increased emissions in the Truck Filling Station, unless of course a vapor recovery system is used in the latter. As the second and the second seco

**PROCESS** 

SIC#

Model for Air Emission Inventories and Controls - Cont'd

16#	PROCESS	_			kg/U	kg/U	kg/U	kg/U	kg/U	kg/
	Crude Oil	m3 ∩ F	C۳	ude Oil					0.12	
	crade off			ude Oil					0.137	
	Jet Naphtha	_		Naphtha					0.15	
	Jet Maphtha			Naphtha				,	0.20	
	Loading of Ships/Ocean Barges	<b>611</b>	Ψ'	ларпена						
	Gasoline	"3 o	F G	asoline					0.215	
	4440 ) (NE	-		asoline					0.291	
	Crude 011	_		ude Oil					0.073	
	Clude Oil			ude Oil					0.083	
	Jet Naphtha			Naphtha					0.06	
	oet napritiia			Naphtha					0.08	
54	Manufacture of Miscellaneous Produc	ts of	Pet	roleum a	nd Coal	I	•	•	•	
									,	
	Asphaltic Concrete Plants <sup>28</sup>			_						
	Conventional Hot-Mix (Batch & Co	nt inuo	Ų\$							
	Uncontrolled			tn	22.5				14	
	Precleaner			tn	7.5	1465	18	19		
	High Efficiency Cyclone			tn	0.85	1465	18		14	
	Spray Tower			tn	0.2	73\$	18			
	Baffle Spray Tower			tn	0.15	735	18			
	Multiple Centrifugal Scrubber	•		tn	0.035	73S	18	19		
	Orifice Scrubber			tn	0.02	73S	18		) 14	:
	Venturi Scrubber			tn	0.02	73S	18		14	
	Baghouse			tn	0.01	1465	18	19	3 14	
	Dryer Drum Hot Mix								:	
	Uncontrolled			tn	2.45					
	Cyclone or Multicyclone			tn	0.34					
	Low Energy Scrubber			tn	0.04		1000		**	
	Venturi Scrubber			tn	0.02					
	Asphalt Roofing <b>29</b>									
	Asphalt Blowing									
	Saturant									
	Uncontrolled			Aspha!t	3.6			0.14	4 0.73	
	Controlled	tn	of	Asphalt	0.25				0.015	
	Coating									
	Uncontrolled			Aspha lt	13.4			1.8		3.5
	Controlled	tn	of	Asphalt				0.	1	
	Shingle Saturation									
	Uncontrolled			Aspha 1t	1.57				3 0.13	
	T.		- #	Shingle	0.25			0.0	1 0.05	

UNIT (U)

50<sub>2</sub>

TSP

NO<sub>X</sub>

CO VOC

<sup>28. (</sup>a) "S" is the weight percent content of sulfur in the fuel oil used.

<sup>(</sup>b) Fugitive dust emissions are not included in the listed factors.

<sup>(</sup>c) Fuel burning emissions are included in Conventional but not in Drum Mix plants. (d) VOC emission factor for Drum Mix plans is not available.

<sup>29.</sup> Control devices include afterburners, high velocity air filters, low voltage ESP and wet scrubbers. Blowing operations are controlled by afterburners.

Model for Air Emission Inventories and Controls - Cont'd

I SIC#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	Ç0 kg/U	VOC kg/U		kg/U
	Controlled	tn of Shingle	0.03				0.09		
	Coke Production (By-product Method)	30							
	Coal Crushing								
	Cyc lone	tn of Coke	0.055						
	Coal Preheating <sup>31</sup>								
	Uncontrolled	tn of Coke	1.75						
	Scrubber	tn of Coke	0.125						
	Wet ESP	tn of Coke	0.006						
	Wet Coal Charging / Larry Car								
	Uncontrolled	tn of Cok¢	0.24	0.01	0.015	0.3	1.25	₩Нз	0.0
	Sequential Charging	tn of Coke	800.0						
	Scrubber	tn of Coke	0.007						
	Door Leak	tn of Coke	0.27	0.005	0.005	0.3	0.75	$NH_3$	0.0
	Coke Pushing								
	Uncontrolled	tn of Coke	0.58			0.035	0.1	NH <sub>3</sub>	0.0
	ESP	tn of Coke	0.225						
	Venturi Scrubber	tn of Coke	0.09						
	Baghouse	tn of Coke	0.045						
	Mobile Quench-Car Scrubber	tn of Coke	0.036						
	Coke Quenching								
	Quenching with Dirty Water (>	5000 m1/1 TDS)							
	Uncontrolled	tn of Coke	2.62						
	Baffles	tn of Coke	0.65						
	Quenching with Clean Water (>	1500 ml/l TDS)							
	Uncontrolled	tn of Coke	0.57						
	8affles	tn of Coke	0.27						
	Combustion of Coke Oven Gas			**					
	Uncontrolled	tn of Coke	0.234	2 32					

### DIVISION 36. MANUFACTURE OF NONMETALLIC MINERAL PRODUCTS EXCEPT PRODUCTS OF PETROLEUM & COKE

#### 362 Manufacture of Glass and Glass Products

36201 Glass and Glass Products<sup>33</sup> Melting Furnace Cor

ontainer Glass						
Uncontrolled	tn	0.7	1.7	3.1	0.1	0.1
Low Energy Scrubber	tn	0.4	0.9	3.1	0.1	0.1
Venturi Scrubber	tn	0.1	0.1	3.1	0.1	0.1
Fabric Filter or ESP	tn		1.7	3.1	0.1	0.1

One ton of bituminous coal yields approximately 0.7 tn of Coke and 280 to 350  $\mathrm{m}^3$  of gas. 30.

Coal preheating is used only in few plants. 31.

Typical  ${\rm SO_2}$  factor based on the assumptions of 0.8% S content of coal & on 33% of S transfer from coal to coke oven gas.

Emissions from the combustion of fuel are included. 33.

 ${\bf Model} \ \ {\bf for} \ \ {\bf Air} \ \ {\bf Emission} \ \ {\bf Inventories} \ \ {\bf and} \ \ {\bf Cont'd}$ 

SIC# PROCESS	UNIT (U)	TSP kg/ti	\$0 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	co kg/U	VOC kg/U		kg/U
Flat Glass								
Uncontrolled	tn	1.0	1.5	4.0	0.1	0.1		
Low Energy Scrubber	tn	0.5	0.8	4.0		0.1		
Venturi Scrubber	tn	0.5	0.1	4.0		0.1		
Fabric Filter or ESP	tn		1.5	4.0	0.1	0.1		
Pressed or Blown Glass	2		210	7.0	5,1	V.1		
Uncontrolled	tn	8.7	2.8	4.3	0.1	0.2		
Low Energy Scrubber	tn	4.2	1.3	4.3	0.1	0.2		
Venturi Scrubber	tn	0.5	0.1	4.3	0.1	0.2		
Fabric Filter or ESP	tn	0.1	2.8	4.3	0.1	0.2		
Forming and Finishing	LII	0.1	2.0	4.5	0.1	U.Z		
Container Glass	tn					4.4		
Pressed and Blown Glass	tn					4.5		
Glass Fibber Manufacture <sup>34</sup>								
Wool Glass Fibber (Uncontrolled)								
Raw Materials Handling	tn	1.9						
Glass Furnace	<b></b>	1.0						
Electric	tn	0.25	0.02	0.34	0.025		F	0.001
Gas-Regenerative	tn	11.	5.		0.13		F	0.001
Gas-Recuperative	tn	14.	5.		0.13		F	
Gas-Unit Melter	tn	4.5	0.3		0.13		F	0.06 0.06
Forming	tn	1.	0.5	0.13	0.15	0.15	r	0.00
Oven Curing (Flame attenuation)	tn	3.		1.	1.8	3.5		
Textile Glass Fibber (Uncontrolled)	L.I.	٠.		1.	1.0	3.5		
Raw Materials Handling	tn	1.9						
Glass Furnace	LII	1.9						
Gas-Regenerative	tn	1.	1.5	10.	0.25			
Gas-Recuperative	tn	8.	15.	10.	0.25			
Gas-Unit Melter	tn	3.	IJ.	10.	0.45			
Forming	tn	0.5		10.	U.4J			
Oven Curing and Cooling	tn	0.6		1 2	0.75			

#### 369 Manufacture of Other Non-Metallic Mineral Products

## 3691 Manufacture of Structural Clay Products

Bricks and Clay Products
Raw Materials Handling<sup>35</sup>

Drying

Uncontrolled	tn of material dried	35
Cyclone	tn of material dried	9.
Cyclone+Scrubber	tn of material dried	3.5

 <sup>(</sup>a) Emissions from the combustion of fuel are included.

<sup>(</sup>b) Control technologies employed include wet ESPs, low and high pressure drop wet scrubbers, low and high temperature thermal incinerators.

<sup>35.</sup> Because of process variations, some raw material handling steps may be partially or completely omitted.

SIC#	PROCESS	UN) TINU	T\$P kg/U				VOC kg/U		kg/V
	Grinding								
	Uncontrolled	tm of material ground	38.						
	Cyclone	th of material ground	9.5						
	Cyclone+Scrubber	tn of material ground	3.8						
	Storage	th of material ground	3.0						
	Uncontrolled	tn of material stored	17.						
	Cyclone	tn of material stored	4.						
	Cyclone+Scrubber	tn of material stored	1.7						
	Curing and Firing <sup>36</sup>	THE THE TOTAL STATE OF THE	,						
	Tunnel Kilns								
	Gas Fired	tn of bricks	0.012	0.	0.09	0.030	.0045	ŕ <sub>2</sub>	0.5
	0il Fired	tn of bricks			0.525			F <sub>2</sub>	0.5
	Coal Fired	tn of bricks		3.655				F <sub>2</sub>	0.5
	Coal/Gas Fired	tn of bricks	0.16A		0.81	0.71	0.000	F <sub>2</sub>	0.5
	Sawdust Fired	tn of bricks	0.12	0.010	0.01			F <sub>2</sub>	0.5
	Periodic Kilns	*** ** ** ***	****					. 7	•
	Gas Fired	tn of bricks	0.033	٥.	0.25	0.075	0.015	F <sub>2</sub>	0.5
	0il Fired	tn of bricks		2.935		0.095		F <sub>2</sub>	0.5
	Coal Fired	tn of bricks		6.06S	1.18			F <sub>2</sub>	0.5

3692 Manufacture of Cement, Lime and Plaster

#### Lime Manufacturing<sup>37</sup>

Coal Storage and Processing (If Coal is used as fuel)

	•
Coal Storage	•
Open Piles	th lime 0.5
Semi-Enclosed Piles	tn lime 0.25
Compartments	tn lime 0.1
Silos	th lime 0.1
Coal Crushing and Screening	
Uncontrolled	tn lime 0.18
FF	tn lime 0.002
Coal Grinding	
(Semi) Direct Fired Syst	tn Lime 0.0
Indirect Fired System	
Uncontrolled	tn Lime 10.
Fabric Filter	tn Lime 0.1
Raw Material Storage	tn Lime 0.16
Crushing & Screening	
Uncontrolled	tn Lime 1.5
Fabric Filter	tn Lime 0.0005

<sup>36.</sup> "S" is the percent sulfur in the fuel. (a)

<sup>&</sup>quot;A" is the percent ash in the coal. (b)

Emissions from the combustion of fuel are included. (d) Control of the kiln gases by scrubbers can reduce fluoride emissions by 95%.

<sup>(</sup>b) Coal fired kilns are rather rare since coal tends to affect product quality.

<sup>37.</sup> "S" is the percent sulfur in the fuel. (a)

<sup>(</sup>b) Emissions from fuel combustion, as well as fugitive dust emissions are included.

Model for Air Emission Inventories and Controls - Cont'd

IC#	PROCESS	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	<b>v</b> oc kg/V	kg/l
					<del></del>			
	Crushed Material Storage							
	Open Piles	tn Lime	1.0					
	Semi-Enclosed Piles	tn Lime	0.5					
	Compartments	tn Lime	0.2					
	Silos	tn Lime	0.2					
	Raw Material Conveying							
	Uncontrolled	tn Lime	1.2					
	Fabric Filter	tn Lime	0.01					
	Raw Material Calcining							
	Vertical Shaft Kiln							
	Uncontrolled	tn Lime	3.0	0.98	0.1	2.0	•	
	Cyclone	tn Lime		0.95	0.1	2.0		
	Multicyclones	tn Lime	0.75	0.95	0.1	2.0		
	Vertical Double Inclined Kilns		0.73	0.55	0.1	2.0		
	Uncontrolled	tn Lime	10.5	0.98	0.1	2.0		
	Cyclone	tn Lime	3.6	0.95	0.1	2.0		
	Multicyclones	tn Lime	2.6	0.95	0.1	2.0		
	Parallel Flow/Counterflow Rege		2.0	V.33	0.1	2.0	•	
	Uncontrolled	to Lime	8.	0.98	0.1	2.0		
	Cyclone	th Lime	2.8	0.95	0.1	2.0		
	Multicyclones		2.0					
	Annular Kilns	th Lime	۷.	0.98	0.1	2.0		
	Uncontrolled	4-1:	10	0.00				
		tn Lime	12.	0.95	0.1	2.0		
	Cyclone	tn Lime	4.2	0.95	0.1	2.0		
	Multicyclones Rotary Short Kiln/Air Suspensi	tn Lime	3.	0.95	0.1	2.0		
	Uncontrolled		40	0.200	1 5	1.0		
		tn Lime		0.368	1.5	1.0		
	Cyclone Multicyclones	tn Lime		0.368	1.5	1.0		
	ESP	tn Lime		0.365	1.5	1.0		
	Fabric Filter	tn Lime		0.368	1.5	1.0		
		tn Lime	0.2	0.36S	1.5	1.0		
	Rotary Long Kiln							
	Uncontrolled	tn Lime		0.36\$	1.5	1.0		
	Cyclone	to Lime		0.36S	1.5	1.0		
	Multicyclones	tn Lime		0.365	1.5	1.0		
	ESP	tn Lime		0.368	1.5	1.0		
	Fabric Filter	tn Lime	0.4	0.365	1.5	1.0		
	Calcimatic Kiln							
	Uncontrolled	tn Lime	25.	0.95	0.1	1.0		
	Cyclone	tn Lime	8.7	0.98	0.1	1.0		
	Multicyclones	tn Lime	6.2	0.98	0.1	1.0		
	Lime Cooling							
	Grate Cooler							
	Uncontrolled	tn Lime	20.					
	Cyclones	tn Lime	4.					
	Multicyclones	th Lime	2.					
	Fabric Filters	tn Lime	0.1					
	Planetary, Rotary, or							
	Vertical Shaft Coolers	tn Lime	0.0					

1C#	PROCESS	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/Մ	VOC kg/Մ ————	kg/l		
	Lime Packaging / Shipping	tn Lime	0.12				,			
	Lime Hydration									
	Uncontrolled	tn of lime	35,00							
	Scrubber	to of lime	0.04							
	Cement Manufacturing <sup>38</sup>									
	Typical Well-Controlled Plant	tn of cement	1.9	1.02	2.15		·			
	Coal Storage and Processing (If Co	al is used as f	uel)							
	Coal Storage (Only if Coal is U		·							
	Open Piles	tn clinker	0.5							
	Semi-Enclosed Piles	tn clinker	0.25							
	Compartments	tn clinker	0.1							
	\$ilos	tn clinker	0.1							
	Coal Crushing and Screening (Only if Coal is Used as Fuel)									
	Uncontrolled	tn clinker	0.18							
	Fabric Filter	tn clinker	0.002							
	Coal Grinding									
	(Semi) Direct Fired Syst	tn Clinker	0.							
	Indirect Fired System									
	Uncontrolled	tn Clinker	10.							
	Fabric Filter	tn Clinker	0.1							
	Raw Materials Storage	tn clinker	0.14							
	Raw Materials Crushing & Screening	1								
	Primary & Secondary Crushing									
	Uncontrolled	tn clinker	4.2							
	Cyclone	tn clinker	0.85							
	Multicyclone	tn clinker	0.63							
	Fabric Filter	tn clinker	0.02							
	Tertiary Crushing <sup>39</sup>									
	Uncontrolled	tn clinker	5.1							
	Cyclone	tn clinker	1.0							
	Multicyclone	tn clinker	0.77							
	Fabric Filter	tn clinker	0.026							
	Raw Material Conveying									
	Uncontrolled	tn clinker	1.5							
	Good Control (FF)	tn clinker	0.075							

<sup>38.</sup> Emissions from the combustion of fuel are included.

<sup>39.</sup> Tertiary crushing of the raw materials to a fairly small size facilitates grinding. However, plugging or gumming of the crushers due to the presence of sticky materials often prevents tertiary crushing.

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U	l kg/∪
	Raw Material Grinding & Calcining <sup>40</sup>							
	Dry Process Kiln							
	Uncontrolled	tn clinker	128	1.02	2.15			
	Multicyclone+ESP	tn clinker	0.34		2.15			
	Baghouse	tn clinker	0.16		2.15			
	Wet Process Kiln							
	Uncontrolled	tn clinker	120.	1.02	2.15			
	ESP	tn clinker	0.39	1.02	2.15			
	Baghouse	tn clinker		1.02				
	Clinker Cooler	2 22.						
	Grate Cooler							
	Uncontrolled	tn clinker	10.6					
	Cyclones	tn clinker	2.2					
	Multicyclones	tn clinker	0.530					
	Gravel Bed Filters	tn clinker	0.160					
	ESP	tn clinker	0.048					
	Baghouse	tn clinker	0.010					
	Planetary or Rotary Cooler	tn clinker	0.0					
	Clinker Storing							
	Open Piles	tn clinker	5.4					
	Semi-Enclosed Piles	tn clinker	2.4					
	Compartments	tn clinker	0.12					
	Silos	tn clinker	0.12					
	Clinker Grinding							
	Tube Mill / Open Cycle							
	Uncontrolled	tn clinker	10.6					
	ESP or FF	tn clinker	0.05					
	Tube Mill / Closed Cycle or Roller							
	Uncontrolled	tn clinker	85					
	ESP or FF	tn clinker	0.43					
	Cement Storing in Siles	tn clinker	0.13					
	Cement Shipment		<del>-</del>					
	Bulk Loading	tn alinker	0.1					
	Packaging		.,					
	Uncontrolled	tn clinker	2.2					
	FF	tn clinker	0.01					

<sup>40. (</sup>a) In typical dry-process installations, a portion of the hot gases from the calcining kilns is fed in the grinding mills for drying the raw meal. Gas from grinders-dryers and kilns is thus combined and treated in a common installation.

<sup>(</sup>b) The listed  $\mathrm{SO}_2$  emission factor is based on German studies indicating  $\mathrm{SO}_2$  removal efficiencies through reactions with alkaline dust from 88% to 100%. Higher  $\mathrm{SO}_2$  emissions are obtained only if the  $\mathrm{SO}_2$  exceeds the alkaline content of the raw meal.

<sup>(</sup>c) The U.S. EPA, on the basis of limited data, reports  $SO_2$  removal from 21% to 45% and suggests the use of the following  $SO_2$  emissions factors: For coal fired kilns: 5.4+3.6\*S, for fuel oil fired kilns 5.4+2.2\*S and for Gas fired kilns 5.4, where S is the weight % sulfur in the fuel used.

SIC#	PROCESS	 ,	419177 (10)	TAA					
310#	rkuce33		UNIT (U)	TSP	50 <sub>2</sub>	NUX	CO	VOC	
				kg/U	kg/U	kg/U	kg/U	kg/U	kg/U

### 3699 Manufacture of Non-Metallic Mineral Products not Elsewhere Classified

Gypsum Manufacture		
Rotary Ore Dryers		
Uncontrolled	tn	5-60
Fabric Filter	tn	0.02
Raw Mills		
Roller Mills		
Uncontrolled	tn	1.3
Fabric Filter	tn	0.06
ESP	ŧπ	0.05
Impact Mills		
Uncontrolled	tn	50
Fabric Filter	tn	0.01
Calciners		
Flash Calciners		
Uncontrolled	ţn	19
Fabric Filter	tn	0.02
Continuous Kettle Calciner		
Uncontrolled	tn	21
Fabric Filter	tn	0.003
ESP	tn	0.05
Concrete Batching		
Process Emissions (Uncontrolled)	tn	0.05
Wind Erosion		
Sand & Aggregate Storage (1000 m	1 <sup>2</sup> )*yr	142.
Vehicle Traffic		
(Unpaved Road) Vehicle km Trav	elled	4.5
Perlite Manufacturing		
Perlite Expansion Vertical Furnace		
Uncontrolled	tn	10.5
Fabric Filter	tn	0.1

# DIVISION 37. BASIC METAL INDUSTRIES

### 371 Iron and Steel Basic Industries

Gray Iron Foundries  $^{41}$ Cupo la 42, 43

-F- :-						
Uncontrolled	tn	6.9	0.68	73	₽b	0.32
Single Wet Cap	tn	4.0	0.35	73	РЪ	0.19

<sup>(</sup>a) For one ton of gray iron product, about 143 kg of Coke are required.

<sup>(</sup>b) The emission factors account also for the fugitive dust sources, as well as for the emissions caused by the burning of coke.

<sup>&</sup>quot;S" is the percent sulfur in the coke. 42.

<sup>43.</sup> CO emission factor of 7.0 must be used in cases where afterburners are installed.

Model for Air Emission Inventories and Controls - Cont'd

I SIC# PROCESS		UN1 	IT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U		kg/U
lmp i ngem	ent Scrubber		tn	2.5	0.38		73		Pb	0.12
Scrubber			tn	1.6	0.35		73		Pb	0.07
	rgy Scrubber		tn	0.4	0.35		73		₽b	0.02
Baghouse			tn	0.3	0.65		73		Pb	0.01
	mer + ESP		tn	0.7	0.65		7		₽b	0.03
Electric Ar										
Uncontro	illed		ŧn	6.3		0.16	9.75	0.09		
Baghouse	·· !		tп	0.2		0.16	9.75	0.09		
· ·	duction Furnace									
Uncontro	lled		tn	0.5					Pb	0.026
Baghouse	:		ţn	0.1					Рb	0.005
Reverberato	ry Furnace									
Uncontro	ol led		tn	1.1					Рb	0.038
Baghouse	<b>!</b>		tn	0.1					Pb	0.004
Iron and Steel	Mills									
Sintering 44	•									
Windbox							•			
Uncor	trolled	th of :	sinter	4.35			22			
Ory 8	SP	tn of	sinter	8.0						
Wet 8	SP	tn of :	sinter	0.085						
Ventu	ıri Scrubber	tn of	sinter	0.235						
Cyclo	ne	tn of :	sinter	0.5						
Fabri	c Filter	tn of	sinter	0.1						
Braker a	and Hot Screens									
Uncor	ntrolled	th of	sinter	3.4						
Ventu	ıri Sçrubber	tn of	sinter	0.295						
Bagho		tn of	sinter	0.05						
Blast Furna										
	olled Casthouse <sup>47</sup>		ţn	0.3						
Furnaçe	with Local Evaculation		tn	0.65						

<sup>44. (</sup>a) Sintering is used in some plants to convert fine size raw materials (iron ore, coke breeze, limestone, mill scale & flue dust) into agglomerated product of suitable size to be charged into the blast furnace.

<sup>(</sup>b) About 2.5 tons of raw materials, including water & fuel, are required to produce 1 ton of product sinter.

<sup>45. (</sup>a) Production of one ton of iron requires 1.4 tons of ore, 0.5 to 0.65 tons of Coke, 0.25 tons of limestone or dolomite, and 1.8 to 2.0 tons of Air.

<sup>(</sup>b) By-products consist of 0.2 to 0.4 tons of slag and 2.5 to 3.5 tons of blast furnace gas containing up to 50 kg of dust.

<sup>(</sup>c) Emissions from the use of the blast furnace gas (after dedusting) are not included in the factors listed here and need to be computed separately.

<sup>46. (</sup>a) Blast Furnace Gas controls, typically (settling chamber or cyclone)+(wet scrubber)+(high energy wet scrubber or ESP), are often considered part of the process since cleaning of the Blast Furnace Gas is required before it can be used as a fuel.

<sup>(</sup>b) The listed TSP emission factors do not include these from blast furnace slips (39.5 kg/tn of hot metal per slip).

<sup>47.</sup> Typical of older furnaces.

SIC#	PROCESS	UNIT	(8)	TSP kg/U	80 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	Ç0 kg/U	<b>VO</b> C kg/U —————	kg/U
	Basic Oxygen Furnaces							•	
	Furnace for Melting & Refining								
	Uncontrolled		tn	14.25					
	Open Hood with ESP			0.065					
	Open Hood with Scrubber			0.045					
	Closed Hood with Scrubber			0.0034					
	Charging, Tapping, Transfer		tn	0.25					
	Electric Arc Furnaces								
	Uncontrolled								
	Carbon Steel		ţn	25			69		
	Alloy Steel		tn	5.65			69		
	Control of Primary Emissions		tn	0.15					
	Control of Primary &								
	Secondary Emissions		tn	0.0215					
	Open Hearth Furnaces								
	Uncontrolled		tn	10.55			9		
	Fabric Filter of ESP		tn	0.22					
	Ferroalloy Production (Electric Smeltin	g Furnai	ces)'	18					
	Uncontrolled - Open Furnace		tn	35					
	Uncontrolled - Covered Furnace		tn	46					
	Baghouse		tn	0.9					
	High Energy Scrubber		tn	0.24					
	Low Energy Scrubber		tn	4.5					
	FeSi (75%)								
	Uncontrolled - Open Furnace		tn	158					
	Uncontrolled - Covered Furnace		ŧπ	103					
	Low Energy Scrubber		tn	4					
	FeSi (90%)								
	Uncontrolled - Open Furnace		tn	282					
	Si Metal (98%)								
	Uncontrolled - Open Furnace		tn	436					
	Baghouse		tn	16					
	FeMn (80%)								
	Uncontrolled - Open Furnace		tn	14					
	Baghouse		tπ	0.24					
	High Energy Scrubber		tn	0.8					
	FeMn (1% Si)								
	Uncontrolled - Covered Furnace		tn	6					
	Uncontrolled - Sealed Furnace		ţn	37					
	High Energy Scrubber		tn	0.25					
	FeCr (High Carbon)								
	Uncontrolled - Open Furnace		ţn	78					
	ESP			1.2					

<sup>48.</sup> Given percentages in the alloys refer of the main alloying element in the product.

 $\label{thm:model} \mbox{Model for Air Emission Inventories and Controls - Cont'd}$ 

IC#	PROCESS	(U) TIMU	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/U ——	CO kg/V	VOC kg/V ——————	kg/∪
	SiMn							
	Uncontrolled - Open Furnace	e tn	96					
	Uncontrolled - Sealed Furna	ace tn	-					
	High Energy Scrubber	tn	2.1					
	Low Energy Scrubber	tn	0.15					
	Steel Foundries							
	Electric Arc Furnace							
	Uncontrolled	tn	6.5		0.1			
	ESP	tn	0.33		0.1			
	Baghouse	tn	0.1		0.1	•		
	Venturi Scrubber	tn	0.26					
	Open Hearth Furnace							
	Uncontrolled	tn	5.5		0.005			
	ESP	tn	0.18		0.005			
	Baghouse	tn	0.006		0.005			
	Venturi Scrubber	tn	0.14					
	Open Hearth Oxygen Lanced Furn		0.17					
	Uncontrolled	tn	5					
		tn	0.175					
	ESP		0.175					
	8aghouse	tn 4-						
	Venturi Scrubber	tn	0.175					
	Electric Induction Furnace Uncontrolled	tn	0.05					
72	Non-Ferrous Metal Basic Industri	es ′						
	Primary Copper Smelting							
	Uncontrolled	tn of Copper Ore	62	530				
		tn of Copper	248.0	2120				
	Hat ESP (200-340 C)	tn of Copper Ore	15.5	530				
		tn of Copper	62	2120				
	Cold ESP (120 C)	tn of Copper Ore	2.5	530				
		tn of Copper	10	2120				
	Single Contact H <sub>2</sub> SO <sub>4</sub> Plant	tn of Copper Ore	2.5	25.2				
		tn of Copper	10	100.7				
	Double Contact H <sub>2</sub> SO <sub>4</sub> Plant	tn of Copper Ore	2.5	8				
	2 4	tn of Copper	10	32				
	Secondary Copper Smelting and Al	loying						
	Copper Scrap							
	Cupola (Uncontrolled)	tn	0.002					
	Reverberatory Furnace		_					
	Uncontrolled	tn	2.6					
	fabric Filter	tn	0.2					
	Electric Arc Furnace							
	Uncontrolled	tn	2.5					
	Fabric Filter	tn	0.5					

C# PROCESS	נותט	(U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/U	VOC kg/U	kg/∪
Electric Induction	Furnace							
Uncontrolled		tn	3.5					
Fabric Filter		tn	0.25					
Copper Insulated Wire								
Cupo la								
Uncontrolled		tn	120					
ESP		tn	5.0					
Copper and Brass Scrap								
Cupola								
Uncontrolled		tn	3.5					
ESP		tn	1.2					
Brass and Bronze								
Reverberatory Furna	ce							
Uncontrolled		tn	18					
Fabric Filter		tn	1.3					
Rotary Furnace								
Uncontrolled		tn	150					
ESP		tn	7					
Crucible or Pot Furi	nace							
Uncontrolled		tn	11					
ESP		tn	0.5					
Electric Arc Furnace	2							
Uncontrolled		tn	5.5					
Fabric Filter		tn	3.0					
Electric Induction (	-urnace							
Uncontrolled		tn	10					
Fabric Filter		tn	0.35					
Alumina Production (Bayer	Process from Bauxite)	49						
Bauxite Grinding								
Uncontrolled	tn of Bau	xite	3					
Spray Tower	tn of Bau	xite	0.9					
Floating bed scrubbe	er tn of Bau	xite	0.85					
Quench Tower+Spray S	Screen th of Bau	xite	0.5					
Alumina Hydroxide Calc	ining							
Uncontrolled	tn of Alu	mina	100					
Spray Tower	tn of Alu	mina	30					
Floating bed scrubbe	er tn of Alu	mina	28					
Quench Tower	tn of Alu	mina	17					
ESP	tn of Alu	mina	2					

<sup>49.</sup> From 1.4 to 3.3 tons of Bauxite Ore processed, one ton of Alumina is produced. One ton of the later yields 526 kg of Aluminum.

Model for Air Emission Inventories and Controls - Cont'd

IC#	PROCESS			UNIT (U)	T\$P kg/U ——	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U	<del></del>	kg/l
	Primary Aluminum Production (from Al	lumina	, j 5 <sup>(</sup>	0							
	Prebaked Cell Method										
	Anode Baking Furnace										
	Uncontrolled	tn c	of ,	Aluminum	1.5					F	0.
	Spray Tower	tn c	of.	Aluminum	0.375					F <sup>-</sup>	0.03
	ESP	tn c	of .	Aluminum	0.375					F <sup>-</sup>	0.03
	Dry Alumina Scrubber	tn c	ρĒ.	Aluminum	0.03					F <sup>-</sup>	0.005
	Prebaked Reduction Cells										
	Uncontrolled (total)	tn c	of.	Aluminum	47	10\$				F-	2
	Fugitive	tn o	ρf	Aluminum	2.5	0.5\$				F-	1.
	Multiple Cyclones	tn o	ρf	Aluminum	9.8					F-	13.
	Dry Aluminum Scrubber	tn c	ρf	Aluminum	0.9					F <sup>-</sup>	0.
	Dry ESP+Spray Tower	tn d	of	Aluminum	2.25					F-	2
	Spray Tower	tn o	of	Aluminum	8.9					F-	2
	Floating Bed Scrubber	ţn c	ÞΕ	Aluminum	8.9					F-	2.3
	Coated FF Dry Scrubber	tn d	٦f	Aluminum	0.9					F-	1.
	Cross Flow Packed Bed	tn o	٥f	Aluminum	13.15					F-	6.0
	Dry+Secondary Scrubber	tn d	οf	Aluminum	0.35					F"	0.:
	Vertical Sodeberg Cell Method										
	Vertical Sodeberg Cells										
	Uncontrolled (total)	tn «	οf	Aluminum	39	105				F-	;
	Fugitive	ţn (	φf	Aluminum	6	0.58				F <sup>-</sup>	3
	Spray Tower	tn (	of	Aluminum	8.25					F"	1
	Venturi Scrubber	tn (	of	Aluminum	1.3					F	0.
	Multiple Cyclones	tn (	of	Aluminum	16.5					F-	16
	Bry Alumina Scrubber	ţn (	of	Aluminum	0.65					F-	0.1
	Scrubber+ESP+Spray										
	Screen and Scrubber	tn (	of	Aluminum	3.85					F-	
	Horizontal Sodeberg Cell Method										
	Horizontal Sodeberg Cells										
	Uncontrolled (total)	tn	of	Aluminum	49	10S				F"	
	Fugitive	ţn	of	Aluminum	5	0.5\$				F -	1
	Spray Tower	ţn :	of	Aluminum	11.					F"	5
	Floating Bed Scrubber	tn	of	mucrimuf A	9.7					F-	1
	Scrubber+Wet ESP	tn	of	Aluminum	0.9					F-	0

<sup>50. (</sup>a) "S" is the weight percent sulfur in the prebaked anodes.

Electricity 13.2 to 18.7 MWH
Alumina 1.89 to 1.92 tons (2.7 to 6.3 tons of Bauxite)
Carbon Electrodes 0.45 to 0.55 tons
Electrolyte Fluoride 0.03 to 0.10 tons.

<sup>(</sup>b) The listed TSP factors include particulate fluorides.

<sup>(</sup>c) The listed F factors include gaseous, as well as particulate fluorides.

<sup>(</sup>d) If controls are applied, the fugitive, as well as controlled stack emissions need to be computed.

<sup>(</sup>e) In older plans cells may not be constructed with covers for the collection of fumes and this may increase drastically the fraction of the uncontrolled fugitive emissions.

<sup>(</sup>f) For the production of one ton of Aluminum the basic energy and material requirements are as follows:

Model for Air Emission Inventories and Controls - Cont'd

IC#	PROCESS	_	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/V	CO kg/U	VOC kg/U		kg/U
	Wet ESP	tn of	Aluminum	0.9					F"	0.6
	Dry Alumina Scrubber		Aluminum	0.9					F-	0.3
	Secondary Aluminum Production									
	Pretreatment									
	Sweating Furnace									
	Uncontrolled	tn of Al p	retreated	7.25						
	Fabric Filter	tn of Alp		1,65						
	Smelting	311 37 711 P								
	Crucible Furnace									
	Uncontrolled		tn of Al	0.95						
	Reverberatory Furnace			0.00						
	Uncontrolled		tn of Al	2.15						
	Fabric Filter or ESP		tn of Al	0.65						
	Demagging (Chlorination)		CII OI 711	0.00						
	Uncontrolled		tn of Cl <sub>2</sub>	500						
	Fabric Filter		tn of Cl2	25						
	Padric Price		0. 0.2							
	Primary Lead Smelting									
	Fugitive Emissions		tn of Pb	16.74					Pb	2.5
	Ore Crushing									
	Uncontrolled	tn of cr	ushed ore	1.0					РЬ	0.15
	Fabric Filter		ushed ore	0.01					Рb	0.0015
	Sintering (updraft)									
	Uncontrolled		tn of Pb	106.5	275.				Рb	87
	Centrifugal Collector		tn of Pb	16.	275.				РЬ	13
	ESP		tn of Pb	3.2	275.				Pb	2.61
	Fabric Filter		tn of Pb	3.2	275.				Pb	2.61
	H <sub>2</sub> SO <sub>4</sub> Plant (Single Conta	ct)	tn of Pb	0.32	9.6				Pb	0.28
	H <sub>2</sub> SO <sub>4</sub> Plant (Dual Contact		tn of Pb	0.32	5.5				Pb	0.26
	Elemental S Recovery Plan		tn of Pb		27.5				Pb	0.26
	Dimethylaniline Absorptio		tn of Pb		8.25				PЬ	0.26
	Ammonia Absorption		tn of Pb		17.9				Рb	0.26
	Blast Furnace									
	Uncontrolled		tn of Pb	180.5	22.5				Pb	29
	Centrifugal Collector		tn of Pb	27.1					Pb	4.35
	ESP		tn of Pb		22.5				Pb	0.9
	Fabric Filter		tn of Pb		•				Pb	0.9
	H <sub>2</sub> SO <sub>4</sub> Plant (Single Conta	ct)	tn of Pb		0.8				Pb	0.1
	H <sub>2</sub> SO <sub>4</sub> Plant (Dual Contact		tn of Pb		0.5				РЬ	0.1
	Elémental S Recovery Plan		tn of Pb						РЬ	0.1
	Dimethylaniline Absorptio		tn of Pb						PЬ	0.1
	Ammonia Absorption		tn of Pb						Pb	0.1
	Dross Reverberatory Furnace									
	Uncontrolled		tn of Pb	10.					₽b	2.4
	Centrifugal Collector		tn of Pb						Pb	0.36
	Fabric Filter		tn of Pb						Pb	0.07
	Materials Handling		/ , _	2.3					-	
	Uncontrolled		tn of Pb	2.4						

 $\label{thm:model} \mbox{Model for Air Emission Inventories and Controls - Cont'd}$ 

C#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>x</sub> kg/V	CÓ kg/U	VOC kg/U		kg/l
	Fabric Filter	tn of Pb	0.07						
S	econdary Lead Processing								
	Pretreatment								
	Sweating Furnace								
	Fugitive Emissions	tn of Pb	1.3					PЬ	0.55
	Uncontrolled	tn of Pb	25.5					₽b	(
	Controlled	tn of Pb	0.25					Pb	0.06
	Smelting								
	Fugitive Emissions	tn of Pb	8.2					Pb	2.19
	Reverberatory Furnace								
	Uncontrolled	tn of Pb	162	40				Pb	32
	Controlled	tn of Pb	0.5	40				Pb	0.
	Blast (Cupola)								
	Uncontrolled	tn of Pb	153	27				Pb	52
	Controlled	tn of Pb	1.12	27				Pb	0.1
	Refining								
	Kettle Refining								
	Uncontrolled	tn of Pb	0.02					РЬ	0.00
	Controlled	tn of Pb							
	Kettle Oxidation								
	Fabric filter	tn of PbO	<20.0					РЬО	<20.
S	Storage Battery_Production								
	Uncontrolled <sup>51</sup>	1000 Batteries	63.2					Pb	6.9
	Controlled	1000 Batteries	3.2					Pb	0.
F	Primary Zinc Smelting								
	Pyrometallurgical Process								
	Fugitive Emissions	tn of Zinc	3.85						
	Roasting								
	Multiple Hearth Roaster								
	Uncontrolled	tn of Zinc	113	1100					
	Cyclone + ESP	tn of Zinc	0.5	1100					
	H <sub>2</sub> \$O <sub>4</sub> Plant	tn of Zinc	0.34	33					
	Suspension Roaster								
	Uncontrolled	tn of Zinc	1000.	1100					
	Cyclone + ESP	tn of Zinc	4.	1100					
	H <sub>2</sub> SO <sub>4</sub> Plant	tn of Zinc	3.	33					
	Fluidized Bed Roaster								
	Uncontrolled	tn of Zinc	1083.	1100					
	Cyclone + ESP	tn of Zinc	4.	1100					
	H <sub>2</sub> SO <sub>4</sub> Plant	tn of Zinc	3.2	33					
	Sinter Plant								
	Uncontrolled	tn of Zinc	62.5	110					
	Cyc lone	tn of Zinc	24.1	110					

<sup>51.</sup> A fabric filter is considered an integral part of the lead oxide mill, if any.

Model for Air Emission Inventories and Controls - Cont'd

SIC# PROCESS	(U) TIMU	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	CO kg/U	VOC kg/U ——————	kg/l
Retorting (Uncontrolled)							
Vertical Retort	tn of Zinc	7.15					
Electric Retort	tn of Zinc	10					
	EN OF ZINC	10					
Electrolytic Process Fugitive Emissions	tn of Zinc	1.26					
_	th of Zinc	1.20					
Roasting							
Multiple Hearth Roaster Uncontrolled	tn of Zinc	113	1100				
Cyclone + ESP	tn of Zinc	0.5	1100				
	tn of Zinc	0.34	33				
${ m H_2SO_4}$ Plant Suspension Roaster	cii di Zimo	0.04	00				
Uncontrolled	tn of Zinc	1000	1100				
	tn of Zinc	4	1100				
Cyclone + ESP	th of Zinc	3	33				
H <sub>2</sub> SO <sub>4</sub> Plant	th or The	J	20				
Fluidized Bed Roaster	tn of Zinc	1083	1100				
Uncontrolled	tn of Zinc	1003	1100				
Cyclone + ESP			33				
H <sub>2</sub> SO <sub>4</sub> Plant	tn of Zinc	3.2	33				
Electrolytic Process Uncontrolled	tn of Zinc	3.3					
Secondary Zinc Smelting							
Pretreatment							
Sweating							
Reverberatory Furnace							
Clean Metallic Scrap	tn of Scrap	0.					
General Metallic Scrap							
Uncontrolled	tn of Scrap	6.5					
Fabric Filter	tn of Scrap	0.1					
Residual Scrap							
Uncontrolled	tn of Scrap	16.					
Fabric Filter	tn of Scrap	0.24					
Rotary Furnace	_	_					
Uncontrolled	tn of Scrap	9.					
Fabric Filter	tn of Scrap	0.14					
Muffle Furnace							
Uncontrolled	tn of Scrap	10.7					
Fabric Filter	tn of Scrap	0.16					
Kettle Furnace		_					
Clean Metallic Scrap	tn of Scrap	0.					
General Metallic Scrap			1				
Uncontrolled	tn of Scrap						
Fabric Filter	tn of Scrap	0.08	1				
Residual Scrap							
Uncontrolled	tn of Scrap						
Fabric filter	tn of Scrap	0.2	!				
Electric Resistance Furnace							
Uncontrolled	tn of Scrap						
Fabric Filter	tn of Scrap	< 0.7	,				

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/V	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U 	kg/U
	Crushing & Screening							
	- Uncontrolled	tn of Scrap	2.2					
	Fabric Filter	tn of Scrap	0.02					
	Sodium Carbonate Leaching	•						
	Crushing & Screening							
	Uncontrolled	tn of Scrap	2.2					
	Fabric Filter	tn of Scrap	0.02					
	Calcining	,						
	Uncontrolled	tn of Scrap	44.5					
	Fabric Filter	tn of Scrap	0.7					
	Melting							
	Kettle (Pot) Melting							
	Uncontrolled	tn Zn	0.05					
	Refining							
	Retort & Muffle Distillation							
	Uncontrolled	tn Žn	23					
	fabric filter	tn Zn	0.35					
	Graphite Rod Distillation	tn Zn	0.0					
	Retort Distillation/Oxidation	tn ZnO	15					
	Muffle Distillation/Oxidation	tn ZnO	15					
	Retort Reduction							
	Uncontrolled	tn Zn	23.5					
	Fabric Filter	tn Zn	0.35					
	Galvanizing	tn Zn Used	2.5					

#### MAJOR DIVISION 4. ELECTRICITY GAS AND WATER

#### 410 Electricity Gas and Steam<sup>52</sup>

<sup>52. (</sup>a) "S" is the weight percent of Sulfur in the fuel.

<sup>(</sup>b) "A" is the weight percent of Ash in the solid fuel.

<sup>(</sup>c) "N" is the weight percent of Nitrogen in the fuel.

<sup>53.</sup> Typical sulfur content of Natural Gas is 0.000615 %.

<sup>54.</sup> For tangentially fired boilers use 5.6f kg/1000 Nm $^3$ . The load reduction coefficient "f" is computed from Equation  $f = 0.3505 - 0.005235 \pm + 0.0001173 \, L^2$ , where L is the mean boiler load, %. A typical mean boiler load is 87 %.

Model for Air Emission Inventories and Controls - Cont'd

SIC# PROCESS	UNI	T (U)	TSP kg/U		NO <sub>x</sub> kg/U				kg/l
Liquefied Petroleum Gas (LPG)		MWH	0.138	9.68	4.08	1.14	0.415		
Industrial Boilers	_3	/1 : _ 1	0.001	0 004					
industrial bollers	m <sup>o</sup>	(Liq)			1.51				
Damash (+ 5	3		0.060			0.71			
Domestic Furnaces	m,		0.031				0.09		
		tn	0.060	0.007	2.05	0.42	0.17		
Liquid Fuels									
Distillate Fuel Oil									
Industrial & Commercial Boilers		tn	0.28	208	2.84	0.71	0.035	\$0 <sub>3</sub>	0.289
Residential Furnaces		tn	0.3655				0.354	\$0 <sub>3</sub>	0.289
Stationary Gas Turbines		tn	0.710	205		2.19		**3	V.LO
•		MWH	0.369			1.14			
Residual Fuel 0:1 <sup>56</sup>			0.000		0.01	1.17	0.415		
Utility Boilers									
Uncontrolled		tn	P	208	8.557	0.64	0.127	SO <sub>2</sub>	0.258
ESP - Low Efficiency		tn	0.5P	208		0.64		SO <sub>3</sub>	0.259
ESP - High Efficiency		tn	0.1P	208	8.5		0.09	503	0.259
Scrubber		tn	0.45P	1.55	8.5		0.09	303	0.200
Industrial & Commercial Boilers <sup>58</sup>		tn	D. 40,		7.059			sn.	0.259
Waste Lub Oil <sup>60</sup>		•	· ·	200	7. ¥	0.04	0.105	303	0.493
Industrial & Commercial Boilers		tn	8.1A	205	2.7	0.67	0.13	Ръ	5.6P
Domestic Heaters		tn	8.6A	205	2.7		0.13	Pb	6.8P

#### Solid Fuels

Anthracite Coal<sup>61</sup>

Pulverized Coal Furnace

<sup>55.</sup> In the absence of boiler I/M programs, smoke emission factors may be closer to 1.6 kg/tm.

<sup>56. &</sup>quot;P", the uncontrolled TSP emission factor, is function of the sulfur content of fuel oil and is computed from Equation P = 0.4 + 1.32 \$

<sup>57.</sup> Use 5.3 kg/tm for tangentially fired boilers, 13.3 for vertical fired boilers and 8.5 for all other boiler types.

<sup>58. (</sup>a) In the absence of boiler I/M programs, the average smoke emission factor can exceed that in the table by about 60%, Economopoulos (1987).

<sup>(</sup>b) In cases where very effective boiler I/M programs are implemented, the average smoke emission factor can be lower by up to 45% of that listed in the table, Economopoulos (1991).

<sup>59.</sup> If the nitrogen content of the fuel is known, the  $NO_X$  emission factor can be computed more accurately from the empirical formula (3.25+59.2  $N^2$ ).

<sup>60. (</sup>a) Typical values of "A" and "S" in lub oils are 0.65 % and 0.5 %.

<sup>(</sup>b) "P" is the weight percent of Lead (Pb) in the fuel. The value of P depends on the lead content of the gasoline used. In the U.S.A. the average values of P dropped from 1 % in 1970 (catalytic cars and unleaded gasoline were not in use) to 0.11 % in 1982-83 (three years after the introduction of catalytic cars and unleaded gasoline) and to 0.04 % in 1985-86 (six years after the introduction of catalytic cars and unleaded gasoline).

<sup>61.</sup> Typical Ash and Sulfur contents are 8.1% & 0.9% for Meta Anthracite, 9.4% & 0.6% for Anthracite, and 12.4% & 2% for Semianthracite respectively (dry basis).

 $\label{thm:model} \mbox{Model for Air Emission Inventories and Controls - Cont'd}$ 

1C#	PROCESS	UNIT	(U)	TSP kg/U	50 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/li	voc kg/U	kg/
	_					<u> </u>	<del></del>		
	Uncontrolled		tn	5A	19.5\$	9.0	0.3	0.055	
	Cyclone		tn	1.25A	19.5S	9.0	0.3	0.055	
	ESP - High Efficiency		tn	0.36A	19.55	9.0	0.3	0.055	
	Fabric Filter		tn	0.01A		9.0	0.3	0.055	
	Travelling Grate Stoker								
	Uncontrolled		tn	4.6	19.55	5.0	0.3	0.055	
	Cyclone		tn	>1.2	19.58	5.0	0.3	0.055	
	Hand Fed Units		ţn	5.0	19.55	1.5	45.0	9.0	
	Bituminous & Subbituminous Coal <sup>62</sup>								
	Pulverized Coal / Dry Bottom Furnace								
	Uncontrolled		tn	5A	19.591	0.563	0.3	0.055	
	Multiple Cyclones		tn	1.25A	19.5\$	10.5	0.3	0.055	
	ESP - High Efficiency								
	- Low S Coal+No Condining		tn	0.33A	19.55	10.5	0.3	0.055	
	- Otherwise		tn	>0.01A	19.55	10.5	0.3	0.055	
	Fabric Filter		tn	0.01A	19.58	10.5	0.3	0.055	
	Flue Gas Desulfurization		tn	0.05A	1.955	10.5	0.3	0.055	
	Pulverized Coal / Wet Bottom Furnace	;							
	Uncontrolled		tn	3.5A	19.58	17.	0.3	0.055	
	Multiple Cyclones		tn	0.88A	19.5\$	17.	0.3	0.055	
	ESP - High Efficiency								
	- Low S Coal+No Condining		tn	0.22 <b>7A</b>	19.5\$	17.		0.055	
	- Otherwise		tn	0.007A	19,55	17.	0.3	0.055	
	Fabric Filter		tn	0.007A	19.55	17.	0.3	0.055	
	Flue Gas Desulfurization		tn	0.035A	1.958	17.	0.3	0.055	
	Cyclone Furnace								
	Uncontrolled		tn	Α	19.5S	18.5	0.3	0.055	
	ESP - High Efficiency		tn	0.065A	19.58	18.5	0.3	0.055	
	Fabric Filter		tn	0.002A	19.55	18.5	0.3	0.055	
	Spreader Stoker Furnace								
	Uncontrolled		tn	30	19.55	7.0		0.055	
	Multiple Cyclones		tn	8.5	19.58	7.0	2.5	0.055	
	Overfeed Stoker Furnace								
	Uncontrolled		tn		19.55			0.055	
	Multiple Cyclones		tn	4.5	19.55	3.25	3.0	0.055	
	Underfeed Stoker Furnace								
	Uncontrolled		tn		5 15.5S			5 1.05	
	Multiple Cyclones		tn		5 <b>15</b> .5S				
	Hand fired Furnace		tn	7.5	5 15.5S	1.5	45.0	9.0	

<sup>62. (</sup>a) In Bituminous coals, typical Ash and Sulfur contents are 4.9% & 0.8% for Low Volatility coals, 2.9 & 0.6% for Medium Volatility coals, 6.5% & 1.3% for High Volatility A coals, 5.4% & 1.4% for High Volatility B coals, and 9.1% & 2.6% for High Volatility C coals respectively (dry basis).

<sup>(</sup>b) In Subbituminous coals typical Ash and Sulfur contents are, 4.7% & 1% for A type, 2.8% & 0.5% for B type, and 13.2 % & 0.4% for C type respectively (dry basis).

<sup>63.</sup> For tangentially fired boilers use 7.5 kg/tn.

Model for Air Emission Inventories and Controls - Cont'd

IC#	PROCESS	UNIT (C		SP SO <sub>2</sub> /U kg/l	NO,			kg/ប
	Lignite <sup>64</sup>							
	Pulverized Coal Furnace							
	Uncontrolled	tn	3.1A	15S <sup>65</sup>	e 66	Λ3	0.055	
	Cyclones		0.93A		6.		0.055	
	ESP - Older Units		0.16A		6.		0.055	
	ESP - High Efficiency		>0.016A		6.		0.055	
	Fabric Filter		0.016A		6.		0.055	
	Flue Gas Desulfurization		0.031A		6.		0.055	
	Cyclone Furnace	-,,	******	1100	٧.	V.5	0.035	
	Uncontrolled	tn	3.3A	158	8.5	0.3	0.055	
	Cyclones	tn	A		8.5		0.055	
	ESP - Older Units		0.165A		8.5		0.055	
	ESP - High Efficiency		>0.017A		8.5		0.055	
	Fabric Filter		0.017A		8.5		0.055	
	Spreader Stoker Furnace			400	٧.٠	<b>V</b> .0	0.000	
	Uncontrolled	tn	3.4A	158	3.0	2.5	0.055	
	Multiple Cyclones	tn	Α		3.0		0.055	
	Overfeed Stoker		-				******	
	Uncontrolled	tn	1.5A	158	3.0	3.0	0.055	
	Multiple Cyclones	tn	0.84A		3.0		0.055	
	Underfeed Stoker							
	Uncontrolled	tn	1.5A	15\$	3.0	5.5	1.05	
	Multiple Cyclones	tn	1.1A		3.0		1.05	
	Wood & Bark							
	Wood Boilers	tn	4.4	0.015	0.34	13.0	0.85	
	Wood-Bark Mixture Boilers							
	Uncontrolled	tn	3.6	0.075	0.34	13.0	0.85	
	Multicyclone	tn		0.075			0.85	
	Bark Botlers							
	Uncontrolled	tn	24	0.2	0.34	13.0	0.85	
	Multiple Cyclones	tn	4.5	0.2	0.34	13.0	0.85	
	Wood Stoves							
	Conventional Units	tn	15	0.2	1.4	140.0	46.0	
	Low emitting non-catalytic	tn	9.6			130.0		
	Low emitting catalytic	tn				39.0	21.6	
	Residential Fireplaces	tn	14.0	0.2	1.7	85.0	43.0	
	Bagasse	tn	8.0	0.0	0.6			

<sup>(</sup>a) "A" is the weight percent of Ash in the fuel (wet basis as fired)

<sup>&</sup>quot;S" is the weight percent of Sulfur in the fuel (wet basis as fired) (b)

<sup>(</sup>c) Typical Ash and Sulfur contents are 8.8 to 9.5 % & 0.8 to 1.1 % (dry basis).

For more accurate estimate compute the  $\mathrm{SO}_2$  emission factor from the relation (20-1.44\*Na<sub>2</sub>0)\*S, where Na<sub>2</sub>0 is the percent content of the ash in alkali constituents.

<sup>66.</sup> Use 7.0 kg/tn for front wall fired and horizontally opposed wall fired units. Use 4.0 kg/tn for opposed wall fired units. Lignites with very high humidity and low calorific values may yield significantly lower  $\mathrm{NO}_{\mathrm{X}}$  emissions.

Model for Air Emission Inventories and Controls - Cont'd

								1
\$1C#	PROCESS	UNIT (U)	TSP	502	NO.	ÇO	VOC	
			kg/U	kg/Ū	kg/Û	kg/U	kg/U	kg/U

#### MAJOR DIVISION 6. WHOLESALE AND RETAIL TRADE

#### 610 Wholesale Trade

Bulk Fuel Terminals		
Storage of Fuels <b>67</b>		
Floating Roof Tanks		
<del>-</del>	rage capacity)*year	1.14
Crude Oil (m <sup>3</sup> sto	rage capacity)*year	0.435
Jet Naphtha (m <sup>3</sup> sto	rage capacity)*year	0.415
Jet Kero (m <sup>3</sup> sto	rage capacity)*year	0.019
Distillate Oil (m <sup>3</sup> sto	rage capacity)*year	0.015
Fixed Roof Tanks		
Gasoline (m <sup>3</sup> sto	rage capacity)*year	13.1
Crude Oil (m <sup>3</sup> sto	rage capacity)*year	2.8
Jet Naphtha (m <sup>3</sup> sto	rage capacity)*year	3.8
	rage capacity)*year	0.19
Distillate Oil (m <sup>3</sup> sto	rage capacity)*year	0.17
Truck Filling Stations		
Gasoline Loading		
Splash Loading	m <sup>3</sup> of Gasoline	1.43
	tn of Gasoline	1.94
Submerged Loading <sup>68</sup>		
Normal Service	m <sup>3</sup> of Gasoline	0.59
	tn of Gasoline	0.80
Vapor Balance Serv	m <sup>3</sup> of Gasoline	0.98
	tn of Gasoline	1.33
Vapor Controlled	m <sup>3</sup> of Gasoline	0.05
	tn of Gasoline	0.07
Jet Naphtha Loading	<b>.</b>	
Splash Loading	m <sup>3</sup> of Gasoline	0.43
	tn of Gasoline	0.58
Submerged Loading	<b>3</b>	
Normal Service	m <sup>3</sup> of Naphtha	0.18
	tn of Naphtha	0.24
Vapor Balance Serv	m <sup>3</sup> of Naphtha	0.30
	tn of Naphtha	0.40

<sup>67.</sup> The listed emission factors yield the VOC emissions in kg/year.

In the Vapor Balance Service the cargo truck retrieves the vapors displaced during the underground tank filling in service stations (see below, SIC 620). This operation increases the VOC concentration in the air within the empty truck and causes higher VOC emissions when the truck is filled. It should be noted in this regard that most of the VOC emissions reduction achieved through the balanced vapor filling of the service stations submerged tanks is offset by the resultant increased emissions in the Truck Filling Station, unless a vapor recovery system is used in the latter.

SIC#	PROCESS	UNIT (U)	TSP kg/U	SO <sub>2</sub> kg/U	 CO kg/U	VOC kg/U	kg/l
620	Retail Trade						
	Service Stations Operation						
	Filling the Underground Tanks						
	Splash Filling	m <sup>3</sup> of Gasoline				1.5	
		tn of Gasoline				2.03	
	Submerged Filling	m <sup>3</sup> of Gasoline				1.0	
	-	tn of Gasoline				1.353	
	Balanced Vapor Filling	m <sup>3</sup> of Gasoline				0.16	
	•	tn of Gasoline				0.217	
	Vehicle Refuelling						
	Uncontrolled	m <sup>3</sup> of Gasoline				1.4	
		tn of Gasoline				1.894	
	Balanced Vapor Filling	m <sup>3</sup> of Gasoline				0.212	
		tn of Gasoline				0.287	

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS	UNIT (U)	TSP	\$0 <sub>2</sub>	NO <sub>×</sub>	CO	VQC	
			kg/U	kg/U	kg/U	kg/U	kg/ü	kg/U

#### MAJOR DIVISION 7. TRANSPORT, STORAGE AND COMMUNICATION

### 711 Land Transport<sup>69</sup>

Light Duty Gasoline Powered Cars <3.5 tn

Evaporative Emissions 70
Hot Soak Emissions 71

HAC SANK CHIISSIAHS	
Cars with Carburettors	1000 km
Cars with Fuel Injection	1000 km
Running Losses	1000 km
Diurnal Losses	

9.4/L<sub>trip</sub> 0.7/L<sub>trip</sub> 0.1 to 1.

Uncontrolled Evaporative Controls<sup>72</sup>

Car\*yr Car\*yr 2.635

<sup>(</sup>b) The relevant emission factors depend on ambient temperature and on gasoline volatility. To account for these effects, the listed factors should be multiplied by appropriate "correction factors". As a guidance for the choice of the latter, the applicable "correction factors" for the EC countries are given below:

	Diurnal	Hot Soak	Running
	Losses	Emissions	Losses
Belgium, France, Luxembourg	1.0	0.9	0.9
Portugal, Spain	1.3	0.8	0.8
Greece, Italy	2.1	1.2	1.2
Ireland, U.K.	2.5	2.2	2.0
Denmark, Germany, Netherlands	1.0	1.0	1.0

<sup>(</sup>c) Estimates of evaporative emissions based on the listed factors are considered high. An alternative model allowing assessment of evaporative emissions as function of the climatic conditions and Gasoline volatility is given in Section 3.3.3.

<sup>69. (</sup>a) "S" is the weight percent of sulfur in the fuel. Typical values for Gasoline are 0.039% to 0.15% & for Diesel 0.2% to 0.5%.

<sup>(</sup>b) "P" is the average Lead content of the Gasolines used in gr/lt. In Unleaded Gasoline Lead concentrations are low (<0.013 gr/lt), while typical values in Premium Gasolines are 0.15 to 0.4 gr/liter.

<sup>70. (</sup>a) The evaporative emissions can be divided into the Running Losses (occurring while the vehicle is being driven), the Hot Soak Losses (evaporation of fuel, mainly from the carburettor bowl and tank, each time the vehicle stops with hot engine) and Diurnal Losses (expansion and emission of vapor, mainly from fuel tank, due to the daily diurnal temperature variations).

<sup>71. &</sup>quot;L<sub>trip</sub>" is the average distance, in km, a car is driven each time its engine starts.

<sup>72.</sup> Evaporative controls employ canisters filled with activated carbon, to which all fuel system vents are connected. Any diurnal or hot soak VOC emissions will thus be absorbed by the carbon and retained in the canister. The carbon is purged of VOC during driving by drawing air back through the canister and into the engine, where it is burnt.

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS		(ט) דוַאנ	TSP kg/U	SO <sub>2</sub> kg/U	NO <sub>X</sub> kg/U	co kg/U	<b>V</b> OC kg/U		l kg/U
	Exhaust Emissions <sup>73</sup>									
	Car Production Period up to 1971									
	Urban Driving									
	Engine < 1400 cc		1000 km	0.07	1.9\$	1.64	45.6	3.86	Рb	0.13P
		tn	of Fuel	0.74	205	17.29	480.6	40.69	РЬ	1.35P
	Engine 1400-2000 cc		1000 km	0.07	2.22\$	1.87	45.6	3.86	РЪ	0.15P
		tn	of Fuel	0.63	20S	16.87	411.6	34.85	Рb	1.35P
	Engine > 2000 cc		1000 km	0.07	2.748	2.25	45.6	3.86	Pb	0.19P
		tn	of Fuel	0.51	208	16.42	332.8	28.17	РЬ	1.35P
	Suburban Driving									
	Engine < 1400 cc		1000 km	0.05	1.15\$	2.01	25.13	2.03	Pb	0.08P
		tn	of Fuel	0.87	<b>20</b> S	35.01	437.4	35.32	Pb	1.35P
	Engine 1400-2000 cc		1000 km	0.05	1.48	2.51	25.13	2.03	Pb	0.09P
		tn	of Fuel	0.71		35.91			РЬ	1.35P
	Engine > 2000 cc		1000 km	0.05	1.668	3.03	25.13	2.03	Pb	0.11P
		tn	of Fuel	0.60	20\$	36.50	302.5	24.43	Рb	1.35P
	Highway Driving									
	Engine < 1400 cc		1000 km	0.05			16.66		Рþ	0.08P
		tn	of Fuel	0.83		33.59			Pb	1.35P
	Engine 1400-2000 cc		1000 km		1.498		16.66		Pb	0.10P
		ŧn	of Fuel	0.67		42.06			Pb	1.35P
	Engine > 2000 cc		1000 km			3.59			Pb	0.12P
		tn	of Fuel	0.55	20\$	39.64	183.7	14.55	ΡЪ	1.35P
	Car Production Period 1972-1977									
	Urban Oriving									
	Engine < 1400 cc		1000 km		1.668		33.42		Pb	0.119
		tn	of Fuel	0.84		19.75			Pb	1.35P
	Engine 1400-2000 cc		1000 km		1.925		33.42		₽b	0.13P
		tn	of Fuel	0.73		19.43			Pb	1.35P
	Engine > 2000 cc		1000 km			2.25			Pb	0.15P
		tn	of Fuel	0.64	205	20.42	303.3	27.65	РÞ	1.35P
	Suburban Driving						10.00		ο.	0.000
	Engine < 1400 cc		1000 km					1.51	Pb	0.06P
		tn	of Fuel	1.06		42.73			₽b	1.35P
	Engine 1400-2000 cc	ين ش	1000 km			2.51		1.51 27.03	Pb Pb	0.08P 1.35P
	Familia > 2000 aa	τn	of Fuel 1000 km	0.90		3.03			Pb	0.08P
	Engine > 2000 cc		of Fuel	0.81				24.26	Рb	1.35P
	Highway Dairing	ţn	OI FOET	U.01	243	40.04	6/3.6	<u>.</u> 4.40	1.11	1.00
	Highway Driving		1000 km	0.05	ስ ዕደና	2 N2	10 00	1.19	Рb	O.07P
	Engine < 1400 cc	4-						24.13	Pb	1.35P
		τn	of Fuel	1.02	203	41.10	400.0	₹4 - T3		1.55

The emission factors listed are based on a mean ambient temperature of 20  $^{\rm o}{\rm C}$  & on the 73. (a) following assumptions: For Urban Driving: Av speed\* 25 km/h; Av trip length = 8 km; Cold/hot starts: 75/25

For Suburban Driving: Av speed= 60 km/h; Av trip length =12 km; Cold/hot starts: 75/25 For Highway Driving: Av speed=100 km/h; Av trip length >20 km; Cold/hot starts: 75/25

Use Model of Section 3.3 for emissions under local climatic & driving conditions. (b)

Model for Air Emission Inventories and Controls - Cont'd

SIC#	PROCESS	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>X</sub> kg/U		V0C kg/U		kg/U
	5	1000 (	0.05	1 100	3 13	10 00	1 10	Рb	0.08P
	Engine 1400-2000 cc	1000 km tn of Fuel	0.05	1.195		19.98 335.1		Рb	1.35P
	Engine > 2000 cc	1000 km		1.34\$		19.98		₽b	0.09P
	Engine > 2000 00	tn of Fuel	0.75			298.7		Рb	1.35P
	Car Production Period 1978-1980 Urban Driving				•••				
	Engine < 1400 cc	1000 km	0.07	1.39\$	1.50	28.44	2.84	Pb	0.09P
	<u>_</u>	tn of Fuel	1.00	20\$	21.65	410.0	40.93	Pb	1.35P
	Engine 1400-2000 cc	1,000 km	0.07	1.68\$		28.44	2.84	Рb	0.119
	•	tn of Fuel	0.83	208	20.47	337.6	33.70	Pb	1.35P
	Engine > 2000 cc	1000 km	0.07	2.135	1.97	28.44	2.84	Рþ	0.14P
		tn of Fuel	0.66	208	18.48	266.5	26.61	Pb	1.35P
	Suburban Driving								
	Engine < 1400 cc	1000 km	0.05	0.88\$	1.90	13.54	1.37	Pb	0.06P
		tn of Fuel	1.14	205	43.04	307.5	31.41	Pb	1.35P
	Engine 1400-2000 cc	1000 km	0.05	1.15		13.54		Pb	O.07P
		tn of Fuel	0.91			245.4		Pb	1.35P
	Engine > 2000 cc	1000 km		1.358		13.54		Pb	0.09P
		tn of Fuel	0.74	20S	36.86	201.1	20.34	Pb	1.35P
	Highway Driving		_						
	Engine < 1400 cc	1000 km		1.03\$		10.47		Pb	0.07P
	<b>.</b>	tn of Fuel	0.97			202.7		Pb	1.35P
	Engine 1400-2000 cc	1000 km		1.23\$		10.47		Pb Pb	0.08P 1.35P
	Fi 2000	tn of Fuel	0.81			170.2 10.47		Pb	0.10P
	Engine > 2000 cc	1000 km tn of Fuel	0.68			142.3		Pb	1.35P
	Car Production Period 1981-1984 Urban Driving	(1) (1) ( 1)	0.00	203	30.44	172.0	10.00		1.55
	Engine < 1400 cc	1000 km	0.07	1.395	1.58	23.40	2.84	РЬ	0.09P
	Lingthe 1 1400 00	tn of Fuel	1.00			337.3		Pb	1.35P
	Engine 1400-2000 cc	1000 km		1.685		23.40		Рb	0.112
	#11 <b>3</b> 1714	tn of Fuel	0.83			277.8		Pb	1.35P
	Engine > 2000 cc	1000 km				23.40		РЬ	O.14P
		tn of Fuel	0.66			219.3		Рb	1.35P
	Suburban Driving								
	Engine < 1400 cc	1000 km	0.05	0.889	1.98	9.26	1.37	Pb	0.06P
		tn of Fuel	1.14	20S	45.01	210.3	31.11	Pb	1.35P
	Engine 1400-2000 cc	1000 km	0.05	1.15	2.35	9.26	1.37	Pb	0.07P
		tn of Fuel	0.91				24.83	Pb	1.35P
	Engine > 2000 cc	1000 km					1.37	Pb	0.099
		tn of Fuel	0.74	20\$	44.98	137.5	20.34	Pb	1.35P
	Highway Driving								
	Engine < 1400 cc	1000 km		1.035			1.00	Pb	0.07P
		tn of Fuel	0.97	_			19.45	Pb	1.35P
	Engine 1400-2000 cc	1000 km				6.71		Pb	0.08P
	F	tn of Fuel	0.81				16.33	Pb	1.35P
	Engine > 2000 cc	1000 km					1.00	Pb Pb	0.10P
		tn of Fuel	0.68	20S	ь <b>и.6</b> 8	91.11	13.65	Pb	1.35P

Model for Air Emission Inventories and Controls - Cont'd

SIC# Pi	ROCESS	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U	CO kg/U	VOC kg/U		kg/U
	Car Production Period 1985-19	92							
	Urban Driving	<u>.                                    </u>							
	Engine < 1400 cc	1000 km	0.07	1.275	1.50	15.73	2.23	Pb	0.09P
	Eligino 1 1400 00	tn of Fuel	1.10		23.75			Ρb	1.35P
	Engine 1400-2000 cc	1000 km	0.07	1.625	1.78	15.73	2.23	РЬ	0.11P
	<u> </u>	tn of Fuel	0.86	20\$	22.02	194.7	27.65	Рb	1.35P
	Engine > 2000 cc	1000 km	0.07	1.85\$	2.51	15.73	2.23	Pb	0.13P
	<b>-</b>	tn of Fuel	0.76	20S	27.11	169.7	24.09	Pb	1.35P
	Suburban Driving								
	Engine < 1400 cc	1000 km	0.05	0.80\$	2.06	6.99	1.05	Pb	0.05P
	- <del>-</del>	tn of Fuel	1.25	205	51.26	173.7	26.11	Pb	1.35P
	Engine 1400-2000 cc	1000 km	0.05	0.978	2.31	6.99	1.05	РЬ	0.07F
	•	tn of Fuel	1.03	205	47.62	144.3	26.68	PЬ	1.35F
	Engine > 2000 cc	1000 km	0.05	1.17\$	3.14	6.99	1.05	РЬ	0.08F
	•	tn of Fuel	0.85	205	53.81	119.9	18.02	Рb	1.356
	Highway Driving								
	Engine < 1400 cc	1000 km	0.05	0.968	2.85	3.56	0.69	Рb	0.07
	·	tn of Fuel	1.04	205	59.18	73.9	14.26	Pb	1.35
	Engine 1400-2000 cc	1000 km	0.05	1.085	3.10	3.56	0.69	Pb	0.07
	·	tn of Fuel	0.93	208	57.21	65.85	12.71	РÞ	1.35
	Engine > 2000 cc	1000 km	0.05	1.36\$	4.09	3.56	0.69	PЬ	0.09
		tn of Fuel	0.74	20S	60.29	52.5	10.13	Pb	1.35
	Cars with Uncontrolled 3-way	Catalytic Convert	ers <sup>74</sup>						
	Urban Driving								
	Engine < 1400 cc	1000 km	0.07		1.31				
		tn of Fuel	0.80		15.13				
	Engine 1400-2000 cc	1000 km	0.07	2.059			0.60		
		tn of Fuel	0.68	205	10.97	62.9			
	Engine > 2000 cc	1000 km		2.359		6.46			
		tn of Fuel	0.60	209	9.56	54.9	5.1		
	Suburban Driving								
	Engine < 1400 cc	1000 km	0.0	5 1.105					
	•	tn of Fuel	0.93				11.10		
	Engine 1400-2000 cc	1000 km			1.43				
		tn of Fuel			23.19				
	Engine > 2000 cc	1000 km			1.43				
		tn of Fuel	0.68	3 209	19.27	40.0	3.73		
	Highway Driving		_			. <u>.</u>			
	Engîne < 1400 cc	1000 km			3 2.23				
		tn of Fuel			33.80				
	Engine 1400-2000 cc	1000 km			3 1.83				
		tn of Fuel			3 26.56				
	Engine > 2000 cc	1000 km			5 1.83				
		tn of Fuel	0.5	8 20:	S 21.16	3 15.0	1.92		

Hot & Cold Urban Driving Cycle and Extra Urban Driving Cycle emission and fuel consumption 74. measurements of TNO (TNO, 1990), modelled by A. Economopoulos.

Model for Air Emission Inventories and Controls - Cont'd

# PROCESS	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U	NO <sub>x</sub> kg/U		VOC kg/U		kg/l
Cars with Controlled 3-w	y Catalytic Converter	<sub>\$</sub> 75						
Urban Driving								
Engine < 1400 c	1000 km	0.07	1.61\$	0.20	1.71	0.24		
	tn of Fuel	0.87	20\$	2.46	21.21	2.95		
Engine 1400-2000 c	1000 km	0.07	1.94\$	0.25	1.49	0.19		
	tn of Fuel	0.72	20\$	2.57	15.39	1.93		
Engine > 2000 c	1000 km	0.07	2.238	0.25	1.49	0.19		
	tn of Fuel	0.63	205	2.24	13.41	1.68		
Suburban Driving								
Engine < 1400 c	1000 km		1.025	0.33	1.33	0.19		
	tn of Fuel	0.98	20\$	6.52	25.96	3.69		
Engine 1400-2000 co	1000 km		1.165	0.34	1.04	0.13		
	tn of Fuel	0.86	208	5.79	17.88	2.19		
Engine > 2000 co	1000 km	0.05	1.40\$		1.04	0.13		
	tn of Fuel	0.71	20\$	4.81	14.87	1.82		
Highway Oriving								
Engine < 1400 ce	1000 km	0.05	1.22S	0.24	0.90	0.11		
	tn of Fuel	0.82	20S	3.89	14.76	1.76		
Engine 1400-2000 co	1000 km	0.05	1.305	0.25	0.54	0.06		
	tn of Fuel	0.77	20\$	3.91	8.29	0.95		
Engine > 2000 co	1000 km	0.05	1.63\$	0.25	0.54	0.06		
	tn of Fuel	0.61	20S	3.12	6.60	0.76		
Heavy Duty Gasoline Powered Vel	icles > 3.5 tn							
Urban Oriving	1000 km	0.4	4.58	4.5	70	7	Рb	0.31F
	tn of Fuel	3.5	20S	20	300	30	Рb	1.35
Suburban Driving	1000 km	0.45	3.7\$	7.5	55	5.5	Рb	0.25
	tn of Fuel	2.4	20\$	40	300	30	Pb	1.35
Highway Driving	1000 km	0.6	3.35	7.5	50	3.5	Pb	0.22
	tn of Fuel	3.6	205	45	300	20	Pb	1.35
Light Duty Diesel Powered Vehic	les < 3.5 tn <b>76</b>							
Urban Driving	1000 km	0.2	1.16S	0.7	1	0.15		
-	tn of Fuel	3.5	205	12	18	2.6		
Suburban Driving	1000 km	0.15	0.84S	0.55	0.85	0.4		
	tn of Fuel	3.5	20S	13	20	9.5		
Highway Driving	1000 km	0.3	1.35	1	1.25	0.4		
	tn of Fuel	4.7	205	15	19.	6.1		

<sup>75.</sup> Hot & Cold Urban Driving Cycle and Extra Urban Driving Cycle emission and fuel consumption measurements by TNO (TNO, 1990), modelled by A. Economopoulos.

TSP: 1.6 CO: 1.1 VOC: 10.0 NOx: 0.9

<sup>76. (</sup>a) In the case of a fleet of old vehicles with poor state of maintenance and poor fuel quality, the emission factors listed need to be multiplied as follows:

<sup>(</sup>b) Based on the Central Bureau of Statistics, Netherlands, the TSP (Smoke) emissions from Urban, Suburban and Highway driving are 1.1, 0.55 and 0.5 kg/1000 km respectively.

Model for Air Emission Inventories and Controls - Cont'd

PROCESS	UNIT (U)	TSP SO <sub>2</sub> kg/U kg/U	kg/U	C0 kg/U ——	VOC kg/U	kg/
	2.5.46.4-77					
Heavy Duty Diesel Powered Vehicles		0 0 4 200	11.8	6.0	2.6	
Urban Driving	1000 km tn of Fuel	0.9 4.29\$ 4.3 20\$		28.	12.	
PL	1000 km	0.9 4.15S		2.9	0.8	
Suburban Oriving	tn of Fuel	4.3 20\$			4.	
Highway Driving	1000 km	0.9 4.15\$		2.9	0.8	
nighway bi iving	tn of Fuel	4.3 20S		14.	4.	
Heavy Duty Diesel Powered Trucks >	16 tn <b>78</b>					
Urban Driving	1000 km	1.6 7,268	18.2	7.3	5.8	
•	tn of Fuel	4.3 205	50.	20.	16.	
Suburban Driving	1000 km	1.6 7.435	24.1	3.7	3.0	
	tn of Fuel	4.3 205	65.	10.	8.	
Highway Driving	1000 km	1.3 6.19	19, 8	3.1	2.4	
	tn of Fuel	4.3 209	65.	10.	8.	
Heavy Duty Diesel Powered Buses >	16 tn <b>79</b>					
Urban Driving	1000 km	1.4 6.63		6.6	5.3	
	tn of Fuel	4.3 209		20.	16.	
Suburban Driving	1000 km	1.2 5.619		2.8	2.2	
	tn of Fuel	4.3 209			8.	
Highway Driving	1000 km	0.9 6.119		2.1	1.7	
	tn of Fuel	4.3 209	65.	10.	8.	
Light Duty LPG Powered Vehicles <	3.5 tn <b>80</b>					
Without Catalytic Converters						
Urban Driving	1000 km		1.24		1.35	
	tn of Fuel		21	56	23	
Suburban Driving	1000 km		1.3		1.15	
	tn of Fuel		29	39		
Highway Driving	1000 km		2.75	1.15 21		
	tn of Fuel		51	21	19	
With 3-way Controlled Catalytic			0.3	1 0	0.7	
Urban Driving	1000km tn of Fuel		0.3 4.4	1.9 28		
Motorcycles						
Engines < 50 cc 2-Stroke	1000 km	0.12 0.36	5 0.05	10	6	
	tn of Fuel	6.7 20				

Based on the Central Bureau of Statistics, Netherlands (1983), the TSP (Smoke) emissions from 77. Urban, Suburban and Highway driving are 5.4, 2.0 and 1.4 kg/1000 km respectively.

<sup>78.</sup> As above.

Based on the Central Bureau of Statistics, Netherlands (1983), the TSP (Smoke) emissions from 79. Urban, Suburban and Highway driving are 5.1, 1.8 and 1.0 kg/1000 km respectively.

The listed emission factors are valid only for properly converted (into LPG use) and well ad-80. justed engines. Otherwise, the emission factors are in the same order as these for Light Duty Gasoline Powered Vehicles < 3.5 tn.

Model for Air Emission Inventories and Controls - Cont'd

I SIC#	PROCESS	UNIT (U)	TSP kg/U		NO <sub>x</sub> kg/U		VOC kg/U		kg/U
	Engines > 50 cc 2-Stroke	1000 km	0.12	0.68	0.08	22	15		
		tn of Fuel	4	20\$	2.7	730	500		
	Engines > 50 cc 4-Stroke	1000 km		0.765	0.30	20	3		
		tn of Fuel		205	8	525	80		
	Fugitive Dust from Vehicle Traffic <sup>81</sup>								
	Unpaved Roads <sup>82</sup>								
	Plant Roads								
	Copper Smelting	1000 km	12.5f						
	Iron & Steel Production	1000 km	5.9f						
	Sand & Gravel Processing	1000 km	3.5f						
	Stone Quarrying/Processing	1000 km	10.4f						
	Coal Mining / Access Road	1000 km	3.8f						
	Coal Mining / Haul Road	1000 km	6.2f						
	Coal Mining / Scraper Road	1000 km	12.5f						
	Rural Roads								
	Gravel	1000 km	3.7f						
	Dirt	1000 km	21.f						
	Crushed Limestone	1000 km	7.1f						
	Paved Roads <sup>83</sup>								
	City Roads <sup>84</sup>								
	Local Streets (Width<10m)								
	< 500 vehicles/d	1000 km	15					РЬ	0.018
	Collector Streets (Width>10m)								
	500-10000 vehicles/d	1000 km	10					РЬ	0.018
	Major Streets / highways							•	
	>10000 vehicles/d	1000 km	4.4					₽b	0.018

<sup>81.</sup> Emission factors account for entrained particles with diameters < 30  $\mu$ .

<sup>82. (</sup>a)  $f = S(W^{0.7})(w^{0.5})$ , where S is the average vehicle speed in km/hr. W is the average vehicle weight in tons, and w is the average number of wheels per vehicle.

<sup>(</sup>b) The listed emission factors apply per 1000km driven in dry weather (during days with < 0.25 mm of precipitation).

<sup>(</sup>c) The emission factors for PM $_{15}$  or PM $_{10}$  particles are 50% and 36% respectively of the listed TSP emission factors (PM $_{10}$  & PM $_{15}$  are particles with diameters <10 & <15  $\mu$  respectively).

<sup>(</sup>d) Periodic (monthly) application of petroleum resin products over a dust control season (e.g. four summer months) yields typical control efficiencies of the order of 60% for the TSP and 70% for PM10 particles.

<sup>83.</sup> The emission factors for  $PM_{15}$  or  $PM_{10}$  particles are 40% & 36% respectively of the listed TSP emission factors for local and collector streets, 45% & 41% respectively of the listed TSP emission factors for major streets/highways and 60% & 54% respectively for Freeways/Expressways ( $PM_{10}$  &  $PM_{15}$  are particles with diameters <10 & <15  $\mu$  respectively).

<sup>84.</sup> Limited data suggest control efficiencies of 34% and 37% for  $PM_{10}$  particles from Vacuum Sweeping and Improved Vacuum Sweeping respectively ( $PM_{10}$  are particles with aerodynamic diameter < 10  $\mu$ ).

# Model for Air Emission Inventories and Controls - Cont'd

I SIC#	PROCESS '	UNIT (U)	TSP kg/U	\$0 <sub>2</sub> kg/U		CO kg/U	VOC kg/U		kg/U
	Freeways / Express Ways							Pb	0.018
	>50000 vehicles/d	1000 km	0.35					FU	Ų. UIG
	Industrial Roads <sup>85</sup>	1000 km	120						
712	Water Transport								
	Ships in Berth86,87								
	Motorships	Ship-days in berth	6.8	136S	90.7	0.036	4.1		
	Steamships	Ship-days in berth	7.5	19.5	22. <b>7</b>	20.8	14.9		
713	Air Transport								
	Landing and Take off of Aircraft								
	Typical Carrier <sup>88</sup> Aircraft Refuelling	Landing+Take off	0.99	1.5	14.2		20.4		
	Jet Naphtha	<sub>m</sub> 3					0,40		
	age mapricia	tn					0.54		

# 719 Services Allied to Transport

### 7192 Storage and Warehousing

Grain Elevators 3.7 Country Elevators 4.8 tn Inland Terminal Elevators 5.0 Export Elevators

"S" is the weight percent of sulfur in the fuel used 86.

For PM<sub>15</sub> particles, limited data suggest control efficiencies of up to 58% for vacuum sweep-85. ing (46% for TSP), (69-0.231\*V)% efficiency for Water Flushing and (96-0.263\*V)% efficiency for Water Flushing followed by Sweeping, where V is the number of vehicle passes since application.

The number of steamships and motorships days-in-berth, if not directly known, can be computed 87. from the number of ship calls per year and the average mooring time. Typical mooring times in hours are as follows: 6 for passenger ships, 45 for freighters and general ships, 24 for container vessels < 40000 GRT, 36 for container vessels > 40000 GRT, 40 for bulk transport vessels < 40000 GRT, 50 for bulk transport vessels > 40000 GRT, 36 for tankers < 40000 GRT, 48 for tankers > 40000 GRT.

Given factors are overall averages for a typical airport, Economopoulos (1980). 88.

# $\label{thm:model} \mbox{Model for Air Emission Inventories and Controls - Cont'd}$

SIC# PROCESS		UNIT (U	) TSP kg/U		NO <sub>x</sub> kg/U	C0 kg/U	VOC kg/U	<b>.</b>	kg/U
MAJOR DIVISION 9. COMMUNITY, S	OCIAL AND PERSO	<u>DNAL SERVI</u>	<u>:ES</u>						
920 Sanitary and Similar Servi	es								
Municipal/Domestic Type of	Wastes								
Open Burning									
Municipal Refuse		tr	. 8	0.5	3.	42.	21.5		
Automobile Components	89	tr		0.0	2.	62.			
Municipal Waste Combusti		₩,		0.0	۵,	02.	71.V		
Mass-Burn Combustors									
Uncontrolled		tr	19	0.85	1.8	1 10	. 0532	Pb	0.09
ESP or FF		tr		0.85	1.8		. 0532	Pb	0.011
Modular Starved-Air (	ombustors		V.15	0.00	1.0	1.10	. 0332	LD	0.011
Uncontrolled	•	tr	0.95	0.85	2.2	0.170	0532	₽b	0.06
ÉSP or FF		tr			2.2	0.170		Pb	0.001
Refuse Derived Fuel (	RDF) Fired Com		0.010	0.00	•	V.170	, 0002	' 🌣	0.001
Uncontrolled	•	tn	40	0.85	2.5	1 80	. 0532	Pb	0.065
ESP or FF		tn		0.85	2.5		. 0532	Pb	0.014
Industrial / Commercial	Refuse Combust			*****		*.00	, 4402	1 10	0.014
Multiple Chamber/Unco		tn	3.5	1.25	1.5	5.0	1.5		
Single Chamber / Unco		tn		1.25	1.0	10.0	7.5		
Trench / Uncontrolled							,		
Wood		tn	13	0.1	4.0				
Rubber Tires		tn	138		,,,,				
Municipal Refuse		tn	37	2.5					
Pathological Wastes									
Uncontrolled		tn	8.0	0.	3.0	0.	0.		
Sewage Sludge Incinerators									
Multiple Hearth Incinera	tors								
Uncontrolled	tn of dr	ied sludge	42	10	5.5	36	3.15	Pb	0.05
Scrubber <sup>90</sup>	tn of dr	ied sludge		2.	2.5		3.15	Pb	0.02
Fluidized Bed Incinerator	'S	_							
Uncontrolled	tn of dri	ied sludge	?	10.	4		1.16	Pb	7
Scrubber		ed sludge	0.33	2.	2.2	2	1.16	РЬ	0.03
Electric Infrared Incine:	ators								
Uncontrolled	tn of dri	ed sludge	4	10.	4				
Scrubber	to of dri	ed sludge	1	2.	3				
52 Laundries, Laundry Services,	and Cleaning	and Dyeing	Plants						
Dry Cleaning	(Comit	a)*(year)					0.6		

<sup>89.</sup> Upholstery, belts, hoses and tires burned together.

<sup>90.</sup> Impingement, Venturi and/or cyclone scrubber.

# Working Table for Assessing the Air Emission Loads 3.2.3 Data and Calculations Sheet for Air Emissions (# \_\_\_\_ of \_\_\_)

		SOURCE	T 5	SP .	so	)2	, NC	) <sub>x</sub>	ÇC	)	V	С	(	THER	
SOURCE	UNIT (U)	SIZE 10 <sup>3</sup> U/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Pollu tant	Fact kg/U	Load tn/y
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			#	<u> </u>	#	<u> </u>		†	#	<u> </u> 				†	<u> </u>
		#		+	#	†	   	<u> </u> 	#	+	<u> </u>	-			-
				·   		-	#		# .	+		ļ ·	#	<u> </u>	+
	-   -   -			+		†		<u> </u>		+		+		ļ.	+
	1			1		†		+		†	+	+		†	†
- Sub Total (f	rom Pre	SFent SF	l meet)	]		-	1		-					1	
See interest fi	7 1 1	,	•	-	#	+		†	#	1		†	1		†
Sub Yotal (f	rom Pro	evious S	Sheets	3		†		†		1	#	†	+		<u> </u>
				}		†		†	#	†		†	#		1
Sub Total	•				1										
Note: U =Unit Fact=Waste	Load F	actor						Ţ		1					+

#### 3.2.4 Example

## The Problem:

A lime manufacturing plant operating within our study area is to be surveyed. Determine the data requirements, collect the necessary information and assess the emission loads:

## Solution of the Problem:

- 1. From Appendix II we find Lime, a non metallic mineral product, classified under the Standard Industrial Classification (SIC) Code # 369. Use of Appendix II facilitates the finding of a particular activity in Section 3.2.3.
- 2. From Section 3.2.3 inspection of the Lime manufacturing emissions model yields the following data input requirements:
  - Are the kilns using coal or other type of fuel? (a)
  - (b) If Coal is used:
    - Quantity of Coal used (tn/year if annual emission es-(i) timates are desirable)
    - Coal Storage (Open piles, Semi-enclosed piles, Com-(ii)partments, or Silos)
    - (iii) Control system for the Coal crushing and screening
    - (uncontrolled or Fabric filter)
      The system used for Coal grinding (Semi Direct, Di-(iv) rect, or Indirect fired)
    - (v) If Indirect fired grinding systems are used what controls are installed (uncontrolled or Fabric Filter).
  - Quantity of Lime Produced (tn/year if annual emission esti-(c) mates are desirable)
  - (d) Sulfur content of fuel used, in weight %. (for estimating the SO<sub>2</sub> emissions)
  - (e) Control system for the Raw material crushing and screening (uncontrolled or Fabric Filter)
  - (f) Storage of crushed material (Open or Semi-enclosed pile, Compartment or Silo)
  - Control for the raw material conveying system (uncontrolled (g) or Fabric filter)
  - Type of kiln used for the Raw material calcining (Vertical (h) shaft kiln, Vertical double inclined kilns, flow/counterflow regenerative kilns, ....)
  - (i) Controls used in the calcining kiln (Uncontrolled or controlled and in the latter case, which of the listed controls is used)
  - (j) Type of Lime cooler used (Grate, Planetary, Rotary or Vertical Shaft cooler)
  - (k) Control used in the Grate cooler (if used) (Uncontrolled, Cyclones, Multicyclones or Fabric Filter)

3. Assume that from the plant survey visit the following data were obtained in relation to the above questionnaire:

Coal is not used as fuel (a)

Lime production is 18,000 tn/year (c)

The sulfur content of the residue oil used is 4% (S = 4) (d)

Raw material crushing and screening is uncontrolled (e)

Crushed material is stored in open piles (f)

- Raw material conveying systems are uncontrolled (g) The calcining kiln is of the vertical shaft type (h) The calcining kiln is controlled by multicyclones (i)
- Lime cooling is by vertical shaft cooler (lower part of (j) kiln).
- The above plant survey data, along with the necessary information from the emission load model (see Section 3.2.2), can be inserted in the working Table given in Section 3.2.3. The latter can be used for computing the annual emissions from each major source within the lime manufacturing plant.

Table 3.2.4-1 shows how data and information can be entered and how emissions can be computed. It should be noted that in the Working Table the emission factors are expressed as kg/Unit, while the activity of each source is entered in 1000 Units/Year. As a result, multiplication of each emission factor by the source activity yields the emission load expressed in tons/year. For example, the TSP emission factor for the raw material conveying is 1.2 (kg TSP per ton of Lime) and the source activity is 18 (thousand tons of Lime production per year). Their multiplication yields 21.6 tons of TSP emissions per year.

Table 3.2.4-1 Example use of the working table of Section 3.2.3 Data and Calculations Sheet for Air Emissions (#  $_1$  of  $_1$ )

		SOURCE SIZE	1:	SP	Sí	<sup>0</sup> 2	N	0 <sub>x</sub>	C		l ·	oc		OTHER	
SOURCE	UNIT (U)		Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Pollu tant	Fact kg/U	Load tn/y
3692 Manufacture of	Cement	, Lime	& Pla	ıster											
Lime Manufacturing Raw Mat Storage Crush & Screening	- 1	18	0.16	2.9			-					-			_
Uncontrolled Crushed Mat Store	tn	18	1.5	27											
Open Piles   Raw Mar. Conveying		18	1.0	18		.				_		.		. ]	
Uncontrolled    		. 18	1.2	21.6	· .	. <b>.</b>	· •	_	.	-			 	- <b> </b>	.
M/cyclones Lime Packaging	tn	·	.	. #	.9*4	64.8	0.1	- 1.8	2.0	36		.		-	-
& Shipping	tn	18	0.12	2.3	.	<b>!!</b>		.	.	.	.	.		.	.
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	#	#	+	ii ii	-		+		-		1		-	-	i
} -	#	#	+		+	#	+	#	ļ	#	+				
Sub Total (fro	m Prese	 ent Shee	et)	35.3	-	64.8	-	1.8	-	36	-		1	}	
			-	#	†	#	+	#	+		†	#		+	#
Sub Total (from	m Previ	ious She	ets	#	<u> </u>	#	1		<u> </u>	#			•	Ţ	
Sub Total Note: U =Unit Fact=Waste Loa	ad Fact	or:			+		+	#			-	  - 		-	

Model for the Exhaust and Evaporative Emissions from LDGP 3.3 Vehicles Under Specific Driving, Climatic and Gasoline Volatility Conditions

#### 3.3.1 Introduction

Light Duty Gasoline Powered (LDGP) vehicles are the dominant source of NOx, CO and VOC emissions in most large urban areas. All three of the above pollutants are precursors to photochemical smog, which appears with increasing frequency and intensity in many urban regions and affects large populations.

Photochemical smog (ozone, nitrogen dioxide, peroxy acetyl nitrate and many other substances in small amounts) is formed through atmospheric reactions, under the influence of sunlight and heat, from the primary pollutants  $NO_x$ , CO and VOC. The speed of the reactions leading to smog formation increases significantly during the summer, when both the intensity of the sunlight and the temperatures are elevated.

The  $\mathrm{NO}_{\mathrm{X}}$ , CO and VOC emission factors are considerably dependent on the daily mean temperature and on the driving patterns (average vehicle speed, percent of engine starts with cold engine, and mean length of each trip). During the peak ozone months all of the above parameters may deviate considerably from their annual averages (temperature is obviously higher, while the driving patterns are often affected by the summer vacations and/or tourism) and may deviate even further from the typical conditions on which the derivation of the emission factors listed in Section 3.2.2 was based. Yet, the calculation of the seasonal emissions may be important if the problem of photochemical pollution is to be addressed.

Because of the particular importance of LDGP vehicle emissions in urban pollution, their significant regional and seasonal variability, and their special importance during the ozone peak season, two models are presented in Sections 3.3.2 and 3.3.3 that allow users to custom fit the emission factors on the basis of the local and seasonal ambient conditions and driving patterns. The model in Section 3.3.2 focuses on exhaust emissions, while that of Section 3.3.3 on Evaporative VOC ones.

- The Exhaust Emissions Model 3.3.2
- Description of the Model 3.3.2.1

The basic input for our exhaust emissions model for LDGP vehicles is from the original ECE CORINAIR report (1980), as well as from the Exhaust emission measurements provided by TNO (1989-1990). From the former, information about exhaust emissions from conventional non catalytic cars was obtained, while from the latter, laboratory measurements relevant to the catalytic cars were used.

Based on the TNO measurements, an exhaust emissions and fuel consumption model for catalytic cars was developed (Economopoulos, 1992), which supplemented the exhaust emissions information for conventional cars provided by the ECE CORINAIR report.

The above extended model, which is capable of predicting the emissions for all types of LDGP vehicles, was used in the analysis of the functional dependence of the exhaust emissions on all parameters that are known to exert a significant effect (daily or seasonal mean temperature, the average vehicle speed, the fraction of cold engine starts,  $f_{\rm CS}$ , and mean length of each trip, L, the age of a conventional vehicle or the type of catalytic system used, and the cylinder displacement of its engine). The end product of this analysis is described by the following relations (Economopoulos, 1992):

$$e = e^{hot} \left[ 1 + f_{cs} \frac{m_{0.75} - 1}{0.75} \right],$$
 (3.3.2.1-1)

where

and

The hot-start NO $_{\rm X}$ , CO, VOC and fuel consumption factor ehot can be conveniently obtained as a function of the average speed, cylinder displacement, and year of car manufacture from the graphs in Figures 3.3.2.1-1 to 3.3.2.1-4. These factors represent the emissions and the fuel consumption for the distances traveled while the car engine is hot (cooling water temperature above 70 °C).

While the car runs with cold engine its emissions and its fuel consumption are different from the hot-start ones. This difference is especially pronounced in the case of cars equipped with catalytic converters. As most of the times the cars are ignited with cold engines, and run a fair fraction of their average trip before their engine gets hot, the hot start emission and fuel consumption factor  $e^{hot}$  need to be corrected so as to compensate for the cold start effects. This correction is achieved by Equation 3.3.2.1-1 through the use of the emission or fuel consumption factor multiplier m<sub>0.75</sub>.

If  $f_{\rm CS}$ =0.75 (meaning that in 75% of the cases the cars are ignited with cold engines and in 25% of the cases with hot engines) then, from Equation 3.3.2.1-1 we obtain:

$$e = (e^{hot})(m_{0.75})$$
 (3.3.2.1-4)

The value of  $f_{\text{CS}}$ =0.75 is considered reasonable and, in the absence of local data, it can be accepted. In that case,  $m_{0.75}$  is a direct multiplier of  $e^{\text{hot}}$  according to Equation 3.3.2.1-4 and this justifies its name (emission or fuel consumption factor multiplier).

For the computation of the actual (cold-start compensated) emission and fuel consumption factors, e, the values of m<sub>0.75</sub> are needed. These can be conveniently obtained through the graphs in Figures 3.3.2.1-5 to 3.3.2.1-8 for  $NO_X$ , CO, VOC and fuel consumption, as a function of the daily, seasonal or annual temperature, the average length of each vehicle trip, L, and the technology used (conventional or catalytic).

In summary, for the estimation of the  ${\rm NO}_{\rm X},$  CO, VOC and fuel consumption factors we need information about the following:

Average speed

Cylinder displacement,

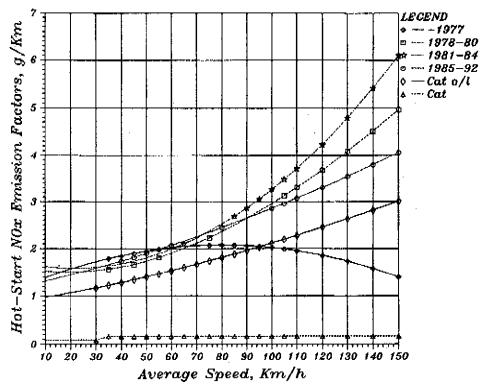
Year of manufacture for conventional cars or type of catalytic system used

Mean daily, seasonal or annual temperature,

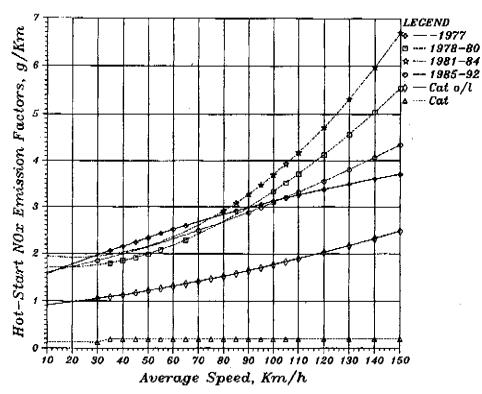
Average length of trip,

Technology type (conventional or catalytic)

Based on the above we obtain the values of  $e^{hot}$  and  $m_{0.75}$  for  $NO_x$ ,  $CO_x$ and VOC and fuel consumption using the diagrams of Figures 3.3.2.1-1 to 3.3.2.1-4 and 3.3.2.1-5 to 3.3.2.1-8 respectively. The above values of ehot and m $_{0.75}$  are inserted in Equation 3.3.2.1-1 to obtain the sought factors for NO $_{\rm X}$ , CO, and VOC emissions and fuel consumption.



Hot-start NOx emission factors for LDGP cars with < 1400 cc engines (Cat o/l = Figure 3.3.2.1-1a catalytic 3-way open loop. Cat = catalytic 3-way controlled)



Hot-start  ${
m MO}_{
m X}$  emission factors for LDGP cars with 1400-2000 cc engines (Cat o/l Figure 3.3.2.1-1b = catalytic 3-way open loop, Cat = catalytic 3-way controlled).

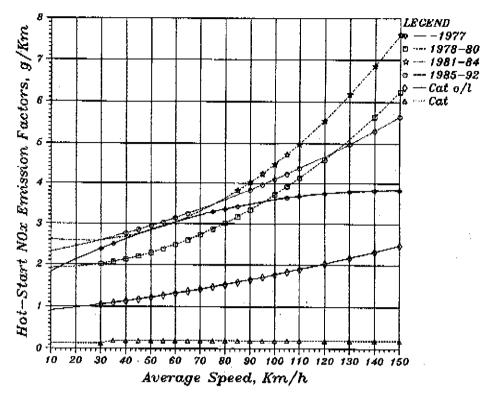


Figure 3.3.2.1-1c Hot-start NO<sub>x</sub> emission factors for LDGP cars with > 2000 cc engines (Cat o/1 = catalytic 3-way open loop, Cat = catalytic 3-way controlled)

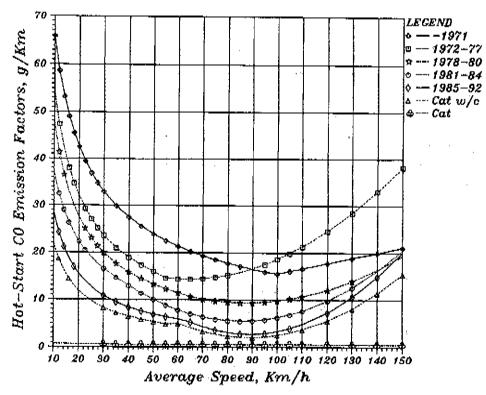
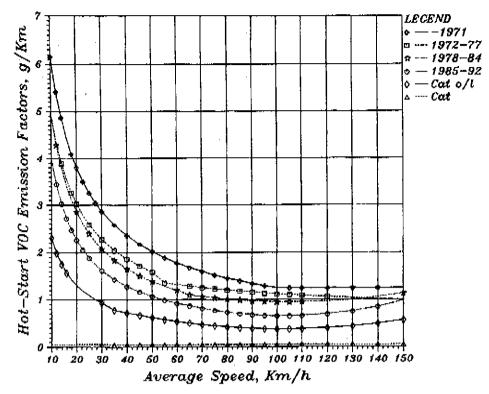
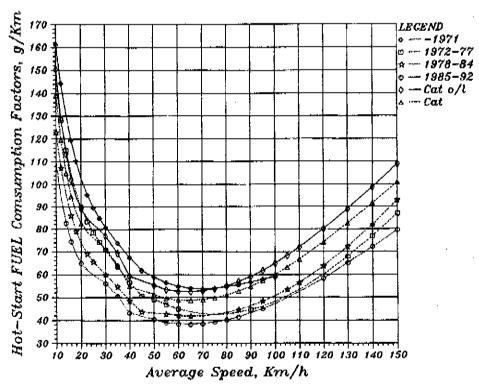


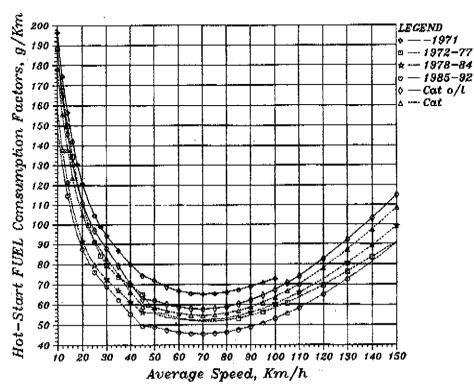
Figure 3.3.2.1-2 Hot-start CO emission factors for LDGP cars (Cat o/l = catalytic 3-way open loop, Cat = catalytic 3-way controlled)



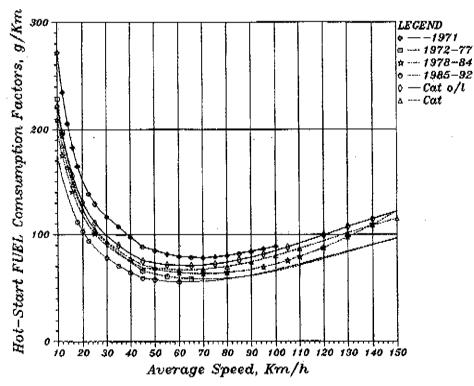
Hot-start VOC emission factors for LOGP cars (Cat o/1 = catalytic 3-way open Figure 3.3.2.1-3 loop, Cat = catalytic 3-way controlled)



Hot-start fuel consumption factors for LDGP cars with < 1400 cc engines (Cat o/) Figure 3.3.2.1-4a = catalytic 3-way open loop, Cat = catalytic 3-way controlled)



Hot-start fuel consumption factors for LDGP cars with 1400-2000 cc engines (Cat Figure 3.3.2.1-4b o/l = catalytic 3-way open loop, Cat = catalytic 3-way controlled)



Hot-start Fuel consumption factors for LDGP cars with > 2000 cc engines (Cat o/l Figure 3.3.2.1-4c = catalytic 3-way open loop, Cat = catalytic 3-way controlled)

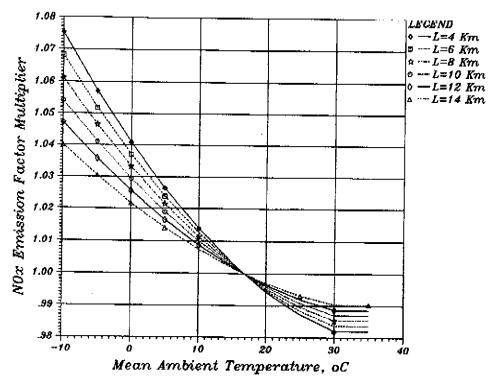


Figure 3.3.2.1-5a  $NO_X$  emission factor multiplier for conventional (non-catalytic) LOGP cars, as function of the average temperature and trip length

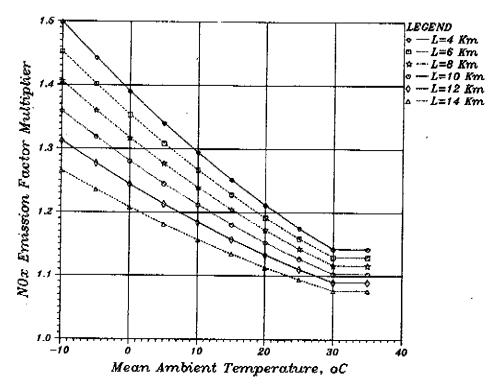
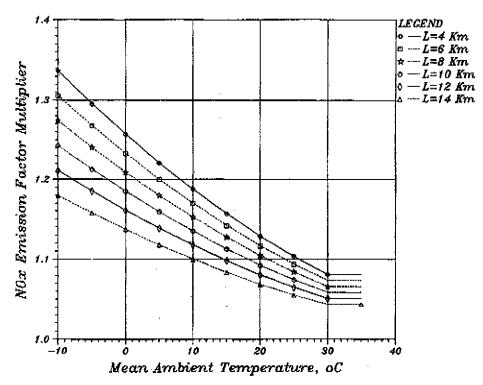
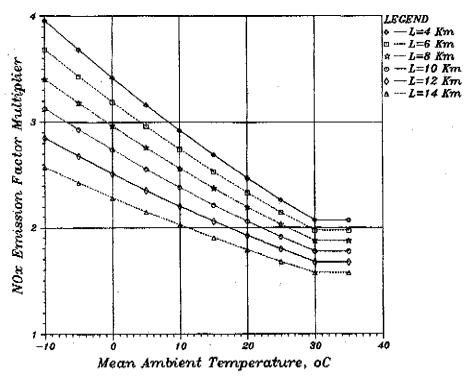


Figure 3.3.2.1-5b  $\cdot NO_x$  emission factor multiplier for LDGP cars with 3-way open loop catalyst and < 1400 cc engine, as function of the average temperature and trip length



NO, emission factor multiplier for LDGP cars with 3-way open loop catalyst and > Figure 3.3.2.1-5c 1400 cc engine, as function of the average temperature and trip length



 $\mathrm{NO}_{\mathrm{x}}$  emission factor multiplier for LDGP cars with 3-way controlled catalyst and Figure 3.3.2.1-5d < 1400 cc engine, as function of the average temperature and trip length

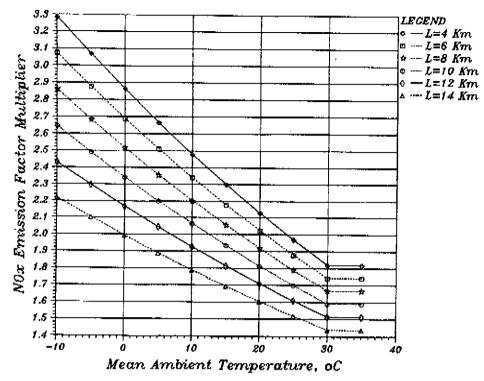


Figure 3.3.2.1-5e  ${
m NO}_{
m x}$  emission factor multiplier for LDGP cars with 3-way controlled catalyst and > 1400 cc engine, as function of the average temperature and trip length

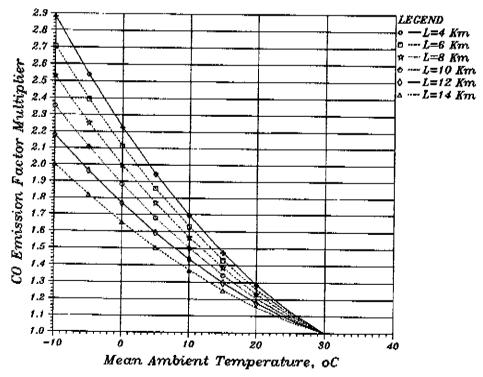


Figure 3.3.2.1-6a CO emission factor multiplier for conventional (non-catalytic) LDGP cars, as function of the average temperature and trip length

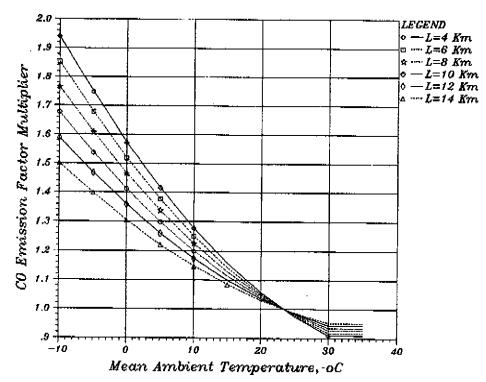


Figure 3.3.2.1-6b CO emission factor multiplier for LDGP cars with 3-way open loop catalyst and < 1400 cc engine, as function of the average temperature and trip length

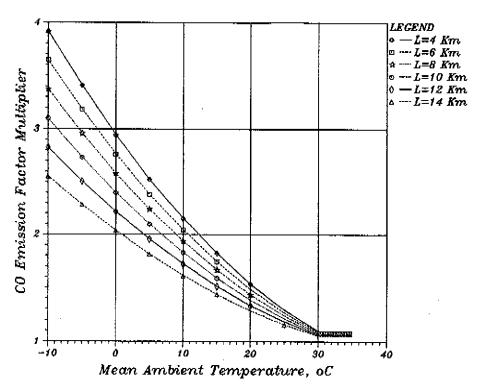


Figure 3.3.2.1-6c CO emission factor multiplier for LDGP cars with 3-way open loop catalyst and >  $1400\ cc$  engine, as function of the average temperature and trip length

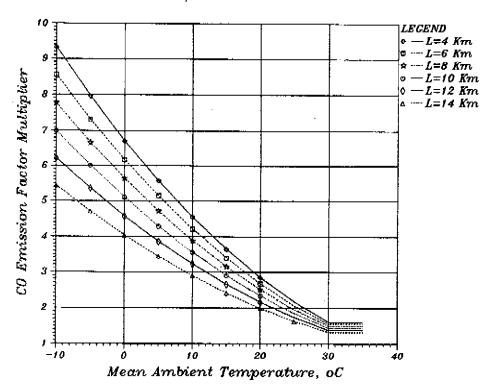


Figure 3.3.2.1-6d CO emission factor multiplier for LDGP cars with 3-way controlled catalyst and < 1400 cc engine, as function of the average temperature and trip length

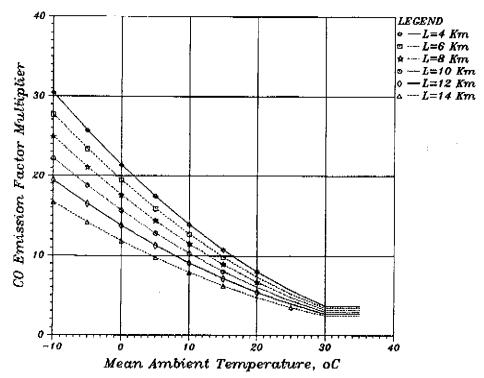


Figure 3.3.2.1-6e CO emission factor multiplier for LDGP cars with 3-way controlled catalyst and > 1400 cc engine, as function of the average temperature and trip length

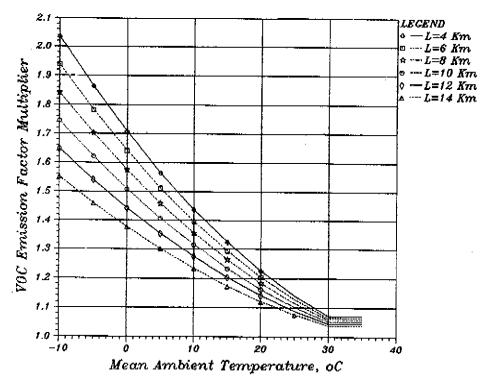


Figure 3.3.2.1-7a VOC emission factor multiplier for conventional (non-catalytic) LDGP cars, as function of the average daily, seasonal, or annual temperature and trip length

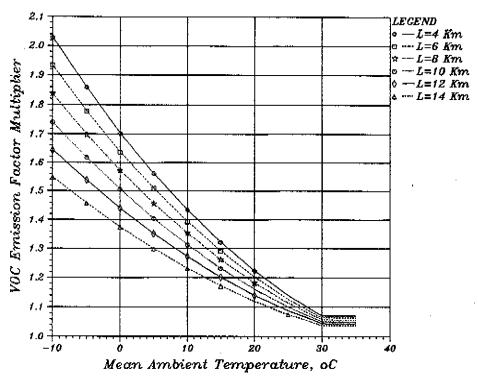


Figure 3.3.2.1-7b VOC emission factor multiplier for LDGP cars with 3-way open loop catalyst and < 1400 cc engine, as function of the average temperature and trip length

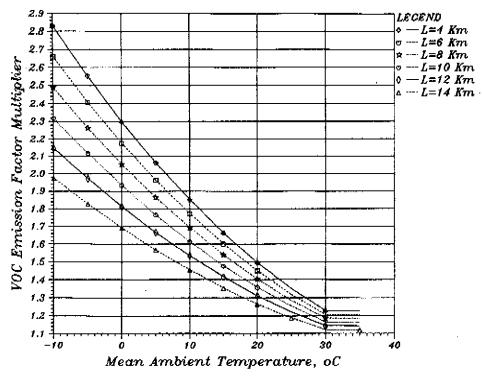


Figure 3.3.2.1-7c **VOC** emission factor multiplier for LDGP cars with 3-way open loop catalyst and > 1400 cc engine, as function of the average temperature and trip length

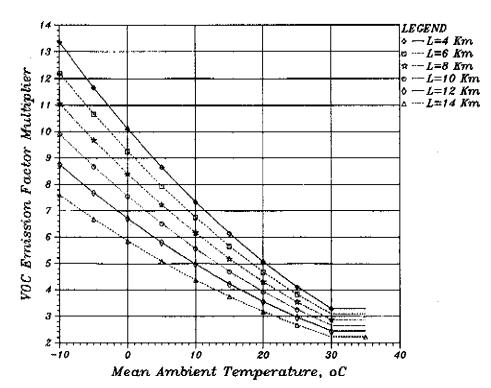
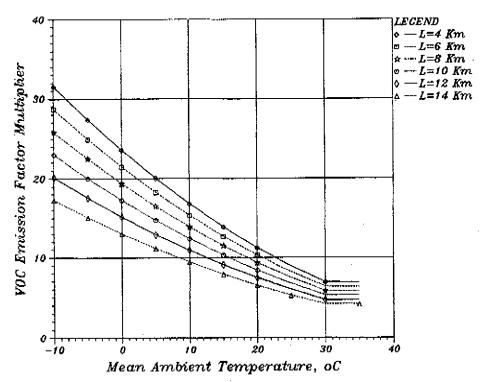
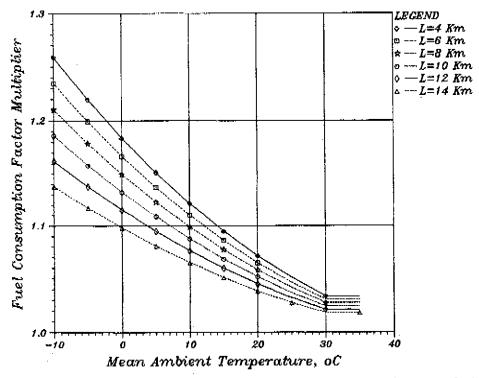


Figure 3.3.2.1-7d VOC emission factor multiplier for LDGP cars with 3-Way controlled catalyst and < 1400 cc engine, as function of the average temperature and trip length



VOC emission factor multiplier for LDGP cars with 3-Way controlled catalyst and Figure 3.3.2.1-7e > 1400 cc engine, as function of the average temperature and trip length



Fuel consumption factor multiplier for LDGP cars, as function of the average Figure 3.3.2.1-8 temperature and trip length

# 3.3.2.2 Example

### The Problem:

Assume that we need to compute the  $NO_{\rm X}$ , CO and VOC emission factors, as well as the fuel consumption factor, for small (<1400 cc engines) conventional (non catalytic) cars manufactured in the period 1985-1992.

The factors are to be computed for an average speed of 25 km/h, for a mean ambient temperature of 20  $^{\rm OC}$ , for an average trip length of 8 km and for a cold start fraction 0.75 (fcs=0.75).

# Solution of the Problem:

From From	Figure Figure	3.3.2.1-1a 3.3.2.1-2 3.3.2.1-3 3.3.2.1-4a	we we	obtain obtain	ehot ehot	for for	co^ voc	cons.	12.8	a/km
From	Figure	3.3.2.1-5a	we	obtain	Mn 75	: for	^ NOv		1.00	

From Figure 3.3.2.1-5a we obtain  $m_{0.75}$  for  $NO_X$  1.00 From Figure 3.3.2.1-6a we obtain  $m_{0.75}$  for CO 1.23 From Figure 3.3.2.1-7a we obtain  $m_{0.75}$  for VOC 1.18 From Figure 3.3.2.1-8 we obtain  $m_{0.75}$  for fuel cons. 1.06

Introducing the above  $e^{hot}$  -  $\rm m_{0.75}$  pairs in Equation 3.3.2.1-1, along with  $\rm f_{CS}\text{=}0.75,$  we obtain:

Emission factor for NO<sub>X</sub> 1.5 g/km Emission factor for CO 15.7 g/km Emission factor for VOC 2.2 g/km Fuel consumption factor 63.4 g/km

It can be seen that the emission factors listed in Section 3.2.2 are identical to the above. This is because the ambient temperature and the local driving conditions assumed here are the same as the default values used in the model in Section 3.2.2.

# 3.3.3 The Evaporative VOC Emissions Model

# 3.3.3.1 Description of the Model

The evaporative VOC emissions model for LDGP vehicles presented in this section is based on the data published by CONCAWE (1987). It should be noted that the factors listed in the inventory model of Section 3.2.2 are based on the CORINAIR study, ECE (1989), and that predictions based on the above data sets differ considerably.

The reason for employing a different data set in our present model than that used in Section 3.2.2, is that the latter allow only a qualitative assessment of the impact of the local climatic and gasoline volatility conditions. In addition, while data from CONCAWE report are rather scant and their extrapolation had to be based on 1970 & 1972 data from the U.S. Bureau of Mines, the origin of the CORINAIR data is rather unclear. In conclusion, the completeness, and probably the accuracy, of both data sets leaves a lot to be desired. Under such conditions, one may wish, to predict the evaporative emissions by both methods so as to have a better idea of the prediction discrepancies, as well as to define the limits of a probable valid range, with the predictions from the CONCAWE set being closer to the lower limit and these from the CORINAIR set to the upper limit. At any rate, the data in the CONCAWE report are better founded and the resulting predictions appear more reasonable.

As in the inventory model of Section 3.2.2, the evaporative VOC emissions have been divided into three categories: The Hot Soak losses, which occur when its hot engine is turned off, due to evaporation of fuel, mainly in the carburetor bowl and tank; The Running Losses, which occur while the vehicle is being driven; The Diurnal Losses, which occur while the vehicle is stationary with its engine off and are due to the expansion and emission of vapour, mainly from the fuel tank, as a result of the daily diurnal ambient temperature variations.

The emission factors for all three categories depend on the average daily, seasonal or annual temperature,  $T_{mean}$  in  $^{\circ}C$ , as well as on the gasoline volatility as expressed by the Reid Vapour Pressure, (a standardised vapour pressure measurement, made at 38 °C with a vapour/liquid ratio 4:1), RVP in kPa. In addition, the Hot Soak emissions per km depend on the average distance a car is driven each time its engine starts, Ltrip in km, while the Diurnal Losses depend on the average daily temperature variation for the day, season or year of reference, DT in oc.

The emission factors for the Hot Soak and Running losses are listed in Table 3.3.3.1-1 below as a function of the  $T_{mean}$ , gasoline RVP and  $L_{trip}$  as gr/km (or as kg/1000 km). The listed figures were derived from the original data given in the CONCAWE report and were converted in a form compatible with that in Table 3.2.2.

The emission factor for the diurnal losses, edjurnal, expressed as kg/(car\*year), can be easily computed from Equation (3.3.3.1-1) below:

 $e_{diurnal} = -9.125+0.1862*DT+0.2263*(T_{mean}+DT/2)+0.0803*RVP$  (3.3.3.1-1)

The predictions from the above model apply for cars with carburettors and with no evaporative controls.

Table 3.3.3.1-1 Hot Soak and Running Losses as Function of Climatic Conditions & Gasoline Volatility for LDGP cars

T <sub>mean</sub>	RVP 60 kPa	RVP 70 kPa	RVP 80 kPa	RVP 90 kPa	RVP 100 kPa	RVP 120 kPa
oC	gr/km	gr/km	gr/km	gr/km	gr/km	gr/km
Small Cars ( <	1400 cc)					
Hot Soak Emis	sions					
-10.0				.765/L <sub>trip</sub>	1.00/L <sub>trip</sub>	1.59/L <sub>trip</sub>
- 5.0				.824/Ltrip	1.03/Ltrip	1.47/Ltrip
- 0.5		.412/L <sub>trip</sub>	.647/L <sub>trip</sub>	.824/Ltrip	1.09/Ltrip	1.79/Ltrip
<b>3</b> .5		441/Ltrip	.676/Ltrip	.882/Ltrip	1.24/L <sub>trip</sub>	2.06/Ltrip
8.0	.500/L <sub>trip</sub>	.529/Ltrip	.794/Ltrip	I.03/Ltrip		/-trip
12.5	.706/L <sub>trip</sub>	.706/L <sub>trip</sub>	1.03/L <sub>trip</sub>	trip		
17.0	.971/L <sub>trip</sub>	1.12/L <sub>trip</sub>	1.59/Ltrip			
21.5	1.38/Ltrip	1.94/L <sub>trip</sub>	2.47/L <sub>trip</sub>			
Running Losse	S					
-10.0				0.0125	0.0175	0.027
- 5.0				0.0125	0.0175	0.029
- 0.5		0.0075	0.01	0.015	0.02	0.032
3.5		0.0075	0.0125	0.015	0.02	0.034
8.0	0.0075	0.01	0.0125	0.0175		
12.5	0.0125	0.0125	0.0175			
17.0	0.0175	0.02	0.0274			
21.5	0.02	0.03	0.052			
Large Cars ( > 1	1400 cc)					
Hot Soak Emis	sions					
-10.0				1.47/L <sub>trip</sub>	1.76/L <sub>trip</sub>	2.44/L <sub>trip</sub>
- 5.0				1.47/Ltrip	1.94/Ltrip	2.94/Ltrip
- 0.5		.794/L <sub>trip</sub>	1.24/L <sub>trip</sub>	1.71/L <sub>trip</sub>	2.21/L <sub>trip</sub>	3.53/Ltrip
3.5		.853/Ltrip	1.35/Ltrip	1.88/L <sub>trip</sub>	2.50/L <sub>trip</sub>	4.24/L <sub>trip</sub>
8.0	.882/L <sub>trip</sub>	.971/Ltrip	1.56/L <sub>trip</sub>	2.29/L <sub>trip</sub>	+trip	//- // -trip
12.5	1.15/L <sub>trin</sub>	1.29/Ltrip	2.00/Ltrip	··-trip		
17.0	1.59/Ltrip	1.94/Ltrip	2.94/Ltrip			
21.5	2.21/L <sub>trip</sub>	3.18/L <sub>trip</sub>	4.44/Ltrip			
Running Losse	s					
-10.0				0.033	0.04	0.056
- 5.0				0.033	0.047	0.066
- 0.5		0.02	0.027	0.04	0.05	0.083
3.5		0.02	0.03	0.043	0.056	0.1
8.0	0.02	0.023	0.037	0.053		
12.5	0.023	0.03	0.047			
17.0	0.033	0.047	0.066			
, 21.5	0.05	0.073	0.096			

#### Example Application 3.3.3.2

### The Problem:

Compute the annual mean emission factors for Hot Soak, Running Losses and Diurnal Losses, as well as the annual evaporative emissions from the LDGP car fleet in Athens using the Models of Section 3.2.2 and 3.3.3.1 for both small and large cars.

The following climatological and gasoline volatility data are given:

Greece Country: City: Athens

Vehicles: 950,000 (80% with engines < 1400 cc)

.8,000 km/yr (within the city) Milage:

17.4 °C <u>Tmean:</u> 10.0 °C DÏ: 8 km

L<sub>trip</sub>: RVP: 70 kPa (65 kPa from 1/4-31/10 & 80 kPa from 1/11-31/3)

Cars with carburettors and with no evaporative controls Note:

can be assumed

# Solution of the Problem:

From Table 3.2.2 we get both the emission factors, as well as the correction factors for Greece as follows:

 $e_{hot-soak} = (9.4/8)*1.2 = 1.41 \text{ gr/km}$ 0.55\*1.2 = 0.66 gr/kmerunning = 2.635\*2.1 = 5.53 kg/car-yearediurnal.

From the above emission factors, the number of cars and the annual milage we get:

 $E_{hot-soak} = 1.41*8000*950000/10^6 = 10716 tn/yr$   $E_{running} = 0.66*8000*950000/10^6 = 5016 tn/yr$  $5.53*950000/10^3 = 5253 \text{ tn/yr}$ Ediurnal 20985 tn/yr Total Evaporative

From Table 3.3.3.1-1 and Equation (3.3.3.1-1) we can obtain the sought emission factors for the given Tmean, DT, Ltrip and gasoline RVP values as follows:

From the above emission factors, the number of cars and the annual mileage we get:

```
For small cars ( < 1400 cc):
    Ehot-soak = 0.14*8000*760000/106 = 851 tn/yr
    Erunning = 0.02*8000*760000/106 = 122 tn/yr

For large cars ( > 1400 cc):
    Ehot-soak = 0.242*8000*190000/106 = 368 tn/yr
    Erunning = 0.047*8000*190000/106 = 71 tn/yr

For both small & large cars
    Ediurnal = 3.43*950000/103 = 3259 tn/yr

Total Evaporative 4671 tn/yr
```

Comparison of the predictions between the two models shows considerable discrepancies, the CORINAIR data set yielding 20985 tn/yr and the CONCAWE data set 4671 tn/yr. The latter appears closer to reality.

# 3.4 Model for the Flue Gas Volume from External Combustion Sources

# 3.4.1 Introduction

The emphasis so far in this section is in the presentation of models allowing the assessment of the emission loads from a given source. Loads alone however, may not be sufficient for estimating the impact of the sources in the environment.

Indeed, the following additional information is required for the application of air quality models in the case of point sources (see Section 8.2):

Exit gas volume, Exit gas temperature, Stack physical height, Stack internal diameter,

For area sources (e.g. road traffic, space heating furnaces, small industrial activities etc), the relevant information is somewhat relaxed as only the release height is required.

This section presents a model which allows convenient assessment of the flue gas volume from external combustion sources as a function of the easily measured (or assumed) CO2 concentration. As the vast majority of point sources for which air quality models are applied, are industrial or utility boilers, the material presented here should cover a significant part of the gas volume data requirements.

#### 3.4.2 Description of the Model

The major parameters which affect the normalized flue gas volume (actual m<sup>3</sup>/s at 200 <sup>o</sup>C per ton/hour of ash free and moisture free fuel used) are the fuel type and the CO2 concentration in the flue gas.

The fuel type defines to a large extent the fractions of the Carbon, Hydrogen, Oxygen and other elements which are present in the fuel and as such affects, through the reactions that take place during the combustion, the volume of the flue gas.

The CO<sub>2</sub> concentration is a good indicator of the excess air used, as the excess air dilutes the CO2 combustion product. The lower the CO2 concentration, the higher the excess of air used and the larger the volume of flue gas.

A quantitative expression of the above dependencies is provided by the graphs in Figures 3.4.2-1 to 3.4.2-5, produced with the help of a boiler simulation model, and which, for various common fuels allows direct reading of the normalized flue gas volume as a function of the CO<sub>2</sub>.

In cases where CO2 measurements are not available, one can always make an assumption considering the following maximum CO2 concentrations (corresponding to combustion zero excess air), the type and size of boiler, and the operating procures:

Table 3.4.2-1 Maximum CO<sub>2</sub> concentration in the flue gas for various fuels

	Maximum C
Fuel type	(Vol %, Dry Basi
Natural Gas (NG) or Liquefied Natural Gas (LNG)	12.2
Liquefied Petroleum Gas	12.2 13.94
Distillate Fuel Oil Residual Fuel Oil	15.7
Meta Anthracite Coal	19.6
Anthracite Coal	19.6
Semi Anthracite Coal	19.1
Bituminous Low Volatility Coal	18.7
Bituminous Medium Volatility Coal	18.5 18.4
Bituminous High Volatility Coal	19.15
Subbituminous Coal Lignite	19.35
Peat	19.

Large industrial and utility boilers under close supervision operate with 10 to 20% excess air. Poorly operated boilers, or some types of boilers where control is difficult (e.g. underfed stokers or hand fired units) may operate with much higher percentages of excess air.

For the limiting  $(CO_2)_{max}$  concentration from Table 3.4.2-1 above and for any assumed Excess Air percentage, the corresponding  $CO_2$  concentration can be computed from the following relation:

$$co_2 = \frac{7900*(co_2)_{max}}{(Excess Air Used, %)*(100-(co_2)_{max}) + 7900} . \qquad (3.4.2-1)$$

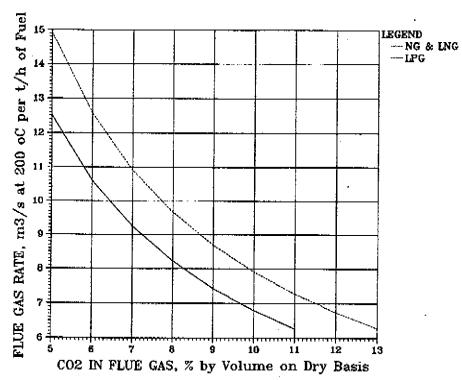


Figure 3.4.2-1 Flue gas volume from external combustion sources firing Natural Gas (NG), Liquefied Natural Gas (LNG) or Liquefied Petroleum Gas (LPG), as function of the  ${\rm CO_2}$ concentration (volume % on a dry basis) in the flue gas.

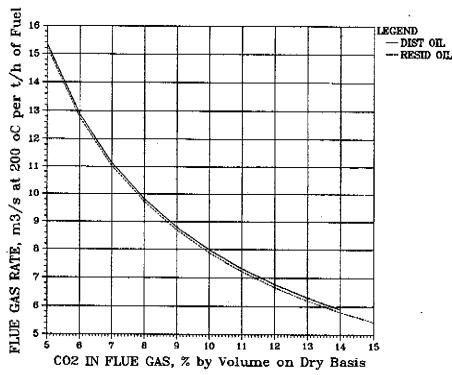
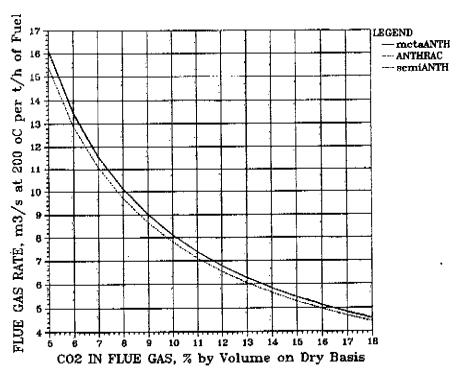
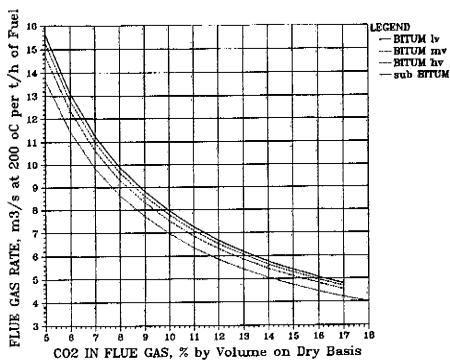


Figure 3.4.2-2 Flue gas volume from external combustion sources firing Distillate and Residue Fuel Oil, as function of the  ${\rm CO_2}$  concentration (volume % on a dry basis) in the flue gas.

moisture free basis.



Flue gas volume from external combustion sources firing Meta Anthracite, An-Figure 3.4.2-3 thracite of Semi Anthracite coal, as function of the  ${\rm CO_2}$  concentration (volume % on a dry basis) in the flue gas. The quantity of coal is on an ash free and



Flue gas volume from external combustion sources firing Bituminous Coal of low. Figure 3.4.2-4 medium, or high volatility (Legend: BITUM lv, mv and hv respectively), and Subbituminous Coal, as function of the  ${\rm CO_2}$  concentration (volume % on a dry basis) in the flue gas. The quantity of coal is on an ash free and moisture free basis.

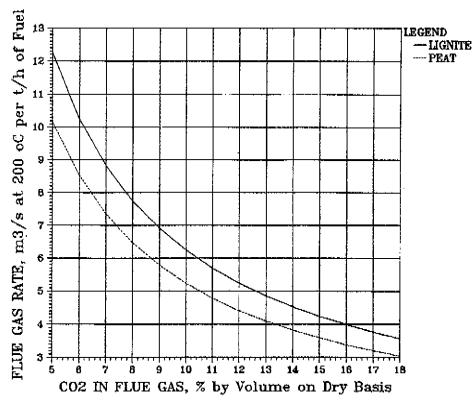


Figure 3.4.2-5 Flue gas volume from external combustion sources firing Lignite and Peat, as function of the CO<sub>2</sub> concentration (volume % on a dry basis) in the flue gas. The quantity of coal is on an ash free and moisture free basis.

# 3.4.3 Example

### The Problem:

A utility boiler firing residue fuel oil consumes 37.5 tons of fuel per hour. Compute the actual flue gas volume for an exit gas temperature of 180  $^{\circ}\text{C}$ .

# Solution of the Problem:

As the  ${\rm CO_2}$  concentration in the flue gas is not given, it will have to be assumed. The boiler is large and is firing oil. Under the circumstances we can assume an operation with excess air of about 10%.

From Table 3.4.2-1 the limiting CO2 concentration is 15.7 %.

From Equation 3.4.2-1 we compute that for 10 % excess air the corresponding CO<sub>2</sub> concentration 14.2%.

From Figure 3.4.2-2 we obtain that the normalized flue gas volume is 5.7 (Am3/s at 200  $^{\circ}$ C per ton/h of fuel used).

Considering that the boiler uses 37.5 tons/hour of fuel, the actual flue gas volume at 180  $^{\circ}$ C is then 5.7\*37.5\*(273+180)/(273+200) = 205 Am<sup>3</sup>/s.

### 3.5 Model for the Temperature Drop Through Stacks

#### 3.5.1 Introduction

The need to assess the flue gas exit volume and temperature so as to be able to use air quality models has been discussed in Section 3.4.1.

From the nature of the source, or through direct measurement, the temperature is usually known, at the boiler exit or at stack entrance point. For the application of the dispersion models however, we need to know the gas temperature at the stack exit point and also therefore the temperature drop of the gas as it passes through the stack.

### 3.5.2 Description of the Model

A fair number of parameters affect the temperature drop through the stack, such as the composition of the gas, the length and the diameter of the stack, the gas rate and the gas temperature at the stack entry point, the ambient air temperature, the stack thermal insulation etc.

To simplify the procedure and to present the results in graphic and easy to use form, some simplifying assumptions have to be made. The most important one is the assumption of 2.5 cm of fibreglass equivalent insulation in cases of insulated stacks. The results are plotted in Figures 3.5.2-1 and 3.5.2-2 and allow direct reading of the normalized allow (temperature drop per 10 m of stack height when the temperature difference between the inlet gas and the ambient air is 180  $^{\rm OC}$  (inlet gas temperature 200  $^{\rm OC}$ ) and ambient air temperature 20  $^{\rm OC}$ ).

The graphs were produced with the help of a stack model which, depending on the physical stack dimensions and the presence or absence of insulation, it computes through an iterative scheme the temperature and the velocity profiles, the physical properties of the flowing gas, and the heat transfer rates, so as to eventually yield the exit gas temperature and the corresponding normalized temperature drop.

In order to use the graphs correctly, the following procedure can be used:

(a) Compute the exit gas volume at 200 °C

(b) Use Figures 3.5.2-1 or 3.5.2-2 to obtain the normalized  $\Delta T$ .

(c) Compute the actual  $\Delta T$  through the entire stack length from Equation:

$$\Delta T = (\Delta T)_{\text{normalized}} \frac{\text{(Stack height, m)}}{10} \frac{\text{(Tinlet gas}^{-T} \text{air)}}{180}$$
 (3.5.2-1)

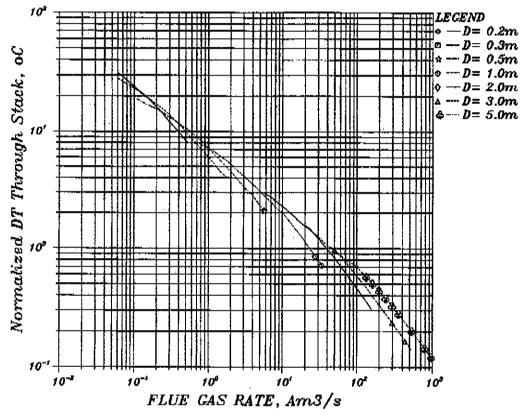


Figure 3.5.2-1 Normalized temperature drop though **non-insulated** stacks (temperature drop per 10 m of stack height when the temperature difference between the inlet gas and the ambient air is 180 °C) as function of the flue gas rate, stack physical height and stack inside diameter.

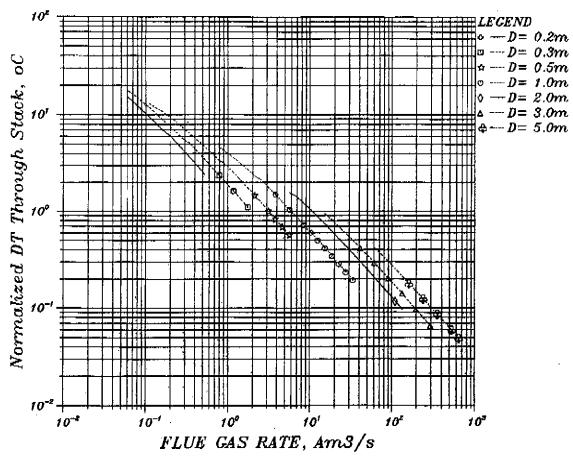


Figure 3.5.2-2 Normalized temperature drop though insulated stacks (temperature drop per 10 m of stack height when the temperature difference between the inlet gas and the ambient air is 180 °C) as function of the flue gas rate, stack physical height and stack inside diameter.

#### 3.5.3 Example

#### Problem:

The gas from the utility boiler considered in the example in Section 3.4.3 goes though a non-insulated stack of 5 m in diameter and 150 m height before being released into the atmosphere.

Compute the temperature of the gas at the exit point when the temperature at the inlet point is 180  $^{\rm OC}$  and the ambient air temperature is -10  $^{\rm OC}$ .

#### Solution:

In Section 3.4.3 we calculated that the exit gas volume at 180  $^{\circ}$ C is 205 Am<sup>3</sup>/s. The gas volume at 200  $^{\circ}$ C is 205\*(273+200)/(273+180)=214 Am<sup>3</sup>/s.

Figure 3.5.2-1 yields ( $\Delta T$ )normalized=0.4

Equation 3.5.2-1 yields  $\Delta T = 6.5$  °C. The exit gas temperature is thus 180-6.5=173.5 °C.

It should be noted that considerably higher temperature drops are obtained in the case of smaller boilers, where the ratio of stack surface to gas rate is much higher.

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CHAPTER

4

# LIQUID WASTE INVENTORIES AND CONTROLS

- 4.1 Compilation of Liquid Waste Inventories Under Present and/or Strategy Target Conditions
- 4.2 Model for Compiling Liquid Waste Inventories and Assessing the Effectiveness of Applicable Controls
  - 4.2.1 Introduction
  - 4.2.2 Model for Liquid Waste Inventories and Controls
  - 4.2.3 Working Table for Assessing the Liquid Waste Loads
  - 4.2.4 Example
- 4.3 Bibliography

# 4.1 Compilation of Liquid Waste Inventories Under Present and/or Strategy Target Conditions

The liquid waste loads and controls model given in Section 4.2.2 provides four columns listing the conventional pollutants BOD<sub>5</sub>, SS, Total N, and Total P, as well as a sixth column reserved for toxic and other important substances, as the case may be for each source considered. In addition to the above, the model in Section 4.2.2 is supplemented by Tables 4.2.2-1 to 4.2.2-5, providing more detailed data and information about waste load factors and treatment efficiencies for municipal wastewaters (SIC 920), waste load factors for rain and land runoff, control efficiencies for agricultural industries (SIC 1110 to 1134), and the composition of leachates from municipal solid waste landfill sites.

In the model in Section 4.2.2, if a waste load factor does not appear in the appropriate place in the table, this usually (but not always) means that its value is either small or zero. However, lack of a penetration factor does not mean zero penetration, but rather that the value of this factor is not known. Missing waste load and/or penetration factors for the sources and pollutants of interest could be completed by the study team on the basis of information which might be available from literature or other sources in the study area.

The procedural aspects of the calculation of liquid loads released from various sources in the study area are presented in Section 2.3 and demonstrated through an example in Section 4.2.4.

Before concluding the discussion on liquid waste inventories, some reference to the important category of distributed sources is warranted. Indeed, such sources are known to significantly affect the quality of water receivers, especially surface ones. The nature of runoff water from various types of land (urban, forest, pasture, agricultural) is addressed through the data in Table 4.2.2-3, and factor ranges are provided to give an idea of the rather significant variations encountered from North American and European areas. Even wider variations could be expected from areas with different rain patterns, different fertiliser use, different vegetation and soil types, different population densities, different street cleaning procedures, etc.

The above information allows users to make preliminary assessments of the polluting loads from land runoff, and this facilitates the preliminary analysis of lake or river pollution problems. As these water bodies provide the natural drainage of large catchment basins, the contribution of the surface and underground water runoff to their pollution problems is often dominant. It should be added that rain runoff from urban areas emerges as a significant, if not a dominant, source of pollution in cases where municipal effluents are treated.

In conclusion, the assessment of the polluting loads from land runoff should be viewed only as a preliminary indication of the magnitude of the problem. In cases where sources of this kind appear significant, more detailed analysis may be necessary.

#### Model for Compiling Liquid Waste Inventories and Assessing 4.2 the Effectiveness of Applicable Controls

#### Introduction 4.2.1

The quantities of effluent loads released into the environment from urban areas or any industrial or other activity depend, in the general case, on a number of parameters. Thus, as in the case of effluents, the load E of pollutant j could be expressed in a mathematical form as follows:

 $E_i = f(Source type,$ (4.2.1-1)Unit of activity, Source size, Process or design particularities, Source age and technological sophistication, Source maintenance and operating practices, Type and quality of the raw materials used, Type, design and age of the control systems employed, Ambient conditions, etc.)

The source type defines the kind of pollution generating activity in somewhat broad terms, e.g. poultry processing or beer production. More precise definition is provided through other parameters as discussed below. Obviously, the source type is closely related to the types and to the quantities of pollutants generated.

From the source type information alone, it is possible to exclude, right from the start, numerous activities with relatively minor effluent problems and in this way, to simplify significantly the source inventory and liquid waste management tasks.

The unit of activity, defines an acceptable way of expressing the magnitude of a given source. Suitably defined units can be used to provide a measure of the source (e.g. population of an urban area) or the activity of an industry (raw materials consumed, or products manufactured).

Selection of the most suitable unit for each type of activity is important, as the unit must have a direct relation to the effluent loads generated, and must offer convenience in obtaining the required data during the field work. For example, the magnitude of a tannery source could be characterized by the electricity or the water consumed, by the number of people employed, by the land area occupied, or by the quantities of the hides processed. The latter is much closer related to the effluent loads generated, can be easily obtained, both during plant survey visits and from government sources (usually as a compounded total for all tanneries), and is thus the unit of choice.

Source size, although a key parameter, is only indirectly related to the normalized load rates (pollutant loads per unit of activity). In general, economies of scale allow better design and operation, as well as stricter effluent controls for larger size units. Moreover, for industrial sources, selection of the particular process to be used is some times dictated by plant size. It is for these reasons that effluent standards are generally significantly stricter for large plants.

In the context of the present methodology the effects of plant size on the normalized loads can be taken into consideration only in cases where the source size affects the process selection.

Process or design particularities depend on local factors and on the source size, and may affect the kinds and to the quantities of pollutants generated from industrial sources. For example, depending on the country and on the size of the factory, different processes with different design features are likely to be involved in textile finishing mills.

Little information is available in the literature so as to allow quantification of the impact of such effects on the normalized loads generated from a particular source.

Source age and technological sophistication are important parameters, as they often significantly affect effluent loads. The aging of a source causes higher loads as systems tend to fail more frequently and their operation tends to depart from the new equipment specifications. In addition, older systems do not take full advantage of technological innovations, which tend to yield environmentally friendlier performance. Naturally, technological sophistication does not only depend on the age of the source alone, but also on environmental legislation, as well as on enforcement aspects.

Quantification of the impact of these parameters is possible for some important sources, as for example in the petroleum oil refining category.

Source maintenance and operating practices is another parameter significantly affecting effluent loads. Fortunately, for the vast majority of industrial sources proper maintenance and operation is also intimately related to production quality and costs and for this reason is usually practiced to acceptable standards. For smaller sources however, improper maintenance and operation is the rule rather than the exception, despite the associated economic losses.

Unfortunately, few data are available in the literature to allow the derivation of quantitative relations regarding the impact of maintenance procedures on effluent loads.

The type and the quality of the raw materials used is in may cases intimately related to the types and to the quantities of pollutants emitted. In industrial processes the type and the quality of raw

materials available often dictate the process to be used and the effluent loads released by them, and this is generally covered by the effluent loads model of Section 4.2.2.

The type, design, and age of the control systems employed determine the removal efficiencies of the effluent loads and are thus intimately related to the impact of the discharges on the final receivers.

The type of control system employed defines by itself the capabilities and limitations (and hence the control efficiency range) for the source under consideration. Analysis of the control system performance through appropriate models could, in principle, provide a better insight and a more accurate assessment of control system efficiencies. However, as the performance of the control systems depends significantly on the nature of the particular wastes, reliable predictions are not always easy to generate. Moreover, the detailed design data and performance analysis requirements burden the inventory and strategy formulation process very significantly.

The age of the control system may affect the efficiency due to the progressive downgrading of the performance with time, but, most importantly, due to the generally more relaxed design specifications of the past. Old age of equipment tends thus to be associated with lower design efficiencies.

In our inventory model the type of control system is used as the leading parameter for assessing a typical control system performance. Detailed assessments on the basis of specific design characteristics are however not addressed, as typical design practices are assumed.

The ambient conditions may significantly affect the rate of the effluent loads. For example, the performance of most treatment processes, especially biological ones, is affected by the temperature. However, this sensitivity is usually compensated by proper sizing of the treatment processes.

The above discussion leads into the important practical question of how the effluent load  $E_{\hat{j}}$  can be expressed as a direct and explicit function of all the parameters that may affect it for all pollutants j of interest.

The first step in this direction is to define the effluent load factor ej for pollutant j, through the following relation:

$$e_j = \frac{E_j, kg/yr}{Source activity, Units/yr}$$
 (4.2.1-2)

The effluent load factor  $\mathbf{e_j}$  is normally expressed as kg/Unit and is assumed to be independent of source size and of source activity (or production) level. The basis for this assumption is the way the activity units are selected. Indeed, as discussed above, a key criterion in the selection of the activity units is their direct and proportional relation to the effluent loads generated. From the above and from Equation (4.2.1-1) we obtain:

The dependence of the emission factors  $\mathbf{e_j}$  on the parameters discussed above and listed in Equation (4.2.1-3), cannot, in most cases, be expressed in a continuous function form due to the discreet nature of some parameters (e.g. alternative types of treatment systems), and to the frequent lack of sufficient information in relation to the remaining parameters. A discreet functional form yielding a series of emission values, each valid under a specific set of common and important parameter combinations, is used instead.

The discreet rather than the continuous nature of the emission factor values explains the tabular construct of the Model in Section 4.2.2, into which the source types are organized on the basis of the UN Standard Classification of Industries and Services. Under each activity listed, all typical alternative processes are included (e.g. under Tanneries and Leather Finishing (SIC 3231), the Hair Pulp/Chrome Tanning, Hair Save/Chrome Tanning, Hair Pulp of Shave/Non-Chrome Tanning, Re-tanning and Wet Finishing Only), and for each such process all major control alternatives are provided (e.g. Primary Sedimentation, Sulfide Oxidation/Sedimentation, Coagulation/Sedimentation, and Activated Sludge).

The waste load factors are always listed for each uncontrolled source. For the computation of the load factors which are applicable after each alternative treatment installation, two methods are followed:

- (a) For single sources, load factors for the treated wastes are directly listed for each alternative type of treatment plant (see for example the Iron and Steel source category, SIC 371).
- (b) Multiple sources of similar nature and wastes with similar treatability characteristics are placed in a block, following which, typical treatment processes applicable to all sources in the block, are listed and penetration factors for each pollutant are provided (see for example the tanneries block, SIC 3231). The waste factors for a given source with a given wastewater treatment scheme may be

thus computed as the product of each uncontrolled waste factor and the corresponding penetration factor.

The impact of the raw materials type and quality is expressed indirectly through the listing of alternative processes (the process selection often depends on the raw materials available), or described in footnotes. Similar provision is made for remaining parameters, whenever their impact becomes important and relevant information exists.

The tabular structure and the form of Section 4.2.2 provides the basis for an elaborate effluent loads model by introducing the impact of all major parameters into the assessment of the pollutant load releases, as well as by providing a precise definition of the data requirements from field surveys. The model in Section 4.2.2 is thus a valuable tool for source inventory studies, not only for computing effluent loads, but also for providing guidance on the data to be collected during the field survey work, as well as for organizing and presenting such data in a concise manner (see also Sections 4.2.3 and 4.2.4 below).

In addition, the model in Section 4.2.2 should be a valuable tool in water pollution management studies as it provides a clear picture of the existing sources and the effluent load generation and, along with it, a fairly comprehensive list of the available alternative control options for each activity. The above constitute key elements in the analysis of the water pollution problems and the formulation of effective control strategies for any given urban or industrial area.

The model in Section 4.2.2 is also useful in Environmental Impact Assessment Studies as it provides, in a convenient form, quantification of the impact of alternative process and emission control system selections for most sources and activities of interest.

The model in Section 4.2.2 is supplemented by Tables 4.2.2-1 to 4.2.2-5, providing more-detailed data and information about waste load factors and treatment efficiencies for municipal waste-waters (SIC 920), waste load factors for rain and land runoff, control efficiencies for agricultural industries (SIC 1110 to 1134), and the composition of leachates from municipal solid waste landfill sites.

### 4.2.2 Model for Liquid Waste Inventories and Controls1.2

 						Wint	
		8005	TSS	Tot N	Tot P	Other F	ollutants
UNIT	WASTE						
(U)	VOLUME	ka/U	ka/U	ka/U	ka/U	Name	kg/U
,	m <sup>3</sup> /υ	Pntr			-		Potr
	,,, ,	* *****	, ,,,,,,,	, ,,,			1,1,4,1

MAJOR DIVISION 1. AGRICULTURE, HUNTING, FORESTRY AND FISHING

#### DIVISION 11. AGRICULTURE AND HUNTING

#### 111 Agricultural and Livestock Production<sup>3</sup>

Beef Cattle, 360 kg aver. Slotted floor/Shallow pit <sup>4</sup>	Head*yr	8.0	164	1204	43.8	11.3
Dairy Cattle, 590 kg aver. <sup>5</sup>						
Free stall barn	Head*уг	15.6	228.5	1533	82.1	12.0
Milking Center	Head*yr	5.6	21.5		2.5	3.3
Swine feedlot, 45 kg aver.						
Solid floor/water washed	Head*yr	14.6	32.9	73.	7.3	2.3
Slotted floor/Pit manure	Head*yr	2.8	32.9	24.8	7.3	2.3
Sheep, 68 kg average						
Housed/Solid manure	Head*yr	2.6	58.4		23	6.6
Housed/Liquid manure	Head*yr	4.9	33.2	158.4	4	21.5

- If a waste load factor does not appear in the appropriate place, this often (but not always) means that its value is either small or zero. However, lack of a penetration factor for a wastewater treatment plant does not mean zero penetration, but rather that the value of this factor is not known.
- 2. The listed waste volume factors do not account for cooling water discharges, which may be very significant. The underline assumption here is that, unless otherwise noted, the cooling waters are recycled and only a small portion of them, the blowdown, is discharged along with the effluents.
- 3. Low density pasture units represent zero level of waste problems, along with the recovery of full fertilizer value. However, the waste from high density confined operations approaches the total loads and thus requires considerable management.
- 4. In beef cattle feedlots calves enter weighing 270 kg, and after a period of 130 to 180 days they leave as market animals weighing about 477 kg.

  Beef feedlots include shallow and deep pit systems, dirt-flat to moderate slope, dirt-steep slope and paved open slots. The listed factors for shallow pit systems represent the highest loads, as the manure is collected almost daily. In all other systems the manure remains on the floor for a period of time and undergoes decomposition, loosing some of its original organic load strength. For example, in deep pit systems where the manure may remain for 6 to 12 months, the BOD can be reduced by about 40 %, the total Nitrogen can be reduced somewhat due to ammonia losses, but the total phosphorus remains unchanged.
- In dairy farms each cow produces 9 to 25 kg of milk daily and 1 calve per year.
- 6 In swine feedlots, feeder pigs enter weighing 25 kg, and after a period of 23 to 25 weeks they leave as 100 kg hogs to be slaughtered.

Model for Liquid Waste Inventories and Controls - Cont'd

			BOD <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
	(U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
	<del></del>							
Housed/Solid manure	Head*yr	1.5	33.7		13.5	3.7		
Housed/Liquid manure	Head*yr	2.9	19.2	169	2.5	1.24		
Chicken <sup>8</sup>	•							
Broilers on feed, I kg	Head*yr	21.5	1.61	4.2	3.6			
	of bird)*yr	21.5	1.61	4.2	3.6			
Turkeys <sup>9</sup>								
Breeding birds, 11.4 kg	Head*yr	0.25	14.2		3	2.5		
Market birds, 6.8 kg	Head*yr	0.15	8.4		1.8	1.5		
Ducks, 16 kg average	Head*yr	84	6.4	9.1	N/A	N/A		
Horses / Manure & Bedding	Head*yr	13.6	146		95.3	16.4		
	Unaerated	lagoon	0.22	0.45	0.44	0.91		
	Oxidation	-	0.11	0.45	0.25	1.0		

#### MAJOR DIVISION 3. MANUFACTURING

#### DIVISION 31. MANUFACTURE OF FOOD, BEVERAGES AND TOBACCO

#### 311 Food Manufacturing

3111 Slaughtering. Preparing & Preserving Meat 10.11.12

Simple slaughterhouses								
With blood recovered	tn LWK	5.3	6	5.6	0.7	0.05	Oil	2.1
Without blood recovered	tn LWK	5.3	10	8.0	0.7	0.05	0i1	4

7. In lamb feedlots, lambs enter weighing 30 to 41 kg, and after a period of 40 to 150 days they leave as market animals weighing about 45 to 59 kg.

8. Both breeding flocks and the growing birds are normally kept on litter (0.9 and 2.7 kg/bird used respectively), where their wastes are absorbed and remain for prolonged periods. The listed factors represent fresh chicken manure with no estimation for the considerable biodegradation or evaporation. They reflect however the loads in newer installations, where the wastes are regularly washed away.

9. Turkeys, like chicken, are growing on litter and the listed factors do not account for the biodegradation.

10. LWK is an abbreviation for the Live Weight of the animals Killed.

11. The average weight of cattle is 430 kg, of calf 97 kg, of hog 120 kg, and of lamb 52 kg.

12. The edible meat is about 60% of LWK;

 $\label{thm:model} \mbox{Model for Liquid Waste Inventories and Controls - Cont'd}$ 

	UNIT	WASTE	BOD <sub>5</sub>	TSS	Tot N	Yot P	Other	Pollutants
	(U)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/ປ Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Complex slaughterhouses	tn LWK	7.4	10.9	9.6	0.84	0.33	011	5.9
Packing houses  Low processing	tn LWK	7.8	8.1	5.9	0.53	0.13	011	3
High processing Rendering plants	tn LWK tn LWK	12.5 3.3	16.1 2.15	10.5 1.13	1.3 0.48	0.4 0.04	011 011	9 0.72
Poultry processing								
With blood recovery	1000 birds	37.5	11.9	12.7				5.6
Without blood recovery	1000 birds	37.5	17	12.7				5.6
Primary skimmi			0.45	0.07			011	0.13
Primary skimming and air floa	tation with co	agu lant	0.15	0.05			011	0.1
	ic and aerobic		0.046	0.065	0.67		0 i l	0.047
Éxtended aerati		_	0.04	0.14	0.72		011	0.02
Aerobic lagoon	and trickling	filter	0.025	0.06	0.7		011	0.04
2-\$	tage trickling	filter	0.045	0.05	0.7		Oi1	0.02

#### 3112 Manufacturing of dairy products 13.14

Dairies						
Receiving station						
Cans	tn of product	0.68	0.46	0.03	0.49	0.11
₿ulk	tn of product	0.08	0.17	0.03	0.06	0.013
Fluid products	tn of product	3.1	3.21	1.5	0.31	0.68
Cultured products	tn of product	3.9	3.21	1.5	0.31	0.68
Butter	tn of product	2.6	1.1	0.4	1.95	0.42
Cottage cheese						
With whey recovery	tn of product	7.7	21.7	3.4		
Natural cheese						
With whey recovery	tn of product	2.3	2.2	0.2	1.56	0.34
Ice cream	tn of product	3	10.9	1.5		
Condensed milk	tn of product	2	6.7	0.83	0.39	0.08
Powder production	tn of product					
Spray drying	in of product	0.7	22.4		1.3	0.28
Roller drying	tn of product	0.8	26.8		1.56	0.34
	Activated	<del>-</del>	0.071	0.046		0.39
	Trickling	filter	0.095	0.43		0.39

<sup>13.</sup> The  $BOD_5$  loads were estimated from the COD loads given in literature, using typical for each project  $COD/BOD_5$  ratios.

The typical distribution of products obtained from 1000 lt of milk is as follows: Butter 5 kg, Cheese 10 kg, Condensed milk (45% dry matter) 26 kg, Condensate (30% dry-matter) 40 kg, Skimmed milk powder 9 kg, and Full-milk powder 12 kg.

 $\label{thm:model} \textbf{Model for Liquid Waste Inventories and Controls - Cont'd}$ 

ţ.	MITT	cre	80D <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
	UNIT (U)	WASTE VOLUME m <sup>3</sup> /U	-	kg/U Pntr	-	-	Name	kg/U Pntr
	Aerated	lagoon	0.155			0.39		
	Stabilizati	on pond	0.05			0.39		
1	Anaerobic di	gestion	0.7			0.39		

### 3113 Canning & Preserving of Fruits & Vegetables

Fruits Processing				
Apricots	tn raw material	29.1	15.4	4.25
Apple				
All products	tn raw material	3.7	5	0.5
All prod. except ;	juicetn raw material	5.4	6.4	0.8
Juice	tn raw material	2.9	2	0.3
Canberries	tn raw material	5.8	2.8	0.6
Citrus	tn raw material	10.1	3.2	1.3
Sweet cherries	tn raw material	7.8	9.6	0.6
Sour cherries	tn raw material	12	17.2	1
Brine cherries	tn raw material	19.9	21.7	1.4
Cranberries	tn raw material	12.3	10	1.4
Oried fruit	tn raw material	13.3	12.4	1.9
Grapefruit				
Canning	tn raw material	72.1	10. <b>7</b>	1.2
Pressing	tn raw material	1.6	1.9	0.4
Olives	tn raw material	38.1	43.7	7.5
Peaches				
Canned	tn raw material	13	14	2.3
Frozen	tn raw material	5.4	11.7	1.8
Pears	tn raw matter	11.8	21.2	3.2
Pickles				
Fresh-packed	tn raw material	8.5	9.5	1.9
Process-packed	tn raw material	9.6	18.3	3.3
Salting stations	tn raw material	1.1	8.0	0.4
Pineapples	tn raw material	13	10.3	2.7
Plums	tn raw material	5	4.1	0.3
Raisins	tn raw material	2.8	6	1.6
Strawberries	tn raw material	13.1	5.3	1.4
Tomatoes				
Pee led	tn raw material	8.9	4.1	6.1
Products	tn raw material	4.7	1.3	2.7
Vegetable Processing				
Asparagus	tn raw material	68.8	2.1	3.4
Beets	tn raw material	5	19.7	3.9
Broccoli	tn raw material	45.6	9.8	5.6
Brussels sprouts	tn raw material	36.3	3.4	10.8
Carrots	tn raw material	12.1	19.5	12
Cauliflower	tn raw material	89.4	5.2	2.7

 $\label{thm:model} \mbox{Model for Liquid Waste Inventories and Controls - Cont'd}$ 

	UNIT	118 C T C	<sup>BOD</sup> 5	ZZT	Tot N	Tot P	Other Po	ollutant
	(U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/V Pntr	Name	kg/U Pnt:
Corn								
Canned	tn raw material	4.5	14.4	6.7				
Frozen	tn raw material	13.3	20.2	5.6				
Dehydrated								
Onion & garlic	tn raw material	19.9	6.5	5.9				
Vegetables	tn raw material	22.1	7.9	5.6				
Dry beans	tn raw material	18	15.3	4.4				
Lima beans	tn raw material	27.1	13.9	10.3				
Mushrooms	tn raw material	22.4	8.7	4.8				
Onions canned	tn raw material	23	22.6	9.3				
Peas				- · •				
Canned	tn raw material	19.7	22.1	5.4				
Frozen	tn raw material	14.5	18.3	4.9	•			
Pimentos	tn raw material	28.8	27.2	2.9				
Potatoes								
All products	tn raw material	10.3	18.1	15.9				
Frozen prod	tn raw material	11.3	22.9	19.4				
Dehydrated prod	to raw material	8.8	11	8.6				
Sauerkraut								
Canning	tn raw material	3.5	3.5	0.6				
Cutting	tn raw material	0.43	1.2	0.2				
Snap beans								
Canned	tn raw material	15.4	3.1	2				
Frozen	tn raw material	19.9	6	3				
Spinach								
Canned	tn raw material	37.6	8.2	6.5				
Frozen	to raw material	29.2	4.8	2				
Squash	tn raw material	5.6	16.8	2.3				
Sweet potatoes	tn raw material	4.1	30.1	11.5				
		1						
	Settling or flo		0.3	0.75				
	Chemical coag		0.2	0.3				
	Trickling :		0.12	0.1				
	Activated	-	0.07	0.1				
	Stabilizatio	on pond	0.1	0.05				

## 3114 Canning, preserving & processing of fish, crustacean & similar foods

Fish and Seafood Processing Catfish processing Blue crab	Industry tn of product	24	7.3	9.4	0.65	011	4.7
Convent'l Processing	tn of product	1.2	5.2	0.74	1	0i1	0.25
Mechanized Processing	tn of product	38	22.5	12	3.7	011	5.6
Shrimp							
Breaded	tn of product	116	84	93	5.9	OfT	20

Model for Liquid Waste Inventories and Controls - Cont'd

	HALTT	MACTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other Po	lutants
	(U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/V Pntr
Canned	tn of product	52	82	43	9.5		Oil	31
Frozen	tn of product	115	120	220	10		017	29
Tuna	tn of product	25	13.4	10.4	2.1		Oil	7.4
Clam								
Hand shucked	tn of product	4.6	5.1	10.2			Oil	0.14
Mechanized	tn of product	19.5	18.7	6.3			Oil	0.46
Fish meal								
With solubles	tn of product	35	3	0.9			Oil	0.56
Without solubles	tn of product	1.9	62.2	34.8			0i1	22.8
Şa lmon	·							
Mechanical buchering	tn of product	18.5	50.8	20.3			0i1	6.5
Hand buchering	tn of product	4	2.1	1.2			Oil	1.5
Sardine	tn of product	8.7	9.2	5.4			Oil	1.7
Herring filet	tn of product	7	32.2	20.9			0i1	6.5
Oyster / steam cleaned	tn of product	98	61.2	155			011	1.5
Screening, float	ation and aerate	d lagoon	0.05 I	0.05	•		Oil	0.4
Manufacture of vegetable			0.05 I	0.05	į		011	0.4
Manufacture of vegetable Olive Oil Expression	and antmal oils	and fats			į		Oil	0,1
Manufacture of vegetable Olive Oil Expression	and animal oils	and fats	210	325	·		Oil	0.1
Manufacture of vegetable Olive Oil Expression Pressing t	and animal oils on of oil product th of olives	and fats 5 1	210 42	32 <b>5</b> 65	į		Oil	0.1
Manufacture of vegetable Olive Oil Expression Pressing t	and animal oils on of oil product tn of olives on of oil product	and fats 5 1 7	210	325	į		Oil	0.1
Manufacture of vegetable Olive Oil Expression Pressing t	and animal oils on of oil product th of olives on of oil product th of olives	and fats 5 1 7 1.4	210 42 95 19	32 <b>5</b> 65 <b>45</b> 5	į		Oil	0.1
Manufacture of vegetable Olive Oil Expression Pressing t	and animal oils on of oil product tn of olives on of oil product	and fats  5 1 7 1.4	210 42 95 19	325 65 455 91	į		Oil	0.
Manufacture of vegetable Olive Oil Expression Pressing t	and animal oils on of oil product the of olives on of oil product the of olives Sedimentation w	and fats  5 1 7 1.4	210 42 95 19	325 65 455 91	;		Oil	0.1
Manufacture of vegetable Olive Oil Expression Pressing t Centrifuging t	and animal oils on of oil product the of olives on of oil product the of olives Sedimentation w	and fats  5 1 7 1.4	210 42 95 19	325 65 455 91	į			
Manufacture of vegetable Olive Oil Expression Pressing t Centrifuging t	and animal oils on of oil product the of olives on of oil product the of olives Sedimentation w	and fats  5 1 7 1.4 with Lime	210 42 95 19 1 0.	325 65 455 91			Oil	
Manufacture of vegetable  Olive Oil Expression Pressing t  Centrifuging t  Edible Oil Refining  Edible Fats and Oils	and animal oils on of oil product the of olives on of oil product the of olives Sedimentation we Anaerobic of	and fats  5 1 7 1.4 with Lime	210 42 95 19 1	325 65 455 91				28.
Manufacture of vegetable Olive Oil Expression Pressing t Centrifuging t  Edible Oil Refining Edible Fats and Oils General	and animal oils on of oil product the of olives on of oil product the of olives Sedimentation we Anaerobic of	and fats  5 1 7 1.4  ith Lime ligestion  6.8 1.85	210 42 95 19 1 0.	325 65 455 91 3				
Manufacture of vegetable Olive Oil Expression Pressing t Centrifuging t  Edible Oil Refining Edible Fats and Oils General Corn oil Olive oil	and animal oils  n of oil product th of olives n of oil product th of olives  Sedimentation w Anaerobic d  th of product th of product	and fats  5 1 7 1.4  with Lime ligestion  6.8 1.85 57.5	210 42 95 19 7 24.9 0.3 12.9	325 65 455 91 3 24,6 0.35 16.4			Oil	28.
Manufacture of vegetable Olive Oil Expression Pressing t Centrifuging t  Edible Oil Refining Edible Fats and Oils General Corn oil Olive oil	and animal oils on of oil product the of olives on of oil product the of olives  Sedimentation we Anaerobic of the of product the of product the of product	and fats  5 1 7 1.4 with Lime ligestion  6.8 1.85 57.5	210 42 95 19 7 0.3 12.9	325 65 455 91 3 24.6 0.35 16.4	2		Oil Oil	28. 6.5

Model for Liquid Waste Inventories and Controls - Cont'd

			11	u + <b>*</b>	MAGTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutan
				NIT U)	WASTE VOLUME m <sup>3</sup> /U	kg/V Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pn
116	Grain mill products										
	Corn										
	Wet milling	tn	of	product	22.4	7.3	5.2				
	Dry milling			product	0.7	1.1	1.6				
	Wheat										
	Normal milling	tn	of	product		No eff	fluents				
	Bulgur milling Rice	tn	of	product	0.29	0.11	0.1				
	Normal milling	tn	of	product		No eff	fluents				
	Parboiled milling	tn	of	product	1.5	1.8	0.07				
				Activated	ș ludae	0.21	0.41				
	Fłow equalizat	tion				0.1	0.2				
					_						
law (	equalization & activated s	TUQQE									
law (	equalization & activated s	ruoge		tiary tre		0.005	0.01				
	equalization & activated s  Manufacture of bakery produ	ucts	Ter	rtiary tre				0.004			
117     	Manufacture of bakery produ Bread Rusk	ucts tn tn	of of	product		0.005 0.11 0.11		0.004 0.004			
117       	Manufacture of bakery produ Bread Rusk Dry pastry	ucts tn tn tn	of of of	product product product		0.005 0.11 0.11 0.7		0.004 0.005			
! 17   ! !	Manufacture of bakery produ Bread Rusk	ucts tn tn tn	of of of	product		0.005 0.11 0.11		0.004			
! 17 ! ! !	Manufacture of bakery produ Bread Rusk Dry pastry	ucts tn tn tn tn	of of of	product product product		0.005 0.11 0.11 0.7		0.004 0.005			
1117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry	ucts tn tn tn tn	of of of of	product product product		0.005 0.11 0.11 0.7		0.004 0.005			
1117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner	tn tn tn tn	of of of of	product product product product product	23	0.11 0.11 0.7 9	0.01	0.004 0.005			
1117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production	tn tn tn tn tn	of of of of	product product product product product	23 sludge	0.11 0.11 0.7 9	0.01	0.004 0.005			
	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production	tn tn tn tn tn	of of of of	product product product product product	23 sludge	0.005 0.11 0.11 0.7 9	0.01 75 0.02	0.004 0.005			
117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production	tn tn tn tn tn tn	of of of of	product product product product product	23 sludge	0.005 0.11 0.11 0.7 9	0.01 75 0.02	0.004 0.005			
117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production Water conservat Above & recycl	tn t	of of of of	product product product product product product	23 sludge water 3-48	0.005 0.11 0.11 0.7 9 20 0.09 0.004	75 0.02 0.003	0.004 0.005			
117   	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry	ucts tn tn tn tn	of of of	product product product		0.005 0.11 0.11 0.7		0.004 0.005			
! 17 ! ! ! !	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production	tn tn tn tn tn	of of of of	product product product product product	23 sludge	0.005 0.11 0.11 0.7 9	0.01 75 0.02	0.004 0.005			
117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production Water conservat Above & recycl	tn tn tn tn tn tn	of of of of	product product product product product	23 sludge	0.005 0.11 0.11 0.7 9 20 0.09 0.004	75 0.02 0.003	0.004 0.005			
1117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production Water conservat Above & recycl	tn tn tn tn tn tn	of of of of	product product product product product	23 sludge	0.005 0.11 0.11 0.7 9 20 0.09 0.004	75 0.02 0.003	0.004 0.005			
117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production Water conservat Above & recycl	tn t	of of of of	product product product product product product	23 sludge water 3-48	0.005 0.11 0.11 0.7 9 20 0.09 0.004	75 0.02 0.003	0.004 0.005			
1117	Manufacture of bakery produ Bread Rusk Dry pastry Wet pastry Sugar factories and refiner Beet sugar production Water conservat Above & recycl	tn t	of of of of & a	product product product product product product	23 sludge water 3-48 sludge	0.005 0.11 0.11 0.7 9 20 0.09 0.004	75 0.02 0.003 6.3	0.004 0.005			

Model for Liquid Waste Inventories and Controls - Cont'd

				MACTE	B00 <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
		UI (l	7) 411,	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kġ/IJ Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Canned soups & baby foods	tn	of	product	22	12	7.6	0.47	0.18	011	2.4
Tomato-cheese-starch										
combinations	tn	of	product	2.9	7.2	6	0.23	0.28	011	4.7
Sauced vegetables	tn	٥f	product	85	25	21	1.1	0.33		
Sweet syrups, jams										
& jellies	ţη	φf	product	2.4	5.1	1	0.04	0.05	011	0.6
Chinese & Mexican foods	tn	of	product	14	6.9	2.8	0.28	0.14	011	3
Breaded frozen products	tn	of	product	48	26	26	2.6	0.35		
	\$+=	Ьŝ	lization	laggons	0.03	0.05		0 i 1		0.05
	366		Activated		0.05			011		0.05
100										
Egg breaking US facilities Dutch facilities	tn	tn	product of eggs	10.3	33 12.4					
US facilities	tn	tn	•		12.4					
US facilities	ŧn	tn Do	of eggs	7.9 0.0039	12.4					
US facilities	tn	tn Do	of eggs zen eggs Activated	7.9 0.0039	12.4 0.006					
US facilities Dutch facilities		tn Đo	of eggs zen eggs Activated Rotatir	7.9 0.0039 d sludge ng disks	12.4 0.006 0.1 0.077		3 7	1		
US facilities Dutch facilities  Wheat, starch gluten	tn	tn Do	of eggs zen eggs Activated Rotatin	7.9 0.0039 d sludge ng disks	12.4 0.006 0.1 0.077	81	3.7	1		
US facilities Dutch facilities  Wheat, starch gluten Starch and glucose	tn tn	tn Do	of eggs zen eggs Activated Rotatin product	7.9 0.0039 d sludge ng disks 9.9 33	12.4 0.006 0.1 0.077 94 13.4	81 9.7		1	\$0.	337
US facilities Dutch facilities  Wheat, starch gluten	tn tn	tn Do	of eggs zen eggs Activated Rotatin	7.9 0.0039 d sludge ng disks	12.4 0.006 0.1 0.077	81	3.7	1	\$0 <sub>4</sub>	337

### Model for Liquid Waste Inventories and Controls - Cont'd

	11417.7	UACTE	80D <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutant
	UN)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pnt
13 B	Beverage Industries							
131 D	Distillery, rectifying and blending spi	rits						
G	irain distilleries <sup>15</sup> tn anhydrous alcoh	ol 63	216	257				
	Aera	l ted lag <del>oo</del> n	0.043	0.077				
	Activa	ted sludge	0.043	0.077				
м	dolasses distilleries <sup>16</sup> tn anhydrous alc	oho1 63	220	300				
	iugar cane distilleriestn anhydrous alc		426					
W	/ine distilleries to anhydrous alcoh		210	75				
	tn of grap	es 3.6	2.1	0.75				
	Aera:	ا ted lagoon	0.001	0.002				
132 W	Activa	ted lagoon ted sludge	0.001 0.001	0.002 0.004				
		ted sludge						
	Activation  Fine production  In of grape	ted sludge	1.6	0.004				
	Activation	es 2	0.001	0.004				
	Activation  Jine production  In of grape  Rotating biological contactor & sa	es 2 and filter	0.001 1.6 0.065	0.004				
₩	Activation  Jine production  The production  Rotating biological contactor & so  Activated sludge /Extended	es 2 and filter	1.6 0.065 0.055	0.004 0.3 0.01 0.01				
W 133 M	Activa-  Activa-  Activa-  Activa-  Activa-  Activa-  Activated sludge / Extended  Activated sludge / Con	es 2 and filter	1.6 0.065 0.055	0.004 0.3 0.01 0.01				
133 M B M	Activation  Jine production  The production  Rotating biological contactor & so Activated sludge / Extended Activated sludge / Contactor  Balt liquors and malt  Reer manufacturing Balting  The production	es 2 and filter d aeration	1.6 0.065 0.055	0.004 0.3 0.01 0.01				
:133 M B M	Activation  Jine production  Rotating biological contactor & so Activated sludge /Extended Activated sludge / Contactor Activated sl	es 2  and filter d aeration nventional	0.001 1.6 0.065 0.055 0.03	0.004 0.3 0.01 0.01 0.01				
133 M B M	Activation  Fine production  Fine production  Rotating biological contactor & sa Activated sludge /Extended Activated sludge / Contact Activated sludge / Co	es 2  and filter diaeration nventional	0.001 1.6 0.065 0.055 0.03	0.004 0.3 0.01 0.01 0.01 0.85 3.9				
133 M B M	Activation  Jine production  Rotating biological contactor & so Activated sludge /Extended Activated sludge / Contactor Activated sl	es 2  and filter diaeration nventional	0.001 1.6 0.065 0.055 0.03	0.004 0.3 0.01 0.01 0.01				
133 M B M	Activation  Activation  Activation  Activated sludge / Extended Activated sludge / Contactor & same ac	es 2  and filter diaeration eventional  eventional	0.001 1.6 0.065 0.055 0.03	0.004 0.3 0.01 0.01 0.85 3.9 7.3				
133 M B M	Activation  Activation  Activation  Activated sludge / Extended Activated sludge / Contactor & same ac	es 2  and filter diaeration nventional  2y 7.3  2 7.4  treatment	0.001 1.6 0.065 0.055 0.03	0.004 0.3 0.01 0.01 0.01 0.85 3.9				
133 M B M	Activation  Fine production  Fine production  Rotating biological contactor & say Activated sludge / Extended Activated sludge / Contactor & say Activated s	es 2  and filter d aeration eventional  2 7.3 er 5.4 er 11  treatment ow loading	0.001 1.6 0.065 0.055 0.03 5 10.5 18.8	0.004 0.3 0.01 0.01 0.85 3.9 7.3 0.37				

<sup>15.</sup> One bushel (35.2 lt or 27.2 kg) of grain yields 17.8 lt of anhydrous alcohol.

<sup>2.4</sup> It of molasses yield 1. It of anhydrous alcohol.

Model for Liquid Waste Inventories and Controls - Cont'd

				80D <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
	-	(U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
3134 Soft drinks									
Major plant With syrup prepar'on Franchise plant With no syrup prepar'on	m3 o1	f product	12.8	3.1	4.3				
Bottled		f product	4.3	2.1	0.7				
Canned	m3 o	f product Aerated Activated	_	0.8	0.3				•

### DIVISION 32. TEXTILE, WEARING APPAREL & LEATHER INDUSTRIES

#### 321 Manufacture of Textiles

Wool processing 17			,			
Ave unscoured stock 18	tn of wool	544	314	196	0i1	191
					Cr	1.33
					Pheno 1	0.22
Ave scoured stock	tn of wool	537	87	43	Cr	1.33
					Pheno 1	0.17
Process-specific						
Scouring	tn of wool	17	227	153	011	191
Dyeing	tn of wool	25	22		Ċr	1.33
					Pheno 1	0.17
Washing	tn of wool	362	63			
Carbonizing	tn of wool	138	2	44		
Bleaching	tn of wool	12.5	1.4			
Cotton processing	•					
Ave compounded <sup>19</sup>	tn of cotton	265	155	70		
Process-specific	•					
Yarn sizing	tn of cotton	4.2	2.8			
Desizing	tn of cotton	22	58	30		
kiering	tn of cotton	100	53	22		
Bleaching	tn of cotton	100	8	5		

<sup>17.</sup> The p<sub>H</sub> varies widely, from 1.9 to 10.4.

<sup>18.</sup> The average compounded load factors listed are based on the assumption that only 20 % of the product is mercerized and 10 % is bleached.

<sup>19.</sup> The average compounded load factors listed are based on the assumption that only 35 % of the product is mercerized, 50 % of the product is dyed and 14 % of the product is printed.

 ${\bf Model\ for\ Liquid\ Waste\ Inventories\ and\ Controls\ -\ Cont'd}$ 

	UNIT	WASTE	BOD <sub>5</sub>	T\$\$	Tot N	Tot P	Other Pol	lutants
	(U)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/V Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Mercerizing	tn of cotton	35	8	2.5				
Dyeing	tn of cotton	50	60	25				
Printing	tn of cotton	14	54	12				
Rayon processing	tπ of rayon	42	30	55				
Acetate process.	tn of acetate	75	45	40				
Nylon process.	tn of nylon	125	45	30			1	
Acrylic process,	th of acrylic	210	125	87				
Polyester process.	tn of polyester	100	185	95				
	Sedime	ntation	0.6	0.4				
	Coagulation / Sedimen	ntation	0.6	0.15				
	Anaerobic	lagoon	0.2	0.3				
	Aerobic	lagoon	0.05	0.05				
	A = 4 4 4			0.05				
Manufacture of Leathe	Activated		0.1	V.U3	·			
Manufacture of Leathe	r & Products of Leath		0.1	0.05				
i Tanneries and leather 1. Hair pulp, Chrome t	r & Products of Leath		63.5	104.	12		011	57.8
l Tanneries and leather	r & Products of Leath	er			12		0il Sulfide	<b>57</b> .8 3.35
i Tanneries and leather 1. Hair pulp, Chrome t	r & Products of Leath	er			12			
Tanneries and leather 1. Hair pulp, Chrome t	r & Products of Leath	er			12		Sulfide	3.35
i Tanneries and leather  1. Hair pulp, Chrome tretan, wet finish  2. Hair save, Chrome t	<b>r &amp; Products of Leath</b> finish <sup>20</sup> an, tn of hides	er			12.8		Sulfide Cr	3.35 4.76
l Tanneries and leather 1. Hair pulp, Chrome t retan, wet finish	<b>r &amp; Products of Leath</b> finish <sup>20</sup> an, tn of hides	er 57	63.5	104.			Sulfide Cr Phenol	3.35 4.76 0.11
i Tanneries and leather  1. Hair pulp, Chrome tretan, wet finish  2. Hair save, Chrome t	<b>r &amp; Products of Leath</b> finish <sup>20</sup> an, tn of hides	er 57	63.5	104.			Sulfide Cr Phenol	3.35 4.76 0.11
i Tanneries and leather  1. Hair pulp, Chrome tretan, wet finish  2. Hair save, Chrome t	<b>r &amp; Products of Leath</b> finish <sup>20</sup> an, tn of hides	er 57	63.5	104.			Sulfide Cr Phenol Oil Sulfide	3.35 4.76 0.11 13.1 1.94
i Tanneries and leather  1. Hair pulp, Chrome tretan, wet finish  2. Hair save, Chrome t	<b>r &amp; Products of Leath</b> finish <sup>20</sup> an, tn of hides	er 57	63.5	104.			Sulfide Cr Phenol Oil Sulfide Cr	3.35 4.76 0.11 13.1 1.94
I Tanneries and leather  1. Hair pulp, Chrome to retan, wet finish  2. Hair save, Chrome to retan, wet finish  3. Hair pulp or save, non chrome tan,	r & Products of Leath finish <sup>20</sup> an, th of hides	er 57	<b>63</b> .5	104. 199.	12.8		Sulfide Cr Phenol Oil Sulfide Cr Phenol	3.35 4.76 0.11 13.1 1.94 - 0.24
<ol> <li>Tanneries and leather</li> <li>Hair pulp, Chrome tretan, wet finish</li> <li>Hair save, Chrome tretan, wet finish</li> <li>Hair pulp or save,</li> </ol>	r & Products of Leath finish <sup>20</sup> an, th of hides	er 57	<b>63</b> .5	104. 199.	12.8		Sulfide Cr Phenol Oil Sulfide Cr Phenol	3.35 4.76 0.11 13.1 1.94 - 0.24
I Tanneries and leather  1. Hair pulp, Chrome to retan, wet finish  2. Hair save, Chrome to retan, wet finish  3. Hair pulp or save, non chrome tan,	r & Products of Leath finish <sup>20</sup> an, th of hides	er 57	<b>63</b> .5	104. 199.	12.8		Sulfide Cr Phenol Oil Sulfide Cr Phenol Oil Sulfide	3.35 4.76 0.11 13.1 1.94 - 0.24 17.3 3.43
<ol> <li>Tanneries and leather</li> <li>Hair pulp, Chrome tretan, wet finish</li> <li>Hair save, Chrome tretan, wet finish</li> <li>Hair pulp or save, non chrome tan, retan, wet finish</li> <li>Retan &amp; wet finish</li> </ol>	r & Products of Leath finish <sup>20</sup> an, th of hides	er 57	<b>63</b> .5	104. 199.	12.8		Sulfide Cr Phenol Oil Sulfide Cr Phenol Oil Sulfide Cr	3.35 4.76 0.11 13.1 1.94 - 0.24 17.3 3.43 0.06
I Tanneries and leather  1. Hair pulp, Chrome tretan, wet finish  2. Hair save, Chrome tretan, wet finish  3. Hair pulp or save, non chrome tan, retan, wet finish	r & Products of Leath finish <sup>20</sup> an, th of hides an, th of hides th of hides	er 57 44	63.5 67.3	104. 199. 96.7	12.8		Sulfide Cr Phenol Oil Sulfide Cr Phenol Oil Sulfide Cr Phenol	3.35 4.76 0.11 13.1 1.94 - 0.24 17.3 3.43 0.06 0.39
<ol> <li>Tanneries and leather</li> <li>Hair pulp, Chrome tretan, wet finish</li> <li>Hair save, Chrome tretan, wet finish</li> <li>Hair pulp or save, non chrome tan, retan, wet finish</li> <li>Retan &amp; wet finish</li> </ol>	r & Products of Leath finish <sup>20</sup> an, th of hides an, th of hides th of hides	er 57 44	63.5 67.3	104. 199. 96.7	12.8		Sulfide Cr Phenol Oil Sulfide Cr Phenol Oil Sulfide Cr Phenol	3.35 4.76 0.11 13.1 1.94 - 0.24 17.3 3.43 0.06 0.39

<sup>20.</sup> Typical weight of big hides (from cattle or horse) is 25-26 kg, while that of small hides (from sheep or goat) 3 kg.

Model for Liquid Waste Inventories and Controls - Cont'd

		WASTE	800 <sub>5</sub>	T\$\$	Tot N	Tot P	Other Pol	lutants
	UNIT (U)	MASTE WOLUME	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/V Pntr	Name	kg/U Pnt:
5. No beamhouse tanneries (tan, retan & wet finish)	tn of hides	56	39.2	49.2	5		Oil Sulfide Cr Phenol	86.3 0.01 2.21
6. Through-the-Blue (hair removal & Chrome tan of cattlehides)	tn of hides	17	130	200	20.3		Oil Sulfide Cr Phenol	17.3 7.6 6.3 0.11
7. Shearling tanneries (tan & finish sheepskins with wool intact)	tn of hides	78	57	77.7	4		Oil Sulfide Cr Phenol	15.3 0.54 7.4
8. Pigskin tanneries (same process as that of category 1)	tn of hides	42	115	181	5.7		Oil Sulfide Cr Phenal	64 12.1 4.4 0.03
9. Retan & wet finish (splits)	tn of hides	27	16.9	23.8	3.9		0il Sulfide Cr Phenol	19.3 0.03 1.07 0.03
	Primary sedim	entation	0.6	0.42	0.74	ļ	0il Sulfide Cr	0.: •
Sulfide ox	idation/sedim	entation	0.56	0.32	2 0.74	ļ	Oil Sulfide Cr	0.; 0
oagulation with chemical addit	ion and sedim	entation	0.52	2 0.09	0.58	3	Oil Sulfide Cr	0. • 0.1
Activated sludg	e (extended a	eration)	0.0	2 0.1	0.60	5	0il Sulfide	0.

### Model for Liquid Waste Inventories and Controls - Cont'd

1		111	NIT	WASTE	8005	TSS	Tot N	Tot P	Other Pol	llutants
		-	u)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
331	Manufacture of Wood & Wood	& Cork	Products	, Except	Furnit	ure				
	Plywood manufacturing Fiberboard manufacture	tn of	1000 m2 product	4.1 20	4 12.5	1.1 20	0.24		Phenol	5

### DIVISION 34. MANUFACTURE OF PAPER & PAPER PRODUCTS, PRINTING & PUBLISHING

### 341 Manufacture of Paper and Paper Products

#### 3411 Manufacture of pulp, paper and paperboard

Pulp mils					
Wood pulp					
Mechanica l	tn of	product			
Sulfate (Kraft) <sup>21</sup>	tn of	product	61.3	31	18
Sulfite	tn of ;	product	92.4	130	26
Semi chemical	tn of	product	47	27	12.5
Paper mills					
Newsprint paper	tn of	product	190	7.5	2
Kraft coarse paper	th of p	product	125	5.5	10.5
Cigarette paper	tn of p	product	100	11.5	37.5
Paperboard/Simple finish	tn of p	product	200	15	30
Graphic paper	tn of p	product		10.5	6.5
		Sedime	entation	0.75	0.75
Di	ssolved	air flo	patation	0.65	0.15
	Ac	ctivated	d sludge	0.05	0.1
		Aerated	lagoon	0.3	0.1
	tabiliza	ation la	agooning	0.6	0.1

<sup>21.</sup> The processes considered are pulping, pulp screening, pulp washing and thickening.

# Model for Liquid Waste Inventories and Controls - Cont'd

•		BOD <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
Ψ11T (U)	WASTE VOLUME m <sup>3</sup> /U		kg/U Pntr			Name	kg/U Pntr

DIVISION 35. MANUFACTURE OF CHEMICALS & OF CHEMICAL, PETROLEUM, COAL, RUBBER & PLASTIC PRODUCTS

### 351 Manufacture of Industrial Chemicals

3511 Manufacture of basic industrial chemicals except fertilizers<sup>22</sup>

Primary Petrochemicals						
Ethylene	tn of product	3.2	1.8			
Propylene	tn of product	4.4	2.4			
Primary Intermediates					6/1	11
Ammonia	tn of product	6.9	0.4	0.1	011	11
Butanol (Butyl Alcohol)	tn of product	4.6	10.3			
Chlorinate hydrocarbons	tn of product	2.2	0.22			
Ethanol (Ethyl Alcohol)	tn of product	9	14.9			
Ethyl benzene	tn of product	6.9	12			
Methanol (Methyl Alcohol	) tn of product	6.9	4.4		011	1.2
Toluene	tn of product	6.9	9.7			
Xylene	tn of product	6.9	15.5			
Secondary Intermediates						
Acetic anhydride	tn of product	18.7	50			
Acetone	tn of product	4.2	12.6			
Acrylates	tn of product	8.3	23			
Acrylonitrile	tn of product	22.9	10			
Butylenes, Butadiene	tn of product	4.4	0.5			
Ethylene glycol						
(Ethanediol)	tn of product	14.6	29			
Formaldehyde (methanal)	tπ of product		٠		011	0.63
Glycerine, glycols	tn of product	14.6	29			
Phenol, Cumene	tn of product	6.2	34.7			
Styrene	tn of product	23.1	38			
Terephthalic acid	tn of product	8.3	16			
Vinyl chloride	tn of product	0.4	0.5			
Primary Polymers						
Butyl rubber	tn of product	16. <b>7</b>	23.4			
Polyvinyl chloride	tn of product	9.3	2.6			
Dyes and Pigments	tn of product	624.	18 <b>7</b> .			
Miscellaneous Organics						
Isocyanate	tn of product	31	54			
Parathion	tn of product	22.9	57			
Phenyl glycine	tn of product	31	54			
Tributyl phosphate	tn of product		13			

Waste volumes and 800 loads vary widely. In most cases other pollutants (SS, Nitrogen, Phenol, Oil, heavy metals and cyanide), as well as  $p_{\mbox{\scriptsize H}}$  and color, are present, but factors are not available. When these products are manufactured by petrochemical refineries, rather than from smaller installations, use the compounded factors applicable for refineries (SIC 3530).

Model for Liquid Waste Inventories and Controls - Cont'd

	UNIT	WASTE	B00 <sub>5</sub>	TSS	Tot N	Tot P	Other Pol	lutants
	(u)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Act	ivated sludge t	reatment	0.01					
	·							
Chlor-alkali <sup>23</sup>								
Memory cell								
	of Cl <sub>2</sub> product			5.6			Hg	0.15
Treated to	of Cl <sub>2</sub> product			0.32			Hg	. 0001
Diaphragm cell (Metal or Untreated tn		3}						
	of Cl <sub>2</sub> product			3.2			Pb	. 046
treated th	of Cl <sub>2</sub> product			0.32			Рb	. 0025
12 Manufacture of fertilizers	and pesticides							
Nitrogenous Fertilizers								
Ammonium nitrate								
Untreated	tn of product				2.9			
Treated	tn of product				0.1			
Ammonium sulphate								
Untreated	tn of product		0.4		10			
Treated	tn of product				0.1			
Urea								
Untreated	tn of product		0.24		10			
Treated	tn of product				0.1			
Phosphatic Fertilizers								
Phosphoric acid	tn of P <sub>2</sub> 0 <sub>5</sub>	670		3900	5	1724	Fluor	24625
(wet process)							Pb,As, Cr,Hg	1.1
Normal super phosphates	tn of P <sub>2</sub> 0 <sub>5</sub>			1.25		0.65	Fluoride	17.5
(Phosphate rock+H2SO4)								
Triple super phosphates (Phosphate rock+H3PO4)	tn of P <sub>2</sub> 0 <sub>5</sub>		0.55			0.32	Fluoride	7.8
N.P.P. fertilizer	tn of product			0.4	0.4			0.06

<sup>23.</sup> Controls in both, the Mercury and the Diaphragm Cell process, comprise Sulfide precipitation and possibly activated carbon treatment.

<sup>24.</sup> If the Hemihydrate, rather than Dihydrate, process is used, the applicable factor is 8.7.

<sup>25.</sup> If Fluorosilicic Acid is recovered from the exhaust gases, the applicable factor is 24.6.

Model for Liquid Waste Inventories and Controls - Cont'd

	INTT	WASTE	B00 <sub>5</sub>	TSS	Tot N	Tot P	Other Pol	lutants
	UNIT (U)	VOLUME m <sup>3</sup> /U	kg/V Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Total water recycle & treatment	of excess effl	uents <sup>26</sup>		0.0		0.0	Fluorid Pb,As,C	
Insecticides, Fungicides, D DDT	lisinfectants ef tn of Product	5.3				Chlore	0il obenzene	76 38
Chlorinated hydrocarbon herbicides	tn of Product	3.6	22. <b>7</b>	9			Phenol	4.9
3513 Manufacture of synthetic re Butadiene-Styrene Untreated	esins, plastic tn of product		made Ft	<sub>pers</sub> 27				
Butadiene-Styrene				<sub>pers</sub> 27				
Butadiene-Styrene Untreated Butadiene-Nitrile rubber Untreated Phenolic resins Untreated Good control Polyethylene	tn of product	4.1	1 <b>4</b>	3.7			Pheno 1	5.6
Butadiene-Styrene Untreated Butadiene-Nitrile rubber Untreated Phenolic resins Untreated Good control	tn of product tn of product tn of product	4.1	14 11	3.7			Pheno 1	5.6

<sup>26.</sup> The major effluents are from the gypsum filter, as well as from the  $P_2O_5$  condensers and off gas scrubbers. The gypsum filter separates the gypsum by-product (4.75 th of gypsum per th of P2O5) from the phosphoric acid solution.

The washed gypsum can be can be carried away as solid cake (with about 25 % water) and drystacked on land as a solid waste. The remaining scrubber/condenser wastes can be recycled through a cooling pond with an area of about 400 m<sup>2</sup> per daily tn of P205 production, or through a cooling tower. The latter reduces drastically the area requirements and is especially suited when fluoride is recovered from the off gas as hydro fluorosilisic acid.

Alternatively, the washed gypsum can be slurried and, mixed with scrubber/condenser waters, can be discharged either directly into the sea, or into a gypsum pond. In the latter case, the settled gypsum is continuously worked with drag lines and transferred to near-by gypsum piles, while the cooled water is recycled back to the process. Depending on the rainfall/evaporation balance, excess water may have to be discharged into the final receiver, but this can be treated so as to have very low loads.

<sup>27.</sup> The pollutant load factors vary widely

Model for Liquid Waste Inventories and Controls - Cont'd

	UNIT	WACTE	B00 <sub>5</sub>	TSS	Tot N	Tot P	Other Pol	lutants
	(U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
High density-solvent					***************************************			
Good control	tn of product		0.3	0.83				
High density-polyform			0.0	0.00				
Good control	tn of product		0.05	0.14				
Polypropylene								
Untreated	tn of product		5	1.16			0 i 1	3
Good control	tn of product		0.42	1.16			2	_
Polystyrene	•							
Untreated	tn of product		1.1	4.2				
Polystyrene-suspension	,							
Good control	tn of product		0.22	0.61				
Polystyrene bulk			*/	0.01				
Good control	tn of product		0.04	0.11				
PVC-emulsion	vii ov product		0.04	0.11				
Untreated	tn of product		0.1	15.5				
Good control	tn of product		0.1	0.36				
PVC-suspension	211 O. p. 00400		V.1	υ,υυ				
Good control	tn of product		0.36	0.99				
PVC-bu lk	en or product		0.50	V.33				
Good control	tn of product		0.06	0.16				
Rayon	th or product		0.00	0.10				
Untreated	tn of product		44	N/A			Sulfide	
	v. v. p. oddor		7	11/15			Ζn	3.5 12
							Mg CS <sub>2</sub>	2 1.5
							H <sub>2</sub> SO <sub>4</sub>	45
							SO <sub>4</sub>	540
Good control	tn of product		4.8	8.8			554	270
Nylon (polyamide)	·							
6+66 resin/Untreated	tn of product		68	4				
6 resin/Good control	tn of product		3.7	2.5				
66 resin/Good control	tn of product		0.66	0.44				
6+66 fibers/Untreated	tn of product		30	3				
6 fibers/Good control	tn of product		1.9	1.3				
66 fibers/Good control	tn of product		0.58	0.39				
Polyesters (e.g. dacron)	on or product		0,50	0.55				
Untreated	tn of product		11.5	6				
Resin/Good control	th of product		0.78	0.52				
Fiber/Good control	tn of product		0.78	0.52				
Resin+fiber continuous	an or product		0.70	0.52				
Good control	tn of product		0.78	0.52				
Resin+fiber batch	on or product		V.70	J. JE				
	tn of product		1.56	1.04				
Good control			1.30	1.04				
Good control ABS/SAN	The state of the s							
Good control ABS/SAN Untreated	tn of product		11.3	15			H <sub>2</sub> SO <sub>4</sub>	22

Model for Liquid Waste Inventories and Controls - Cont'd

			MATE	800 <sub>5</sub>	TSS	Tot N	Tot P	Other Po	llutant:
		) //	WASTE VOLUMË m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/V Pntr	kg/U Pntr	Name	kg/U Pnt
Good control	tn of	product		0.63	1.2				
Cellophane									
Untreated	tn of	product		76.5	38				
Good control	tn of	product		8.7	16				
Cellulose acetate									
Untreated	tn of	product		38	11				
Resin or fiber									
Good control	tn of	product		4.1	2.7				
Resin and fiber									
Good control	tn of	product		8.3	5.5				
Acrylic resin									
Untreated	tn of	product		25	1.1				
Good control	tn of	product		2.75	1.1				
Epoxy resins									
Untreated	tn of	product		70	14.5			NaOH	11
Batch & continuous	tn of	product		2.1	1.4				
Batch fusion	tn of	product		0.25	0.17				
Urea and Melamine resins									
Good control	tn of	product		0.2	0.13				
Manufacture of Other Chements 22 Manufacture of drugs and remaining the contract of drugs and drugs									
	tn o	f product		2050	834	279	40	0i1	104
Fermentation products									
Fermentation products Biological & natural exact	tion					~		Oil	0.3
		f product		210	64	6	4		_
Biological & natural exac	tn o	f product f product		210 210	64	6	4	Oil	
Biological & natural exact Blood fractionation	tn o	f product				-	4	0il 0il	
Biological & natural exact Blood fractionation Vaccine production	tn o	f product		210	64	6	4	Oil	0.3 4.5

Model for Liquid Waste Inventories and Controls - Cont'd

	UNIT	LIACTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other Pol	llutants
	(U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
3 Manufacture of soap and c	leaning preparat	ions						
Soap Production								
Soap from kettle boilin Soap from fatty acids Fatty acids:	g tπ product	4.5	6	4			011	0.9
Production	tn product	13.528	12	23			Oil	2.5
Hydrogenation	to product		1.5	1			Oil	1
Neutralization	tn product		0.1	0.2			011	0.05
Glycerine concentrati			•	U.4			<b>V</b> 11	0.03
(1st step)	in product		15	2			011	1
Glycerine distillatio			10	_			VII	1
(2nd step)	tn product		5	2			Oil	,
Soap Processing	Product		3				UII	1
Soap flakes and powders	in product		0.1	0.1			041	۸ ۰
Bar soaps	tn product		3.4	5.8			011	0.1
Liquid soaps	tn anhydr soap		0.1	0.1			011	0.4
Detergents	on amyar soup		0.1	V.1			<b>Q</b> 11	0.1
Sulfonation								
Oleum sulfonation	th anhydr prod		0.2	0.3			Surfact	0.7
	* '						017	0.3
Air-\$03 sulfation &							Ψ.,	0.5
sulfonation	tn anhydr prod		3	0.3			Surfact	3
	, ,		·	J			Oil	0.5
\$03 solvent and							011	0.5
vacuum sulfonation	tn anhydr prod		3	0.3			Surfact	3
	• •		-				0i1	0.5
Sulfamic acid							011	0.5
sulfation	tn anhydr prod		3	0.3			011	0.5
Chlorosulfonic acid	• •		•	2.0			<b>U</b> 11	V.J
sulfation	tn anhydr prod		3	0.3			Surfact	3
	- '		_	7.0			011	0.5
Spray-dried detergents							<b>3</b> 71	0.5
W/o use of scrubbers	tn anhydr prod		0.1	0.1			Surfact	0.2
With use of scrubbers			0.8	0.1			Surfact	1.5
	•						Oil	0.3
Liquid detergents	tn anhydr prod		2				Surfact	
	- , -		-				54,7401	
Dry detergent blending	tn anhydr prod		0.1	0.1			Surfact	0.1
Detergent bars & cakes	tn anhydr prod		7	2			Surfact	5
				-			011	0.2

<sup>28.</sup> The listed factor accounts also for the waste volumes from the fatty acids hydrogenation and neutralization.

Model for Liquid Waste Inventories and Controls - Cont'd

			80D <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
	UNIT (U)	WASTE VOLUME π <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
		Separators					011	0.15
	Floatation without						011	0.25
	Floatation with						011	0.1
	Biological		0.1	0.1			Surf	actant 0.1
	_						0i1	0.1
			l					
			<b></b>	1				
3529 Manufacture of chemic	al products not el	sewhere cla	3\$\$1T1 <del>0</del> C					
Animal glue								

421

457

426

Floatation Sedimentation Biological treatment

tn of product

tn of product

tn of product

2500

580

280

4250

1920

400

353 Petroleum Refineries<sup>29</sup>

From fleshings

From chrome stock

From hides

•	1 ELIO ICAM No. IIICI 100								
	Topping refinery <sup>30</sup>	1000 m3 of crude	484	3.4	11.7	1.2	Oil Phenol Sulfide Cr	8.3 .034 .054 .007	
	Cracking refinery <sup>31</sup>	1000 m3 of crude	605	<b>7</b> 2.9	18.2	28.3	Oil Phenol Sulfide Cr	31.2 4 0.94 0.25	

The pollutant loads refer to relatively modern refineries, after their API separators. 29.

Topping Refineries contains the primary and fundamental processes (atmospheric and vacuum 30. crude oil distillation, steam cracking of gas oils, catalytic reforming, Naphtha- Distillateand heavy oil-HDS, isomerization, sulfur recovery etc.), but can be considerably more complex as they may include aromatics extraction (BTX), lub oil and asphalt production units.

Cracking Refineries are considerably more complex than topping refineries and can be equipped 31. with catalytic cracking, hydrocracking and/or coking (either of these units qualifies a refinery to be in the cracking category).

Model for Liquid Waste Inventories and Controls - Cont'd

	UNIT	WASTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other Pol	lutants
	(U)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Petrochemical refinery <sup>32</sup>	1000 m3 of crude	726	172	48.6	34.3		0il Phenol	52.9 7.7
							Sulfide Cr	.86 .234
Lub oil refinery <sup>33</sup>	1000 m3 of crude	1090	217	71.5	24.1		0 i 1	120
							Pheno 1	8.3
							Sulfide C-	.014
							Çr	.046
Integrated refinery <sup>34</sup>	1000 m3 of crude	1162	197	58.1	20.5		Oil	74.9
							Pheno1	3.8
							Sulfide	2
· <u></u>							Cr	0.49
Coagula	ation and air floa	tation	0.65	0.67			017	0.15
							Pheno 1	0.1
							Sulfide	1
	Activated	sludge	0.17	0.25			Øil	0.04
							Pheno 1	0.1
							Sulfide	0.04
	Trickling	filter	0.3	0.25			<b>0</b> i 1	0.04
							Pheno 1	0.1
							Sulfide	0.1
	Aerated	lagoon	0.3	0.8			011	0.04
							Pheno 1	0.1
							Sulfide	0.04
	Oxidatio	n pond	0.4	0.55			Oil	0.04
							Pheno 1	0.1
							\$ulfide	0.2
				0.0				

<sup>32.</sup> Petrochemical are similar to Integrated refineries, but without lub oil production.

<sup>33.</sup> Lub 0il Refineries are comparable to integrated refineries, but without the aromatics extraction and petrochemicals production units.

<sup>34.</sup> Integrated Refineries are the most complex type of refinery comprising all major operations, including cracking, lub oil, and petrochemicals production units.

Model for Liquid Waste Inventories and Controls - Cont'd

	······································			80D <sub>5</sub>	TSS	Tot N	Tot P	Other Poll	utants 
		UNIT (U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr		kg/U Pntr	Name	kg/U Pntr
54	Manufacture of Miscellaneous P	roducts of P	etro leum	and Co	al				
	Building felt and tar paper tr	of product	50	8	40				
	Coke Plant								
	Untreated	tn of coke	14.7	3.9		3.5		Phenol CN Thioc/te	0.28 0.61 2.1
	Old Plants	tn of coke	9.9	0.7	: .	3.5		Phenol CN Thioc/te	0.28 0.03 0.13
	Base level treatment <sup>35</sup>	tn of coke	9.9	0.3		3.5		Phenol CN Thioc/to	.015
	Biological treatment	tn of coke	1.6	0.3		3.5		Phenol CN Thioc/t	0.07 0.02 e 0.08
355	Manufacture of Rubber Product	s	•		•				
355	1 Tire and tube industries t	n of product	37	0.4	1			011	0.12

# DIVISION 36. MANUFACTURE OF NONMEYALLIC MINERAL PRODUCTS EXCEPT PRODUCTS OF PETROLEUM AND COKE

#### 362 Manufacture of Glass and Glass Products

Plate glass						
Untreated	tn of product	45.9	2.3	690		
Chemical Sedimentation	tn of product	45.9		2.76		
2ary Sedimet'n+Filtr'n	tn of product			. 045		
Float glass						
Untreated	tn of product	. 14	.001	. 002	011	.001
Chemical Sedimentation	tn of product	0.14		.001	0i1	. 001
2ary Sedimet'n+Filtr'n	tn of product	0.14		.001	017	.001
Windshield glass					•	
Untreated	1000 m <sup>2</sup> of glass	4.9	0.73	4.90	· 0i1	0.64
Chemical Sedimentation		4.9		1.95	. 011	0.64

<sup>35.</sup> The base level treatment comprises the use of free and fixed ammonia stills, dephenolizers, and recirculated final coolers with cooling tower blowdown.

Model for Liquid Waste Inventories and Controls - Cont'd

UNIT	WASTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
(U)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/V Pntr	kg/U Pntr	kg/V Pntr	Name	kg/U Pntr
2ary Sedimet'n+Filtr'n 1000 m <sup>2</sup> of glass Sheet glass Rolled glass	4.9		0.24 cooling			011	0.49

### DIVISION 37. BASIC METAL INDUSTRIES

### 371 Iron and Steel Basic Industries

. Iron and Steel Basic Indu	stries						
Iron and steel mills							
Blast furnace (Scrubber	wastes	)					
Untreated	tn of	product	12.3	29.3	0.27	Pheno T F CN	0.01 .023 .039
Sedimentation	tn of	product	12.3	1.5	0.27	Phenol F CN	0.01 .023 .039
Chemical coagulation & alkaline chlorinati	tn of on	product	12.3	. 13	.018	Phenol F CN	.001 .023 .0001
Recycling/5% blowdown & alkaline chlorinati	tn of on	product	0.55	. 006	.001	Pheno 1 F CN	0.0 .0005 0.0
Basic oxygen furnace							
Precipitator/quencher							
Untreated	to of	product	0.6	0.40			
Floc'tion/sedim'tion		product	0.6	.049 .011			
Venturi/quencher	01	b, ocact	V.0	.011			
Untreated	tn of	product	1.9	.146			
Floc'tion/sedim'tion		product	1.9	. 034			
Off-gas system		•		, 00-7			
Untreated	tn of	product	0.5	. 036			
Floc'tion/sedim'tion		product	0.5	.009			
Electric arc furnace							
Venturi/quencher			•				
Untreated	to of	product	4.6	5 2C			
Floc'tion/sedim'tion		product	4.6	0.36 0.09			
The second secon	JN 01	p. ouect	™ - LJ	0.09	•		

Model for Liquid Waste Inventories and Controls - Cont'd

	14177	LACTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other	Pollutants
	UNIT (U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	_	kg/V Pntr	kg/U Pntr	Name	kg/U Pntr
Open hearth furnace								
Venturi/quencher								
Untreated	tn of product	3.5		0.27				
Floc'tion/sedim'tion	tn of product	3.5		.065	•			
Hot-rolling mills								
Untreated	tn of product	42		33.9			011	1.87
Scale pits	tn of product	42		10.8			Oil	1.87
Deep bed filters	tn of product	42		0.76			011	0.25
Settling & WW recycling	tn of product	2.3		0.04			011	.015
Cold rolling								
Untreated	tn of product	6.7	2.2	0.71			011	2.05
H <sub>2</sub> SO <sub>4</sub> pickling								
Carbon steel	tn of product	1.8					Fe	6.4
Stainless steel	tn of product	1 - 4					SO4 Fe	22.1
	*** ** ***	7					504	9.1
Alloys	tn of product	1.2					Fe	2.6
							S04	9.8
HC1 pickling								
Carbon steel	tn of product	1.2					Fe	. 18.4
							CT	24.8
Stainless steel	tn of product	1.6					Fe	57.8
							c)	76.2
Alloys	tn of product	1.1					Fe	33.7
							Сì	44.5
Ga Ivanizing								
Untreated								
Hot dip	tn of product	9.4		2.32		0.02	Fe	0.19
							Zn	. 007
							Cr	.015
Electrogalvanizing	tn of product	6.9		N/A			Zn	. 405
Treated	tn of product			.125			0 i 1	
							F€	. 007
							Žn	.009
							Cr	. 004

Model for Liquid Waste Inventories and Controls - Cont'd

	•			800 <sub>5</sub>	TS\$	Tot N	Tot P	Other Po	llutants
		UNIT (U)	WASTE VOLUME m <sup>3</sup> /U	/OLUME kg/V /	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
72	Non-Ferrous Metal Basic	Industries							
	Primary Aluminum Product	ton							
	Alumina from bauxite <sup>30</sup>	5.37 tn of Alumina			2.4			011	0.24
								\$0 <sub>4</sub>	2.3
								Fluor	2.2
								Zn	.008
								Cu	. 002
		tn of Aluminum			4.5			011	0.46
								S0 <sub>4</sub>	4,4
								Fluor	4.2
								' Zn	.016
								Си	.003
	Aluminum from Alumina								
	Anode pre-baking	tn of product			5.0			011	0.03
								Fluor	0.12
	Reduction cells	tn of product		2.0	14.5	0.04		F <sub>2</sub>	5.5
								Fluor	1.5
	Secondary Aluminum								
	Sme Iting	tn of product	0.008		1.5				
	Casting & foundry	tn of product	0.02					011	0.65
	Primary Lead								
	Untreated	tn of product			350				
	Primary zing								
	Untreated	tn of product			0.9			Zn S <b>O</b> 4	1.8 30

<sup>36.</sup> From 1.4 to 3.3 tons of Bauxite Ore processed, 1.0 ton of alumina is produced. The latter yields 526 kg of Aluminum.

<sup>37.</sup> Red muds, 675 kg/tn of alumina, may be discharged as suspended solids if they are not removed from the effluents.

Model for Liquid Waste Inventories and Controls - Cont'd

		UNIT	DACTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other Po	llutants
		UNIT (U)	WASTE VOLUME m <sup>3</sup> /U	kg/V Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
381	Manufacture of Fabricated Meta	1 Products,	Except M	lachiner	y & Equ	ipment			
	Electroplating38.39								
	Degreasing baths	1000 m <sup>2</sup>						011	5
	Pickling baths								
	Steel	1000 m <sup>2</sup>						Fe Cl <sup>-</sup>	25 0.12
	Brass	1000 m <sup>2</sup>						Cu Zn	23 15
	Alkaline pickling for Al	1000 m <sup>2</sup>		·				Al NaOH	55 <b>43</b> 0
	Nickel bright	1000 m <sup>2</sup>						N 1 SO <sub>4</sub>	25 33
		Base t Stage I t	reatment reatment	} !				Ni Ni	0.06 0.009
	Chromium ornamental	1000 m <sup>2</sup>						Cr <sup>6</sup>	37
		Base t Stage I t	reatment reatment	)				Cr <sup>6</sup> Cr <sup>6</sup>	0.06 0.009
	Žino bright								
	Cyanide bath	1000 m <sup>2</sup>	<u>.</u>					Oil Zn CN NaOH	0.5 6.9 15 50
	Non-cyanide bath	1000 m <sup>2</sup>	?					Oil Zń NaOH	0.5 3 47

The Base Treatment comprises neutralization and segregated chemical treatment of organic and 38.

The Stage I treatment comprises recycling of cooling water, multi-tank rinsing, reclamation 39. of drag-out, neutralization, and segregated chemical treatment of organic and chromium  ${\sf VI}$  .

 $\label{thm:model} \textbf{Model for Liquid Waste Inventories and Controls - Cont'd}$ 

	UNIT	WASTE	BOD <sub>5</sub>	TSS	Tot N	Tot P	Other Po	ollutants
	(U)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pntr
Acid bath	1000 m <sup>2</sup>				0.7		0 í 1 Zn	0.5 8.0
	Base tr	eatment					Žn NaOH	0.02 0.0
	Stage I tr	eatment 					Zn NaOH	0.003 0.0
Copper								
Cyanide bath	1000 m <sup>2</sup>						011 Cu CN	2 10 20
Acid bath	1000 m <sup>2</sup>						Cu SO4	12 75
Pyrophosphate bath	1000 m <sup>2</sup>						Cu	4.5
	Base tr	eatment					Cu	0.03
	Stage I tr	eatment 					Cu CN	0.004 0.002
Cadmitum								
Cynanide bath	1000 m <sup>2</sup>						Cd CN NaOH	4 10 6
	Base tr	eatment					Cd	0.02
	Stage I tr	eatment					Cd CN	0.002 0.002
Silver	1000 m <sup>2</sup>						Ag CN	7 10
	Stage I tr	eatment					Ag	0.001

Model for Liquid Waste Inventories and Controls - Cont'd

	UNIT WA	WASTE	80D <sub>5</sub>	TSS	Tot N	Tot P	Other Poll	lutant:
_	(U)	WASTE m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/V Pntr		kg/U Pnt
Tin	2		-					
Alkaline bath	1000 m <sup>2</sup>						Sn NaOH	4 4
Bright acid bath	1000 m <sup>2</sup>						Sn	5
Tin fluoroborate bath	1000 m <sup>2</sup>						\$n F/borate	16
	Stage I tr	reatment					Sn NaOH	0.0
Lead fluoroborate bath	1000 m <sup>2</sup>						Oil	1
ecas i lasi obbilate batil	1000 111						Pb	21
							F/borate	48
	Stage I tı	reatment	l 1				Pb	0.0
Gold								
Ornamental	1000 m <sup>2</sup>						Аш	0.3
<b>-</b>	1000 m <sup>2</sup>						CN	0.4 2.5
Technical	1000 m-						Au CN	1.4
	Stage I t	reatment	1				Au	0.
			I				CN	0.0
Brass Cyanide bath	1000 m <sup>2</sup>						Zn	3.2
			-				CN	1.2
	Base t	reatment	I				Zn	0.
							Zn	

Model for Liquid Waste Inventories and Controls - Cont'd

	UNIT V	WASTE	80D <sub>5</sub>	TSS	Tot N	Tot P	Other Pol	lutant
_	(U)	VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pnt
Electroless metal bath								
Nickel baths	1000 m <sup>2</sup>						011	4
							Ní	1.1
							Phosph	4
Copper baths	1000 m <sup>2</sup>						0 i 1	15
соррег васпа	1000 111						Cu	1.6
A	1000 m <sup>2</sup>						A1	7.5
Anodizing sulfuric baths	1000 111						\$04	235
Phosphating baths								
Zinc phosphating	1000 m <sup>2</sup>						ζn	3
							Fe	1.8
							Phosph	12
Iron phosphating	1000 m <sup>2</sup>						0i1	5
Tron phosphae mg	1000 III						Phosph	4
Chromating baths								
For aluminum	1000 m <sup>2</sup>						Çr	0.8
							F	0.4
For zinc (yellow	1000 m <sup>2</sup>						Çr	1.4
passivating bath)							Zn	0.3
For zinc (blue	1000 m <sup>Z</sup>						Cr.	3.3
passivating bath)	1000 111						Zn	16
<b>,</b> ,							F	7.5
JOR DIVISION 4. <u>ÉLECTRICITY GA</u>	S AND WATER							,
O Electricity Gas and Steam								
01 Steam turbines	GWH		2.2	286		0.05	Oil	. 04
							Çr	. 00
							Cu	.00
							Ni	. 04
							Zn	. 01

# Model for Liquid Waste Inventories and Controls - Cont'd

•	UNIT	WASTE VOLUME kg/U	800 <sub>5</sub>	/U kg/U		Tot P	0ther	Pollutants
	(U)		kg/U Pntr			kg/U Pntr	Name	kg/U Pntr
MAJOR DIVISION 6.	OLESALE & RETAIL TRADE &	HOTELS &	RESTAUR	ANTS				
620 Retail Trade								

Shopping centers employee\*yr 21.9 7.3

### 631 Restaurants, Cafes, and Other Eating & Drinking

Restaurants meal\*yr 7.3 3.7

#### 632 Hotels, Rooming Houses, Camps and other Lodging

Motels with restaurant	Bed*yr	70.	21.9
Campgrounds	(Trailer site)*yr	70	21.9
	Trailer*yr	108	58.4
Camps			
No meals served	person*yr	22	7.3
Luxury	person*yr	140	36.
Dwellings (seasonal occ	up) person*yr	70	21.9
Parks	person*vr	7.3	3.7

### MAJOR DIVISION 7. TRANSPORT, STORAGE AND COMMUNICATION

#### 713 Air Transport

Airports Passenger\*yr 7.3

# Model for Liquid Waste Inventories and Controls - Cont'd

		(A) 7 T	MACTE	80D <sub>5</sub>	TS\$	Tot N	Tot P	Other Po	llutants
		UNIT (U)	WASTE VOLUME m <sup>3</sup> /U	kg/U Pntr	kg/U Pntr	kg/U Pntr	kg/U Pntr	Name	kg/U Pnti
IOLAI	R DIVISION 9. COMMUNITY.	SOCIAL AND PERSON	IAL SERVI	CES					
20	Sanitary and Similar Serv	rices							
200	Community, social and per	sonal services							
	Population served by Sewers <sup>40</sup>		r.c	10.1	20.0	2.2	A 02	0:1	7.3
	Septic tanks <sup>41</sup>	person*yr person*yr	55 7.3	18.1 6.9	39.2 16	3.3	0.93	0 i 1	7.3
	Septio tanks	per 3011 yr	7.5	0.5	10				
		Primary sedime	ntation '	0.67	0.4	0.925	0.90		
		Chemical coag		0.25	0.15	0.75	0.15		
	Hi	gh rate trickling	filter	0.25	0.21		•	Bacter	ia 0.1
	t	ow rate trickling	filter	. 075	0.19			Bacter	ia 0.1
	Activat	ed sludge / Conve	ntional	0.1	0.12	0.65	0.62	Bacter	ia 0.2
	Activated sl	udge / Extended a	eration	. 035	0.12	0.77	0.85		ia 0.2
		laste stabilizatio		0.2			0.60		ia<<0.1
	Biological treatmen	t & chemical coag	ulation	0.06	0.13	0.86	0.06		
31	Education Services								
	Schools	,							
	No boarding	student*yr	27	7.3					
	Boarding	student*yr	139	29.2					
40	Recreational and Cultural	l Services							
	Theaters								
	Drive-in	Stall*yr	7.3	3.7					
	Indoor	seat*yr	7.3	3.7					

40. The waste volume and loads exhibit the following typical ranges:

swimmer\*yr

Waste volume: 30. to 110. m3/capita/yr BOD<sub>5</sub>: 16.4 to 19.7 kg/capita/yr TSS: 25.5 to 53. kg/capita/yr 4.4 kg/capita/yr Total N: 2.2 to Total P: 1.64 kg/capita/yr 0.22 to 3.6 to 11. kg/capita/yr

For additional parameters see Table 4.2.2-1

Swimming pools

41. When septage is treated along with domestic wastes, the proportions should be kept low enough so as not to affect the operation of the treatment plant, otherwise pre-aeration may be required to avert anoxic conditions.

14.6

3.7

Pollutant loads from Sewered Urban Areas (Source: S. J. Arceivala, Marcel Dekker, Inc.) Table 4.2.2-1

Pollutant	Effluent Load factor (g/capita/day)
80D <sub>5</sub>	45 - 54
Chemical Oxygen Demand (Dichromate)	1.6 to 1.9 x BOD <sub>5</sub>
Total Organic Carbon	0.6 to 1.0 x BOD <sub>5</sub>
Total Solids	170 - 220
Suspended Solids	70 - 145
Grit (inorganic, 0.2 mm and above)	5 - 15
Grease	10 - 30
Alkalinity, as CaCO3	20 - 30
Chlorides	4 - 8
Nitrogen, total, as N Organic Nitrogen Free Ammonia <sup>a</sup> Nitrite Nitrate	6 - 12 0.4 x total N 0.6 x total N 0.0 to 0.05 x total N
Phosphorus, total, as P Organic Phosphorus Inorganic (ortho and polyphosphates)	0.6 - 4.5 0.3 x total P 0.7 x total P
Potassium, as K2O	2 - 6
Microorganisms Present in Wastewater	(count per 100 ml wastewater
Total bacteria Coliforms Fecal Streptococci Salmonella typhosa Protozoan cysts Helminthic eggs Virus (plaque forming units)	$10^{9}-10^{10}$ $10^{6}-10^{9}$ $10^{5}-10^{6}$ $10^{1}-10^{4}$ up to $10^{3}$ up to $10^{3}$ $10^{2}-10^{4}$

<sup>a</sup>Ammonia in the wastewaters is a by-product of the urea decomposition The wastewater volume, depending on the standard of living and on local conditions, ranges from 50 to 300 lt/d. In some U.S. and other communities it can even exceed 500 lt/d.

Table 4.2.2-2 Typical Performance Efficiencies for Municipal Wastewater Treatment Processes

reatment	BOD Removal, %	TSS Removal, %	Nitrogen Removal, %	Phosphorus Removal, %	Bacteria Removal, %	Viruses Removal log <sub>10</sub> units
rimary Treatment:						
Screening	5-10	2-20			10-20	
Grit Chambers	10-20	20-40			10-20	,
Skimming	20-30	20-40			10-20	
Sedimentation	30-35	60-65	7.5	10	25-75	0-1
econdary Treatment:						
Chemical						
Coagulation	50-85	70-90	25	85	40-80	0-1
High Rate						
Trickling Filter	65 <b>-</b> 95	65-92			80-95	0-1
Low Rate						
Trickling Filter	90-95	70-92			90-95	0-1
Activated Sludge	85-93	85-90	30-40	30-45	60-90	0~1
Extended Aeration	95-98	85-90	15-3 <b>0</b>	10-20	60~90	0-1
Aerated Lagoon	70-90				60-96	1-3
Waste Stabilization	n 70-90		40-50	20-60	60-99.9+	1-4
ertiary Treatment:						
Disinfection					99-99.9+	0-4

Nutrient and Organic loads from rainfall and land Table 4.2.2-3 runoff (Source: S. J. Arceivala, Marcel Dekker, Inc.)

	1//0.)					
Source	Units	Total N as N	Total P as P	800	COD	TSS
Direct rainfall	mg/l	0.5-1.5	0.004-0.03		10-20	10-20
Urban stormwater runoff	(separate	sewers)				
a. Cincinnati <sup>a</sup>	kg/km <sup>2</sup> /yr	875	105	4.725	31,150	64,050
b. Europe	kg/km <sup>2</sup> /yr	952	90			
Forest runoff						
a. Several US studies	kg/km²/yr	143-357	2.6-12.8			
b. Swiss pre-Alps	kg/km <sup>2</sup> /yr	840	4			
<ul><li>c. Diverse forests (Finland)</li></ul>	kg/km <sup>2</sup> /yr		17-27			
Pastures in Swiss pre-A	lps					
Natura l	kg/km <sup>2</sup> /yr	1,650				
Fertilized	kg/km <sup>2</sup> /yr	1,940				
Agricultural Runoff		•				
a. Typical Range	kg/km²/yr		7-105 <b>b</b>			
b. 3 US areas	kg/km²/yr	784	45			
c. Swiss plateau <sup>c</sup>	kg/km <sup>2</sup> /yr	1,400-3,000	21-50			
d. 7.5-acre US field	kg/km <sup>2</sup> /day f rainfall	20	1 - 7			
e. Irrigation return Surface Subsurface	kg/km²/yr	274-2690 4,250-18,600	103-434 280 <b>-</b> 906			

a Average numbers of bacteria per 100 ml: Total coliforms 58,000; Fecal coliforms 10,900; Fecal Streptococci 20,500.

 $<sup>^{\</sup>mathbf{b}}$  0.05-1.0 mg/l as total P, of which 15-50% may be as soluble orthophosphates

G Mixed agricultural use, fertilized

Table 4.2.2-4 Efficiency of Treatment Systems for Agro-Industry Wastes (Adapted from: E.J. Middlebrooks, John Willey & Sons)

Treatment System	Effluent Reduction
Primary Treatment of By-product recovery	· · · · · · · · · · · · · · · · · · ·
Sedimentation or Gravity separation	BOD <sub>5</sub> 20-30% removal TSS 20-50% removal
Dissolved Air Flotation (DAF)	0il       15-20% removal         BOD5       30% removal         TSS       30% removal
DAF with p <sub>H</sub> control & flocculants added	Oil 60% rem'l to 100-200mg/l BOD <sub>5</sub> 90% removal TSS 98% removal Oil 95-99% removal
Secondary Treatment	
Anaerobic & aerobic lagoons Anaerobic & aerated & aerobic lagoons Anaerobic contact process Activated sludge Extended aeration Anaerobic lagoons and biodisks	BOD5       95% removal         BOD5       to 99% removal         BOD5       90-95% removal         BOD5       90-95% removal         BOD5       95% removal         BOD5       90-95% removal         BOD5       90-95% removal
Tertiary Treatment	
Chlorination Sand filter Microstrainer	Disinfection BODs to 5-10 mg/l TSS to 3-8 mg/l BODs to 10-20 mg/l TSS to 10-15 mg/l
Electrodialysis Ion exchange Ammonia stripping Carbon adsorption Chemical precipitation Reverse osmosis	TDS 90% removal Salt 90% removal NH3 90-95% removal BOD <sub>5</sub> to 95% removal P 85-95% rem'l to 0.5 mg/l Salt to 5 mg/l TDS to 20 mg/l
No Discharge	
Spray irrigation Flood irrigation Ponding and evaporation	Total removal Total removal Total remova]

Composition of Leachates from Landfills (Source: G. Table 4.2.2-5 G. Tchobanoglous, Theisen, H., and R. Eliassen, Solid Wastes: Engineering Principles and Management Issues. , McGraw-Hill)

	Range mg/lt	Typical mg/lt
BOD <sub>5</sub>	2,000-30,000	10,000
Chemical Oxygen Demand (COD)	3,000-45,000	18,000
Total Organic Carbon (TOC)	1,500-20,000	6,000
Total Suspended Solids	200-1,000	500
Organic Nitrogen	10-600	200
Ammonia Nitrogen	10-800	200
Nitrate	5-40	25
Total phosphorus	1-70	30
Orthophosphorus	1-50	20
Alkalinity as CaCO <sub>3</sub>	1,000-10,000	3,000
PH	5.3-8.5	6
Total hardness as CaCO <sub>3</sub>	300-10,000	3,500
Calcium	200-3,000	1,000
Magnesium	50-1,500	250
Potassium	200-2,000	300
Sodium	200-2,000	500
Chloride	100-3,000	500
Sulfate	100-1,500	300
Iron (total)	50-600	60

For the computation of the waste loads the annual leachate volume is required. Leachates Note: are produced from the decomposition of the solid wastes, and from water that has entered the landfill either directly from rainfall, or from surface drainage and groundwater. If the latter can be assumed negligible, the leachates volume could be conservatively taken as equal to the rainfall volume. Evaporation however, may be significant, not only from the landfill surface, but also from the landfill mass due to the exothermic reactions taking place there.

# 4.2.3 Working Table for Assessing the Effluent Loads

Data and Calculation Sheet for Liquid Wastes (# \_\_\_\_ of \_\_\_\_)

Ī		nu care					Ψ', L	- qu		43.00	. 3 (	<i>"</i>	01		_ /	
			SOURCE SIZE	VOL	JME	В	<sup>DD</sup> 5	Ţ	ss	Tot	al N	Tota	al P		ÖTHER	
	SOURCE	UNIT (U)		Fact m <sup>3</sup> /U	1000 m <sup>3</sup> /y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Fact kg/U	Load tn/y	Pollu tant	Fact kg/U	Load tn/y
	V															
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# 4.2.4 Example

#### The Problem:

A textile mill operating within our study area is to be surveyed. Determine the data requirements, collect the necessary information and assess the effluent loads:

#### Solution to the Problem:

- 1. From Appendix II we find the manufacture of Textiles classified under the Standard Industrial Classification (SIC) Code # 321. Use of Appendix II facilitates the finding of a particular activity in Section 4.2.2.
- From Section 4.2.2, inspection of the Textile manufacturing liquid wastes model yields the following input data requirements:

(a)	If wool is processed:	
	Quantity of wool scoured,	tn/yr
	Quantity of wool dyed,	tn/yr
	Quantity of wool washed,	tn/yr
	Quantity of wool carbonized,	tn/yr
	Quantity of wool bleached,	tn/yr
(b)	If cotton is processed:	
	Quantity of yarn sized,	tn/yr
	Quantity of cotton desized,	tn/yr
	Quantity of cotton kiered,	tn/yr
	Quantity of cotton bleached,	tn/yr
	Quantity of cotton mercerized,	tn/yr
	Quantity of cotton dyed,	tn/yr
4.3	Quantity of cotton printed,	tn/yr
(c)	If rayon is processed:	
(4)	Quantity of textiles,	tn/yr
(d)	If rayon is processed:	4 /
(0)	Quantity of textiles,	tn/yr
(e)	If rayon is processed:	A /
(f)	Quantity of textiles,	tn/yr
(1)	If rayon is processed:	<b></b> /
(g)	Quantity of textiles, If rayon is processed:	tn/yr
(8)	Quantity of textiles,	tn/yr
	quantity of textiles,	ui/yr

In addition, if a treatment plant exists, information about its type and its operating status must be collected. Typical treatment installations include: plain sedimentation, chemical coagulation/sedimentation, anaerobic lagooning, aerobic lagooning and activated sludge.

- 3. Assume that from the plant survey visit the following data were obtained in relation to the above questionnaire:
  - (a) Only cotton is processed

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Quantity of cotton sized, 840 tn/yr Quantity of cotton desized, 840 tn/yr Quantity of cotton kiered, 840 tn/yr Quantity of cotton bleached, 840 tn/yr Quantity of cotton mercerized, 290 tn/yr Quantity of cotton dyed, 420 tn/yr Quantity of cotton printed, 120 tn/yr
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- (b) The treatment plant comprises only plain sedimentation.
- 4. The above plant survey data, along with the necessary information from the liquid waste load model of Section 4.2.2, can be inserted in the working Table given in Section 4.2.3. The latter can be used for computing the annual effluent loads released from the plant.

Table 4.2.4-1 shows how data and information can be entered and how effluent loads can be computed. It should be noted that in this Working Table:

- (a) Each listed load factor is the product of multiplication of each uncontrolled waste factor and the corresponding penetration factor for the plain sedimentation used. For example, the BOD<sub>5</sub> load factor for untreated cotton sizing is 2.8 kg/tn and the BOD<sub>5</sub> penetration from plain sedimentation is 0.6, Section 4.2.2, SIC 321. Their product, 2.8x0.6=1.7, is the BOD<sub>5</sub> load factor for the treated effluent from cotton sizing.
- (b) The load factors are expressed as kg/Unit, while the activity of each source is entered in 1000 Units/Year. As a result, multiplication of each load factor by the source activity yields the effluent load expressed in tons/year. For example, the BOD5 load factor for cotton sizing is 1.7 kg/tn of cotton and the source activity is 0.84 thousand tons of cotton sized per year. Their multiplication yields 1.4 tons of BOD5 per year.

Table 4.2.4-1 Example use of the working table of Section 4.2.3 Data and Calculation Sheet for Liquid Wastes (#  $_1$  of  $_1$ )

		SOURCE SIZE	VOL	JME	В	DD <sub>5</sub>	T:	55	Tota	al N	Tota	al P		OTHER	
	UNIT		Fact	1000	Fact.	Load	Fact	Load	Fact	Load	Fact	Load:	Pollu	Fact	Load
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312 Textiles Manuf	acturin														
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Textile Mill Surve	yed "	<b>]</b> . ]									ŀ		•		
Sizing	tn	0.84	4.2	3.5	1.7	1.4			į					]	
Desizing	tn	0.84	22	18.5	34.8	29.2	12.0	10.1							
Kiering	tn	0.84	100	1 1			8.8					1			
Bleaching	tn	0.84	13				2.0								
Mercerizing	tn	0.29					1.0		11						
Dyeing	tn	0.42	15				10.0		II .		ļ				ļ
Printing	tn	0.12	14	1.7	32.4	3.9	4.8	0.6						ŀ	
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Fact=Waste	Lead Fa	ctor						}							1

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CHAPTER 5

# SOLID WASTE INVENTORIES

- 5.1 Compilation of Solid Waste Inventories Under Present and/or Strategy Target Conditions
- 5.2 Model for Compiling Solid Waste Inventories
  - 5.2.1 Introduction
  - 5.2.2 Model for Solid and Hazardous Waste Inventories
  - 5.2.3 Working Table for Assessing the Solid Waste Loads
  - 5.2.4 Example
- 5.3 Bibliography

# 5.1 Compilation of Solid Waste Inventories Under Present and/or Strategy Target Conditions

The procedural aspects for the calculation of the solid waste loads released from various sources in the study area are presented in Section 2.3 and demonstrated through an example in Section 5.2.4.

In the air and liquid wastes examined so far, the pollutants types are fairly well defined. This is not the case however, for the solid and hazardous wastes, as they are often complex mixtures of inert, oily, organic and toxic substances. The classification of such wastes in categories has to be based on their nature, using as criteria for this purpose their land or water pollution potential, as well as the applicable treatment technologies.

In this book and in the model in Section 5.2.2 in particular, the solid waste load factors from the various types of sources are organized according to the system proposed by the World Bank/WHO/UNEP in six broad categories and a number of sub-categories thereof. As this classification of solid and hazardous wastes is important, a brief summary of the categories and their sub-categories follows:

### 1. Inorganic Wastes

- A. Acids and Alkalis come mainly from surface preparation and finishing of metals. They are hazardous because of their corrosive action.
- B. Cyanide Wastes come mainly from the metal finishing industry and the heat treatment of certain steels. Their acute toxicity makes them hazardous.
- C. Heavy Metal Sludges and Solutions come from a wide variety of manufacturing processes such as chlor-alkali, metal plating, tanneries, and textile mills. They are a major hazard because of the toxicity of heavy metals such as arsenic, cadmium, hexavalent chromium, lead, mercury, nickel, zinc and copper.
- D. Asbestos Wastes come mainly from demolition or building of power plants, gas works, dock yards, buildings etc, where this material is used. The inhalation of asbestos fibers due to their carcinogenic potential represents a major hazard.
- E. Other Solid Residues come mainly from the smelting and refining of metals. Their dusts and sludges contain toxic metals including nickel, arsenic, zinc, mercury, cadmium and lead.

### 2. Oily Wastes

These are generated primarily from the processing, use and storage of mineral oils. Example are bottom sludges from oil storage tanks and waste cutting oils. They may also contain toxic metals.

# 3. Organic Wastes

- A. Halogenated Solvents are generated primarily from dry cleaning and metal cleaning operations and to a much smaller extent from degreasing and deciling processes in the textile and leather industry. The hazards associated with these wastes are a result of their toxicity and relatively high persistence.
- B. Non-Halogenated Solvent Wastes are generated primarily in the production of paints, inks, adhesives, resins, solvent-based wood preservatives, toiletries, food flavourings cosmetics etc.
- C. PCB Wastes are generated primarily from the manufacture of PCBs and from the decommissioning of equipment, in which PCBs are used. PCBs are used in industry as dielectric fluids (in electric transformers and capacitors), as well as hydraulic and heat transfer fluids. The hazards associated with these wastes are a result of their high persistence and bioaccumulation.
- D. Paint and Resin Wastes are generated primarily from a variety of paint formulation and other tertiary chemical processes, and also from the application of paints and resins to finished products. They are typically combinations of solvents and polymeric materials, including, in some cases, toxic metals.
- E. Biocide Wastes are generated primarily from the manufacture and formulation of biocides and from their use in agriculture.
- F. Organic Chemical Residues include both halogenated and non-halogenated chemicals, but differ from categories (A) to (E) above in that their presence is not in concentrated form. They are generated by a broad range of industries including petroleum refining manufacture of chemicals, dye stuffs, pharmaceuticals, plastics, rubbers and resins. They are also generated from coal carbonization. Distillation residues and filter materials are common components.

# 4. Putrescible Organic Wastes

These include wastes from the production of edible oils, leftovers from slaughterhouses, tanneries, and other animal based products. In this category we have classified the wastes from agricultural activities, sludges from wastewater treatment plants, which do not contain excessive amounts of toxic substances, as well as the normal municipal refuse.

# 5. High Volume/Low Hazard Wastes

These include wastes which, based on their intrinsic properties, present relatively low hazards. Examples include drilling muds from petroleum and gas extraction, fly ash from fossil fuel fired power plants, mine tailings, or metalliferous slags.

# 6. Infectious Wastes

Include infectious wastes associated with diseased animal tissues, and may originate from slaughterhouses, hospitals etc.

# 5.2 Model for Compiling Solid Waste Inventories

### 5.2.1 Introduction

The quantities of solid and hazardous wastes generated from any industrial or other activity depend, in general, on a number of parameters. Thus, the emission E of waste j could be expressed in a mathematical form as follows:

The source type defines the kind of pollution generating activity in somewhat broad terms, e.g. leather tanning or textile finishing. More precise definition is provided through other parameters as discussed below. Obviously, the source type is a parameter which is closely related to the nature and quantity of the wastes generated.

Through the source type parameter alone it is possible to simplify the source inventory and the solid waste management tasks very substantially by excluding, right from the start, numerous activities with relatively minor solid waste generating potential.

The unit of activity, defines the magnitude of a given source. Suitably defined units can be used to provide a measure of the source (e.g. population of an urban area) or the activity of an industry (raw materials consumed, or products manufactured).

Selection of the most suitable unit for each type of activity is important, as the unit must have a direct relation to the effluent loads generated, and must offer convenience in obtaining the required data during the field work. For example, the magnitude of a tannery source could be characterized by the electricity or the water consumed, by the number of people employed, by the land area occupied, or by the quantities of the hides processed. The latter

is much more closely related to the effluent loads generated; it can be easily obtained, both during plant survey visits and from government sources (usually as a compounded total for all tanneries), and is thus the unit of choice.

Source size, although a key parameter, is only indirectly related to the normalized load rates (pollutant loads per unit of activity). In large-size sources, economies of scale allow better design and operation, waste-material recycling and reuse (Overcash, 1986), and improved processing and handling (e.g. sludge digestion in wastewater treatment plants), and these can substantially reduce the waste generating potential. On the other hand large-size sources are more likely to be equipped with efficient air and/or effluent control systems, which generate significant quantities of solid and often hazardous wastes (see below).

In the context of the present methodology the above effects of the source size on the normalized loads is taken into consideration through the listing of alternative air and water treatment and waste processing possibilities.

The type and the quality of the raw materials used are in principle intimately related to the quantities and the nature of the solid and hazardous wastes generated. In the treatment of municipal effluents, the presence of toxic wastes in the generated sludge depends on the quality of the received wastewater. In industrial processes the type and the quality of raw materials available often dictate the process to be used. The above are covered by the solid waste loads model of Section 5.2.2.

The use of Air Pollution Control systems inevitably results in the production of solid and hazardous wastes as they capture the pollutants that would have been emitted and convert them into a solid wastes form.

The air pollutant control systems can be distinguished into three basic categories depending on their solid wastes generating potential: thermal or catalytic incinerators, which convert pollutants into less harmful emissions, and the adsorption or refrigeration systems, which capture pollutants in the form of useful liquid products, present the smallest solid wastes pollution potential; dust control systems, such as cyclones, fabric filters and electrostatic precipitators, which operate without the use of water, capture the suspended particulates and yield significant quantities of solid wastes, often of a toxic nature; finally, wet scrubbers remove dust and gaseous pollutants yielding sludges, which, due to their large volume and their hazardous nature present the most difficult disposal problems.

The impact of the above parameters is included in the model in Section 5.2.2, as data are provided, which allow the assessment of the waste quantities generated, both in dry and in wet states, by the air pollution control installations of selected sources.

The use of Wastewater Systems inevitably results in the generation of sludges often of a hazardous nature, as most of the suspended solids settle and the organic materials are digested by bacteria and converted into settled biomass. In this process most of the heavy metals in the wastewater, also find their way into the sludge.

The impact of this parameter is included in the model in Section 5.2.2 as data are provided, which allow the assessment of the waste quantities generated, both in dry and in wet states, by the wastewater treatment installations of selected sources.

The above discussion leads into the practical question of how the waste load  $E_j$  could be expressed as a direct and explicit function of all the parameters that may affect it for all waste types j of interest.

The first step in this direction is to define the waste load factor  $\mathbf{e}_j$  for the waste type j, through the following relation:

$$e_j = \frac{E_j, kg/yr}{Source activity, Units/yr}$$
 (5.2.1-2)

The waste load factor  $\mathbf{e}_j$  is normally expressed as kg/Unit and is assumed to be independent of the source size and the source activity (or production) level. The basis for this important assumption is the way the activity units are selected. Indeed, as discussed above, a key criterion in the selection of the activity units is their direct and proportional relation to the waste loads generated. From the above and from Equation (5.2.1-1) we obtain:

The emission factor  $\mathbf{e_j}$  is used extensively hereafter, as the key objective of our solid wastes load emissions model is to define the value of  $\mathbf{e_j}$  for every type of waste j.

The dependence of the waste load factors  $e_j$  on the parameters discussed above and listed in Equation (5.2.1-1), cannot, in most cases, be expressed in a continuous function form due to the discreet nature of most parameters (e.g. the type of treatment plant used), and to frequent lack of sufficient information in relation to the remaining parameters. A discreet functional form yielding a series of waste load factors, each

valid under a specific set of common and important parameter combinations, is used instead.

The discreet rather than the continuous nature of the emission factor values explains the tabular construct of the Model in Section 5.2.2. into which the source types are organized on the basis of the UN Standard Classification of Industries and Services. Under each activity listed, typical alternative processes are included (e.g. under Tanneries and Leather Finishing (SIC 3231), the Chrome Tanning, Vegetable Tanning, Tanning only, Finishing only, Re-tanning and Finishing), and for each such process the major air pollution and/or effluent control alternatives are listed (e.g. effluent pretreatment or full effluent treatment).

The tabular structure and the form of Section 5.2.2 constitutes a solid wastes inventory model, which introduces the impact of all major parameters into the assessment of the generated waste loads, and provides a precise definition of the data requirements from field surveys. The model in Section 5.2.2 constitutes thus a valuable tool for source inventory studies, not only for computing the waste loads and for providing guidance on the data to be collected during the field survey work, but also for organizing and presenting such data in a concise manner (see also Sections 5.2.3 and 5.2.4 below).

The nature of the solid wastes produced is a key parameter from both, the management and treatment points of view, and the land or water pollution potential. This important issue is addressed by the model of Section 5.2.2 in three ways:

1. The wastes are classified according to the system proposed by the World Bank/WHO/UNEP in six broad categories and a number of sub-categories thereof as follows:

### Inorganic wastes

- A. Acid and alkalis
- В. Cyanide wastes
- Heavy metal sludges and solutions
- Asbestos residues
- Other solid residues

#### Oily wastes

# Organic wastes

- Spent halogenated solvents
- B. Non-Halogenated solvent wastes
- C. PCB wastes
- D. Paint and resin wastes
- E. Biocide wastes
- F. Organic chemical residues

Putrescible organic wastes

High volume/low hazard wastes

#### Infectious wastes

In Section 5.1 the nature of the wastes in each of the above categories and sub-categories is described, while the major industrial and other activities that generate them are listed.

- 2. Footnotes provide a short description of the nature and/or additional information about the composition of many types of waste.
- 3. For municipal solid wastes (belonging in the general category of Putrescible Organic Wastes) typical composition, density, and calorific value data for various countries provided in Table 5.2.2-1. Moreover, Table 5.2.2-2 provides typical property values for individual municipal waste components enabling users to assess the typical moisture content, density, low calorific value and residue on the basis of available waste composition data. Table 5.2.2-3 provides data about the compaction ratio of the various types of solid wastes for alternative compaction degrees enabling users to compute the landfill volume requirements, Section 10.3.2.5.

Any classification scheme, including the one adopted here, aims to classify the wastes produced in broad categories. Such groupings however do not convey sufficient information for management purposes and, as a result, the need arises to consider the hazardous and toxic wastes generated by each type of source separately. In highly industrialized economies this would require a lengthy list of sources. For most developing countries however, the structure and complexity of their chemical and processing industries is considerably simpler, and as a result, the number of source types which are important, is not prohibitively long for rapid assessment procedures. The model in Section 5.2.2 includes many of the types of sources likely to be encountered in developing countries, and especially those which require priority action.

# 5.2.2 Model for Solid and Hazardous Waste Inventories $^{f 1}$

		rganic	Oily	Org	janic	Putres- cible		Infec- tious
UNIT	*	Kg/U	 Kg <b>∮</b> U	*	Kg/U	Kg/U	 Кg/U	 Kg/ህ

### MAJOR DIVISION 1. AGRICULTURE, HUNTING, FORESTRY AND FISHING

#### 111 Agricultural and Livestock Production

Agricultural		
Cotton	tn of product	2500
Rice	tn of product	800
Oats	tn of product	1400
Sugar (Cane)	tn of product	300
Sugar (Beet)	tn of product	100
Coffee	tn of product	3500
Barley	tn of product	1800
Rye	tn of product	1600
Maize	tn of product	1500
Sorghum	tn of product	700
Soya	tn of product	1600
Wheat	tn of product	1100
Other cereals	tn of product	700
Farm Animals and Poul	try <sup>2</sup>	
Bovine Cattle	animal*year	4000
Sheep	animal*year	1100
Pigs	animal*year	700
Chicken	bird*year	20
Turkeys	bird*year	200
Horses	animal*year	4000

#### MAJOR DIVISION 2. COAL MINING AND QUARRYING

### DIVISION 21. COAL MINING

Coal Mining		
Surface Working <sup>3</sup>	tn of product	12100
Underground Working <sup>4</sup>	tn of product	37

<sup>1.</sup> For a description of the waste categories and sub-categories (the latter denoted in the model by the capital letters A to F) see Sections 5.1 and 5.2.1

<sup>2.</sup> The wastes produced by animal farms are mostly manure, but in the case of chicken and turkeys they contain the litter, which is periodically added

<sup>3.</sup> Overburden

Model for Solid & Hazardous Waste Inventories - Cont'd

			I	norganic	0 f 1y	٥r	ganic	Putres- cible	Low Hazard	Infec- tious
		. TINU	*	Kg/U	 Kg/∪	* Kg/U		 Кg/U	Kg/U	Kg/U
SIVIC	ION 23. METAL ORE MINING					-				
2301	Iron Ore Mining									
	Surface Working	tn of prod	uct						100	
	Underground Working	tn of prod	uct						2100	
302	Non-Ferrous Ore Mining									
	Copper Ore									
	Surface Working	tn of prod	uct						2250	
	Underground Working Bauxite Ore	tn of prod	uct						75	
	Surface Working Lead Ore	tn of prod	uct						6000	
	Underground Working Zinc Ore	tm of prod	uct						250	
	Underground Working Tungsten Ore	tn of prod	uct						200	
	Underground Working Silver Ore	tn of prod	uct						300	
	Surface Working	tn of prod	uct						8350	
	Underground Working	tn of prod	uct						350	
	Uranium Ore									
	Surface Working	tn of prod	uct						19500	
	Underground Working Gold Vein	tn of prod	uct						400	
	Surface Working	tn of prod							2400	
	Underground Working Gold Alluvial	tn of prod							200	
	Surface Working Other	tn of prod							730	
	Surface Working	tn of prod	ıct						3450	
	Underground Working	tn of prod	ıct						25	
IVIS	ION 29. OTHER MINING									
901	Stone Quarrying, Clay and	Sand Pits								
	Crushed and Broken Stone Surface Working	tn of produ							80	

Low grade coal and parent rock

37

# Model for Solid & Hazardous Waste Inventories - Cont'd

		UNIT -		In	organic	ganic Oily		ganic	Putres- cible	Low Hazard 	Infec- tious 
				*	Kg/U	Kg/U	* Kg/U		Kg/U		
	Clay			- '							
		tn of	product							900	
	Underground Working	tn of	product							20	
	Talc, Soapstone, Pyrophyllit	e				•					
	Surface Working	tn of	product							1650	
	Underground Working	tn of	product							40	
2902	Chemical and Fertilizer Mine	eral Mi	ining								
	Phosphate Rock										
	Surface Working	tn of	product							2050	
	Underground Working	tn of	product							10	
	Potassium Salts										
	Underground Working	tn of	product						T.	30	
	Gypsum / Surface Working	tn of	product							500	
	Fluorspar/Underground Workin	ng tn	product							200	
	Barytes										
	Surface Working	tn of	product							650	
	Underground Working	tn of	product							200	
2909	Mining and Quarrying Not El	sewher	e Classi	fied	i						
	Abrasives / Surface Working	tn of	product							450	
	Asbestos / Surface Working		product							3200	
	Mica / Surface Working	tn of	product	:						500	
	Diatomite / Surface Working	tn of	product	:						1450	
			product							1010	
	Perlite / Surface Working		product							600	
	Pumice / Surface Working		product							100	•

### MAJOR DIVISION 3. MANUFACTURING

# DIVISION 31. MANUFACTURE OF FOOD BEVERAGES AND TOBACCO

#### 311/2 Food Manufacturing

Slaughterhouse	tn LWK <sup>5</sup>	35 <sup>6</sup>
<u>-</u>	tn LWK	

<sup>5.</sup> LWK is the Live Weight of animals Killed

<sup>6.</sup> Blood, paunch, hooves, etc

Infected animals and organs

Model for Solid & Hazardous Waste Inventories - Cont'd

		UNIT	In	organic	Oily	0r	ganic	Putres- cible	Low Hazard	Infec-
			*	Kg/U	Kg/U	*	Kg/U	—— Kg/Ų	Kg/U	Kg/i
	Poultry Processing8	1000 8irds				-		35		
	Packing House <sup>9</sup>	tn of product						300		
3113	Canning of Fruits and Veg	etables10								
	Apples	tn of product						280		
	Beets, carrots	tn of product						210		
	Citrus	tn of product						390		
	Corn	tn of product						660		
	Olives	tn of product						140		
	Peaches	tm of product						270		
	Pears	tn of product						290		
	Peas	tn of product						120		
	Potatoes	tn of product						330		
	Tomatoes	tn of product						80		
	Vegetables, misc.	tn of product						220		
3114	Canning of Fish <sup>11</sup>									
	Fish	tn of product						280		
	Crab, Shrimp	tn of product						570		
3115	Vegetable Oil Refining12	tn of product						4.7		
3118	Sugar Refineries <sup>13</sup>	tn of product						N/A		
3121	Starch and Glucose <sup>14</sup>	tn of product						N/A		
313	Beverage Industries									
3131	Alcohol Distilleries <sup>15</sup>	tn of product						300		
3133	Beer Brewing 16	tn of cereal						100		
		m3 of beer						20		

Feathers, hooves, inedibles

<sup>9.</sup> Bones, inedible meat, etc

Peels, cores, seeds, etc

Inedible fish parts

<sup>12.</sup> Purification mud soaked in oil

<sup>13.</sup> Spent beats and cames

Corn residues

<sup>15.</sup> Spent resins, figs, canes, etc

<sup>16.</sup> Spent hop, grain, residues, yeast

# $\label{thm:model} \textbf{Model for Solid \& Hazardous Waste Inventories - Cont'd}$

		11077	In	organic	Oily	Organic		Putres- cible		Infec- tious
		UNIT	*	Kg/U	Kg/U	*	Kg/U	Kg/U	 Kg/U	Kg/l
IVIS	ION 32. TEXTILE, WEARING A	APPAREL AND LEATH	ER	INDUSTRI	ES			•••••		
21	Manufacture of Textiles						•			
211	Wool Processing			٠						
	Scouring									
	Process17	tn of product						10	95	
	Effluent Treatment	tn of product						57018		
		(tn of product)						(5700)		
	Dyeing and Finishing									
	Process <sup>19</sup>	tn of product				D	38		20	
	Effluent Pretreatme	•							<sub>25</sub> 20	
		(tn of product)							(100)	
	Treatment	tn of product	С	N/A						
3211	Cotton Processing									
	Yarn Preparation <sup>21</sup>	tn of product							32	
	Weaving <sup>22</sup>	tn of product							11	
	Dyeing and Finishing									
	Process <sup>23</sup>	tn of product							7	
	Effluent Pretreatme	ent tn of product						0.8 <sup>24</sup>		
		(tn of product)						(2.8)		
	Effluent Treatment	tn of product						20 <b>25</b>		
		(tn of product)						(2300)		
3214	Carpet and Rug Manufactur	ė								
	Process	tn of product							31	
	Pretreatment	tn of product				D	1.226	i		
		(tn of product)				D	. (2)			
	Treatment	tn of product		2.327						
		(tn of product)	C	(4.9)						

<sup>17.</sup> Dirt, wool, fly and sweeps

<sup>18.</sup> Treatment sludge

<sup>19.</sup> Flock, dye, chemical containers, etc

<sup>20.</sup> Screening fibers

<sup>21.</sup> Fiber and yarn

<sup>22.</sup> Fiber, yarn and cloth

<sup>23.</sup> Cloth and flock

<sup>24.</sup> Screening fibers

<sup>25.</sup> Treatment sludge

<sup>26.</sup> Pretreatment sludge

<sup>27.</sup> Treatment sludge. Possible presence of heavy metals

-		UNIT	Īr	norganic	Oily	0r	ganic	Putres- cible	Low Hazard	Infec- tious
		ONII	*	Kg/U	Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/l
323	Tanneries and Leatl	her Finishing	-			•				
3231	Leather Tanneries <sup>20</sup>	8,29								
	Complete Chromic	um Tanning (Cow Hides)								
	Process	1000 equiv hides	¢	910				450		
		(1000 equiv hides)	C	(1770)				(550)		
	Effluent Pre	treat't1000 equiv hides	Ċ	90						
		(1000 equiv hides)	¢	(390)						
	Effluent Tre	atment 1000 equiv hides	C	300						
		(1000 equiv hides)	Ċ	(2700)						
	Complete Vegetab	ole Tanning (Cow Hides)								
	Process	1000 equiv hides	C	1200				1000		
		(1000 equiv hides)	¢	(1400)				(3350)		
	Effluent Pre	atreat't1000 equiv hides	Ç	140	•					
		(1000 equiv hides)	C	(700)						
	Effluent Tre	atment 1000 equiv hides	C	350						
		(1000 equiv hides)	¢	(7000)						
	Complete Vegetab	ole Tanning (Sheep Skins	)							
	Process	1000 equiv hides	Ċ	540				300		
		(1000 equiv hides)	¢	(1430)				(440)		
	Effluent Pre	atreat't1000 equiv hides	C	50						
		(1000 equiv hides)	C	(230)						
	Tanning Sections	of Hides		:						
	Process	1000 equiv hides	C	4000				90		
		(1000 equiv hides)	С	(8500)				(150)		
	Effluent Pre	atreat't1000 equiv hides	C	5						
		(1000 equiv hides)	Ċ	(22)						
	Leather Finishir	ng Only								
	Process	1000 equiv hides	C	75				55		
		(1000 equiv hides)	C	(84)				(161)		
	Re-tanning and F	inishing								
	Process	1000 equiv hides	£	230				910		
		(1000 equiv hides)	Ċ	(250)				(1770)		
	Effluent Pre	atreat't1000 equiv hides		10						
		(1000 equiv hides)	Ċ	(40)						

<sup>28.</sup> Typical weight of a big hide (from cattle or horse) is 25 to 26 kg, while that of a small hide (from sheep or goat) is 3 kg.

<sup>29.</sup> The major wastes in this category are toxic ones, containing Cr. Pb, and Zn, as well as putrescible scrap products.

	Inorganic	Oily	Organic	Putres- cible		Infectious
UNIT	* Kg/U	Kg/U	* Kg/l	Kg/U	 Kg/U	Kg/U

DIVISION 34. MANUFACTURE OF PAPER AND PAPER PRODUCTS

3411 Manufacture of Pulp, Paper and Paperboard
Pulp Mills tn of product

<sub>50</sub>30

# DIVISION 35. MANUFACTURE OF CHEMICALS & OF CHEMICAL, COAL, RUBBER & PLASTIC PRODUCTS

### 351 Manufacture of Industrial Chemicals

## 3511 Manufacture of Basic Industrial Chemicals except Fertilizers

Chlor-Alkali Plants  $\begin{tabular}{lll} Mercury-cathode cell process the of Cl$_2$ C $40^{31}$ \\ Sulfuric Acid $tn$ \\ \end{tabular}$ 

N/A<sup>32</sup>

Phosphoric Acid (Wet Process) to

4750<sup>33</sup>

Ammonia
3511 Ethylene Dichloride

Chlorobenzene Process

A 6.4<sup>35</sup>

3511 Phenols

A 12.6<sup>36</sup>

N/A34

3512 Pesticides

tn active ingredient tn active ingredient

tn

tn

E 200<sup>37</sup> E N/A<sup>38</sup>

<sup>30.</sup> Cellulose, lignins, reducing sugars

<sup>31.</sup> Graphite, purification muds, CaCO3, Mg(OH)2, Hg / Dry basis

<sup>32.</sup> Spent converter catalyst (V205)

<sup>33.</sup> Gypsum / Dry basis

<sup>34.</sup> Oily condensates from feedstock

<sup>35.</sup> Organic Chlorinated Compounds

<sup>36.</sup> Organic Chlorinated Compounds

<sup>37.</sup> Containers, bags, 1.5% active ingredients

<sup>38.</sup> Broken emulsion products

		unit —	I n	organic	Oily	Organic		Putres- cible	Low Hazard	Infec- tious
		0411	*	Kg/U	Kg/Ų	*	Kg/U	Kg/U	Kg/U	Kg/U
352	Manufacture of Other Chem	ical Products	-			-				
3521	Paints, Varnishes and Lac	quers								
	Solvent Paints	tn of paint				D	8.339			
	Latex Paints	tn of paint				D	5.840			
3522	Manufacture of Drugs and	Medicines								
	Preparation of Active Ing	redients								
	Synthetic Organic							•	1	
	Medicals <sup>41</sup>	tn of product	С	86 <b>42</b>		Α	100			
		tn of product				В	700			
		tn of product				F	450 <b>43</b>			
	Fermentation products	(Antibiotics)								
	Process	tn of product				В	120044			
		tn of product						2300 <b>45</b>		
		(tn of product)						(10000)		
	Effluent Treatment	tn of product						3500 <b>46</b>		
		(tn of product)						(35000)		
	Botanicals <sup>47</sup>	tn of product				A	30			
		tn of product				В	60			
		tn of product		•				330000		
	Pharmaceutical									
	Preparations 48	tn of product							N/A <sup>49</sup>	

<sup>39.</sup> Paint sludge, solvents, heavy metals 4.5%

<sup>40.</sup> Paint sludge, solvents, Hg 125 g/l

<sup>41.</sup> Aspirin, tranquillizers and vitamins are some of the products in this category. The listed factors are typical for the average mixture of chemicals. Aspirin may generate less waste, while some tranquillizers and vitamins more than that derived from the listed factors.

<sup>42.</sup> Zinc 70 kg/tn, As 15 kg/tn, Cr 0.7 kg/tn, Cu 0.1 kg/tn, Hg 0.02 kg/tn

<sup>43.</sup> Approximately 400 kg/tn are tars, muds, and still bottoms, while 50 kg/tn are contaminated, high inert content wastes (filters and activated carbon)

<sup>44.</sup> Solvent waste concentrate (Butyl acetate, dissolved fats/proteins)

<sup>45.</sup> Mycelium (medium on which living organisms are developed) wastes

<sup>46.</sup> Biological sludge

<sup>47.</sup> Quinine, reserpine, steroids, and laxatives are some of the products in this category

<sup>48.</sup> Tablets, Capsules, Liquid preparations

<sup>49.</sup> Mainly broken glass

-			Inorga	ic	Oily	0rį	ganic	Putres- cible	Low Hazard	Infec- tious
		UNIT	* Kg/	 U	Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/U
353	Petroleum Refining					<del>"</del> -				
3530	Petroleum Refineries <sup>50</sup>									
	Topping Ref'ry	1000 m <sup>3</sup> feedstock			1311					
	Low-Cracking Refiry	1000 m <sup>3</sup> feedstock			1675					
	High-Cracking Ref'ry				3303					
	Lubrication Ref'ry	1000 m <sup>3</sup> feedstock			6140					
					E1	_	EA			
3530	Spent Lub Oil Regenerat	ion m <sup>3</sup>			20951	F	<sub>77</sub> 52			
3530 354	Spent Lub Oil Regenerat		and Coke	<b>:</b>	509-21	F	7732			
354	Manufacture of Misc Pro	ducts of Petroleum	and Coke	<b>:</b>	509-31	F				
			and Coke	<b>:</b>	20931	F F	77 <b>52</b> 5.5 <b>53</b> 8.25			
354	Manufacture of Misc Pro	<b>ducts of Petroleum</b> tn of coke 1000 m <sup>3</sup> of gas	and Coke		209-1	F	<sub>5,5</sub> 53			
354 3540	Manufacture of Misc Prod Coke Ovens	ducts of Petroleum tn of coke 1000 m <sup>3</sup> of gas roducts	and Coke		209-1	F	<sub>5,5</sub> 53			
354 3540 355	Manufacture of Misc Produce Ovens  Manufacture of Rubber Produce Ovens	ducts of Petroleum tn of coke 1000 m <sup>3</sup> of gas roducts	and Coke		209-1	F	<sub>5,5</sub> 53		55	

### DIVISION 37. BASIC METAL INDUSTRIES

### 371 Iron and Steel Basic Industries

Iron Foundries Malleable Iron

tn of castings E 142<sup>55</sup> Process

E 600<sup>56</sup>

The major wastes problem constitute the oily sludges, which are often contaminated with heavy 50.

Approximately 150 kg/tn are oily resins with sulfuric acid and 59 kg/tn oily sludges 51.

<sup>52.</sup> Purification muds soaked with oil

Condensates and sludges with Cr 10  $g/m^3$ , Cu 4  $gr/m^3$ , Mn 102  $g/m^3$ , Ni 5.5  $g/m^3$ , Pb 30.5  $g/m^3$ , 53. Zn 96.5  $g/m^3$ , and 0il 20.3 %

<sup>54.</sup> The wastes from this category comprise rubber, fillers, etc

Slag, dust, refractories, along with some heavy metals **5**5.

Casting sand with heavy metals and phenols 56.

Model for Solid & Hazardous Waste Inventories - Cont'd

	UNIT	Inorganic	Oily	Qτţ	ganic	Putres- cible	Low Hazard	Infec- tious
	OMI	* Kg/U	Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/l
Scrubber	tn of castings	E 32.8 <sup>57</sup>						
Wrought Iron	· ·							
Process	tn of castings	€ 134 <sup>58</sup>						
	tn of castings							
Scrubber	tn of castings							
Iron and Steel Mills								
Blast Furnace								
Process	tn of pig iron						348 <b>61</b>	
Cyclones	tn of pig iron	E 16.2 <sup>62</sup>						
Wet Scrubber	tn of pig iron	E 24.463						
80F Steel Furnace								
Process	tm of steel						145 <b>64</b>	
Cyclones	tn of steel	E 16 <sup>65</sup>						
Wet Scrubber	tn of stee!	E 17.3 <sup>66</sup>						
Electric Arc Steel Fu	nace							
Process	tn of steel						120 <b>67</b>	
Cyclones	tn of steel	E 12.8 <sup>68</sup>						
Wet Scrubber	tn of Steel	E 8.7 <sup>69</sup>						
Open Hearth Furnace								
Process	tn of steel						<sub>243</sub> 70	
Cyclones	tn of steel	E 13.7 <sup>71</sup>						
Continuous Casting	tn of steel	E 0.172					8.773	
Hot Rolling	tn of steel	E 1.74 <sup>74</sup>					18.375	
Cold Rolling	tn of steel	E 0.16 <sup>76</sup>					0.052 <b>77</b>	

<sup>57.</sup> Sludge with Heavy metals

<sup>58.</sup> Slag, dust, refractories with Heavy metals

<sup>59.</sup> Casting sand with Heavy metals and phenols

Sludge with heavy metals 60.

<sup>61.</sup> Slag with Cr. Cu, Mn, Ni, Pb, and Zn present

<sup>62.</sup> Dust with Cr. Cu, Mn, Ni, Pb, and Zn present

<sup>63.</sup> Sludge with Cr. Cu. Mn. Ni. Pb. and In present

<sup>64.</sup> Slag with Cr, Cu, Mn, Ni, Pb, and Zn present

Dust with Cr, Cu, Mn, Ni, Pb, and Zn present 65.

<sup>66.</sup> Sludge with Cr. Cu. Mn, Ni. Pb. and Zn present

<sup>67.</sup> Slug with Cr. Cu. Mn. Ni. Pb. and Zn present

<sup>68.</sup> Dust with Cr. Cu. Mn. Ni. Pb. and Zn present

<sup>69.</sup> Sludge with Cr. Cu, Mn, Ni, Pb, and Zn present

<sup>70.</sup> Slag with Cr. Cu. Mn. Ni. Pb. and Zn present

<sup>71.</sup> Dust with Cr, Cu, Mn, Ni, Pb, and Zn present

Sludge with heavy metals 72.

<sup>73.</sup> Rust Scale

<sup>74.</sup> Sludge with heavy metals

<sup>75,</sup> Rust Scale

<sup>76.</sup> Sludge with heavy metals

		Inorganic	0ily	0r	ganic	Putres- cible	Low Hazard	Infec- tious
	UNIT	* Kg/U	Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/⊍
Pickling	tn of steel	A 22.8 <sup>78</sup>						
Tinning	tn of steel	70						
Ga lvan iz ing	tn of steel	E 10.8 <mark>80</mark>						
Pickling	tn of steel							
Ferro-Alloy Production								
Ferromanganese								
Process	tn of castings						24082	
Wet Scrubber	tn of castings	E 165 <b>83</b>						
Silicomanganese	_							
Process	tn of castings						1100 <sup>84</sup>	
Wet Scrubber	tn of castings	E 98 <b>85</b>						
Ferrosilicon	tn of castings	E 338 <mark>86</mark>						
Ferrochromium	tn of castings						1901 <sup>87</sup>	
Ferronickel	-							
Process	tn of castings						31084 <b>88</b>	
Wet Scrubber	tn of castings	E 576 <b>89</b>						
Steel Foundries								
Process	tn of castings						360 <b>90</b>	
	tn of castings						780 <sup>91</sup>	
Wet Scrubber	tn of castings	E 36.4 <sup>92</sup>						

- 77 Rust Scale
- 78. Pickling Fluid with heavy metals
- 79. Sludge with heavy metals
- 80. Sludge with heavy metals
- 81. Pickling Fluid with heavy metals
- 82. Slag with heavy metals
- 83. Sludge with Heavy metals
- 84. Slag with heavy metals
- 85. Sludge with heavy metals
- 86. Dust with Heavy metals
- 87. Slag and dust with heavy metals
- 88. Slag and dust with heavy metals
- 89. Sludge with heavy metals
- 90. Slag, dust, and refractories with heavy metals
- 91. Casting sand with heavy metals and phenols
- 92. Sludge with heavy metals

				In	organic	0 i 1y	Or	ganic	Putres- cible	Low Hazard	Infec- tious
	, 	UNIT		*	Kġ/U	Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/U
372	Non-Ferrous Metal Basic Industri	<u>es</u>									
	Copper										
	Primary Copper Smelting		tn							3000 <b>93</b>	
			tn	Ε	17 <b>94</b>						
			tn	Ē	155 <b>95</b>						
	Copper Electrolytic Refining		tn	Ε	2.4 <sup>96</sup>						
	Secondary Copper Smelting		tn							350 <sup>97</sup>	
	Aluminum										
	Alumina from Bauxite tn of	f Alumi	na							2000 <b>98</b>	
	Primary Aluminum Smelting										
	Cast House & Roding Room	tn of	A٦	Ε	7.5 <sup>99</sup>						
	Electrolytic Cells										
	Process				8.5 <sup>100</sup>						
	Scrubbers	tn of	Αì	É	117101						
	Secondary Aluminum Smelting										
	Scrap Smelting										
	Wet Scrubber		tn	E	<sub>75</sub> 102						
	Dross Smelting		tn	E1	<sub>400</sub> 103						
	Primary Lead Smelting and Refinir	ng									
	Process		tn							410104	
	Wet Scrubber		tn	Ē	89105						
	Secondary Lead Smelting and Refir										
	Soft Lead / Blast Furnace		tn	E	<sub>472</sub> 106						
	Hard Lead /Cupola Furnace		ţn							225107	

<sup>93.</sup> Slag with Cd, Cr, Cu, Hg, Mn, Ni, Pb, Sb, Se, and Zn

<sup>94.</sup> Dust with Cd. Cr. Cu, Hg, Mn, Ni, Pb, Sb, Se, and Zn

<sup>95.</sup> Sludge with Cd, Cr, Cu, Hg, Mn, Ni, Pb, Sb, Se, and Zn

<sup>96.</sup> Sludge with Cd. Cr. Cu, Hg, Mn, Ní, Pb, Sb, Se, and Zn

<sup>97.</sup> Slag with Cd, Cr, Cu, Hg, Mn, Ni, Pb, Sb, Se, and Zn

<sup>98.</sup> Red Muds / Dry basis

<sup>99.</sup> Dust with F, Cu and Pb

<sup>100.</sup> Spent potliners & skim (F and CN)

<sup>101.</sup> Potline scrubber sludge (14% F2)

<sup>102.</sup> Scrubber sludge with Cr. Cu. Pb. and In present

<sup>103.</sup> High salt slag with Cr. Cu. Mn. Ni, Pb. and Zn

<sup>104.</sup> Slag with Cd, Cr, Cu, Mn, Pb, Sb, and Zn

<sup>105.</sup> Sludge with Cd, Cr, Cu, Mn, Pb, Sb, Zn, and Hg

<sup>106.</sup> Slag and scrubber sludge with Cd, Cr. Cu. Mn, Ni, Pb, Sb, Sn, and Zn

<sup>107.</sup> Slag with Cu. Mn. Ni. Pb. Sb. Sn. and Zn

		Inorganic	Oily	Ori	ganic	Putres- cible	Low Hazard	Infec- tious
UNIT		* Kg/V	−−− Kg/U	*	Kg/V	—— Kg/Ų	Kg/U	Kg/l
White Metal / Reverberatory	tn						166108	
Primary Zinc Smelting								
Electrolytic Refining	tn	E26.1 <sup>109</sup>						
Pyrometallurgical Sme?ting/Ref'g	tn	E1050110						
Primary Tin Smelting and Refining	tn						915111	
Primary Antimony SmeIting and Refining							***	
	tn	114					2800113	
Electrolytic Process	tn	E 210 <sup>114</sup>						
Primary Mercury Smelting and Refining	tn	E207000115	5					
Primary Titanium Refining	tn	ε 330 <sup>116</sup>						

3819 Manufacture of Fabricated Metal Products Except Machinery & Equipment not Elsewhere Classified

Electroplating of Copper
Effluent Treatment th of Cu anodes E 9117

Electroplating of Ni
Effluent Treatment th of Ni anodes E 4.118

Electroplating of Chromium
Effluent Treatment th of Cr<sub>2</sub>0<sub>3</sub> E 250<sup>119</sup>

Electroplating of Zn
Effluent Treatment th of Zn anodes E 220<sup>120</sup>

<sup>108.</sup> Slag with Cd, Cr, Cu, Mn, Ni, Pb, Sb, Sn, and Zn

<sup>109.</sup> Sludges with Cd. Cr. Cu. Hg, Mn, Pb, Se, and Zn

<sup>110.</sup> Retort residue with Cd, Cr, Cu, Pb, Se, and Zn

<sup>111.</sup> Slag with Sn and Pb, and possibly with Sb, As, and Zn

<sup>112.</sup> Pyrometallurgical Process

<sup>113.</sup> Slag with Pb, Cu, Zn, and Sb

<sup>114.</sup> Spent anolyte (As 16 g/m³, Pb 5 g/m³, Cu 50 g/m³, Zn 2 g/m³, Ni 5 g/m³, Sb 27 kg/m³, Cr 32 g/m³, Cd 1 g/m³)

<sup>115.</sup> Calcine residue with As, Pb. Cu, Zn, Ni, Hg, Mn, Sb, Cd, and Cr

<sup>116.</sup> Chlorinator and Condenser Sludges with V. Cr. Zr. Ti. and Cl

<sup>117.</sup> Cu in sludge (Cyanide may be also present) / Dry basis

<sup>118.</sup> Ni in sludge / Dry basis

<sup>119.</sup> Cr in sludge / Dry basis

•			In	organic	0íly	0rg	ganic	Putres- cible	Low Hazard	Infec-
		UNIT	*	Kg/U	Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/l
384	Manufacture of Transport Equi	pment	-							
3841	Ship Building and Repairing				101					
	Dry Docks				N/A <sup>121</sup>					
MAJOR	DIVISION 4. ELECTRICITY GAS	AND_WATER								
1101	Electricity Generation 122									
	Lignite Power Plants									
	Emission Controls Bituminous Coal Power Plan	MWH							10.0*A	
	Emission Controls	MWH							4.3*A	
	Transformers	MWH				Α !	<sub>I/A</sub> 123			
MAJOR	DIVISION 9. COMMUNITY, SOCIA	L AND PERSONA	L S	ERVICES						
920	Sanitary and Similar Services									
	Municipal Refuse Collection 12									
	Very Low Income Areas 125	person*year						150		
	Developing Areas <sup>126</sup> Industrialized Areas <sup>127</sup>	person*year person*year						250 400		
	THOUSER IN ITZEO AREAS	person year						400		

- 120. In in sludge (cyanides may be also present) / Dry basis
- 121. Oily and toxic sludges from ship cleaning

Wastewater Treatment Plants<sup>129</sup>
Primary Sedimentation

- 122. The major waste in this category is the fly ash. "A" is the ash content of coal, weight %
- 123. Polychlorinated biphenyls
- 124. Typical composition given in Table 9.2.2-1
- 125. Lowest income areas in South East Asia
- 126. Typical cities in Asia, North Africa, and South America
- 127. Typical Cities in Industrialized Countries
- 128. Typical cities in wealthy regions of the USA and Gulf
- 129. The main waste problem from this category is the sludge generated from the wastewater treatment operation. The presence of heavy metals in the sludge varies widely and depends on the type of industries that discharge into the sewerage system and on the pretreatment of their effluents. It can be generally assumed that a fair fraction of the heavy metals in the incoming wastewater find their way into the generated sludge.

Model for Solid & Hazardous Waste Inventories - Cont'd

, ,		INIT-	In	organic	Qily	Org	ganic	Putres- cible	Low Hazard	Infec- tious
		UNIT	*	Kg/U	 Kg/U	*	Kg/U	Kg/U	Kg/U	Kg/U
	Undigested Sludge	person*year						11		
		(person*year)						(220)		
	Digested in separate	e tanksperson*ye	ar					5.8		
		(person*year)						(100)		
	Digested on sand bed							5.8		
		(person*year)						(37)		
	Primary Sedimentation a	nd Activated Slu	idge	Treatme	nt					
	Undigested	person*year						20.4		
		(person*year)						(510)		
	Digested in separate	•	ar					12.0		
		(person*year)						(146)		
	Digested on sand bed							12.0		
		(person*year)						(37)		
	Activated Sludge Treatm									
	Wet Sludge	person*year						16.8		
		(person*year)						(1423)		
	Trickling Filtration	person*year						4.4		
		(person*year)						(73)		
	Chemical Precipitation									
	Wet sludge	person*year						28.8		
		(person*year)						(402)	•	
	Dewatered on sand be							28.8		
	5+:- <del>7</del> !- d:+d	(person*year)						(110) 7:3		
	Septic Tank, digested	person*year						(73)		
	Tobaff took disposted	(person*year)								
	Imhoff tank, digested	person*year						6.2 (37)		
		(person*year)						(37)		
	Potable Water Treatment	1000m <sup>3</sup> water							200130	
	rocable water freatment	(1000m <sup>3</sup> water)							(2000)	
		(1000m water)							(2000)	
930	Social and Related Communi	ty Services								
933	Medical, Dental and Other	Health Services								
	University Hospitals	(bed*year)						1096		364
	General Hospitals	(bed*year)						706		243
	Obstetrical Clinics	(bed*year)						736		432
	Medical Centers	(bed*year)						1400		600
	Psychiatric Clinics	(bed*year)						375		63
	Homes for Aged	(bed*year)						232		33
									•	

<sup>\* =</sup> Subcategory for hazardous wastes (see Sections 5.1 and 5.2.1)
( ) = Waste load factor on a wet weight basis

<sup>130.</sup> Sediment / Dry basis

Table 5.2.2-1 Typical Properties of Municipal Wastes in Various Countries (page 1 of 2)

8	Brazil	Ecuador	Egypt	France	Germany
Waste Factor, kg/cap/d			0.5	1.2	
Putrescible %	47.8	65.5	60.0	15.6	45.5
Paper %	31.5	17.9	13.0	35.3	23.0
Metals %	5.9	1.4	3.0	4.8	4.0
Glass %	4.7	1.7	2.5	11.7	13.0
Textiles %	4.1	3.1	2.5	4.9	
Plastic and rubber %	3.9	2.7	1.5	6.9	7.0
lisc. combustible %		3.0			4.0
lisc. incombustible %		0.9			3.5
Inerts %	2.1	3.8	17.5		
later content, %				31	
Density, kg/m <sup>3</sup>		292			
_ow Calor Value,kcal/kg				2,000	
Ho	lland	India	Israel	Italy	Libya
waste Factor, kg/cap/d			0.5	0.9	
Putrescible %	53.0	75.2	52.0	45.0	54.1
aper %	23.0	1.5	21.0	20.0	12.1
letals %	2.5	0.1	3.0	6.0	6.8
Glass %	8.0	0.2	3.0	5.0	3.3
extiles %	0.0	3.1	4.0	3.0	1.9
Plastic and rubber %	6.5	0.9	12.0	4.0	2.1
lisc. combustible %	4.0	0.2	**.0	7.0	
lisc. incombustible %	3.0	6.9			
nerts %	• • • •	12.0			
later content, %		12,10	45.0	45.0	
Density, kg/m <sup>3</sup>		570	,0.0	10.0	
ow Calor Value, kcal/kg		2,2	1450	1300	
	Malta	Mexico	Nigeria	Paraguay	Peru
/aste Factor, kg/cap/d	0.7				
Putrescible %	38.0	56.4	76.0	60.8	34.3
Paper %	24.0	16.7	6.6	12.2	24.3
fetals %	8.0	5.8	2.5	2.3	3.4
ilass %	9.0	3.7	0.6	4.6	1.7
extiles %	11.0	6.0	1.4	2.5	1.7
Plastic and rubber %		5.8	4.0	4.4	2.9
lisc. combustible %					
lisc. incombustible %					
nert below 10 mm %		5.7	8.9	13.2	31.7
ater content, %	25.0	•		<del>_</del>	·
ensity, kg/m <sup>3</sup>					
ow Calor Value,kcal/kg	1560				

Table 5.2.2-1 Continued (page 2 of 2)

ſ					1
	Spain	Tunisia	Turkey	Syria	United Kingdom
Waste Factor, kg/cap/d		0.4	0.7-0.8	0.7	
Putrescible %	50.0	80.8	27-38	40.0	28.0
Paper %	15.0	9.6	8-12	26	37.0
Metals %	3.0	2.1	1-2	3	9.0
Glass %		1.1	1-2	3	9.0
Textiles %		2.9	0.5-0.7	4	3.0
Plastic and rubber %	5.0	1.2	2-5	4.5	3.0
Misc. combustible %	18.0	0.5			1.0
Misc. incombustible %	9.0	0.1			1.0
Inert below 10 mm %		1.8			9.0
Water content, %				54	
Density, kg/m <sup>3</sup>		321			150
Low Calor Value, kcal/kg				1500	

Ven	ezuela	Yemen Yu	goslavia
Waste Factor, kg/cap/d			1.25
Putrescible %	40.4	57.0	23.3
Paper %	34.9	15.5	26.5
Metals %	6.0	13.2	2.5
Glass %	6.6	2.6	7.3
Textiles %	2.0	6.8	3.8
Plastic and rubber %	7.8	2.9	10.9
Misc. combustible %			
Misc. incombustible %			v
Inert below 10 mm %	2.3	2.0	
Water content, %			31-47
Density, kg/m <sup>3</sup>			
Low Calor Value,kcal/kg			1910

Note: The density of municipal wastes from industrialized and developing countries ranges from 100 to 150 and from 300 to over 550  $\rm kg/m^3$  respectively.

Table 5.2.2-2 Typical Properties of Municipal Waste Components (Adapted from: H. Peavy, D. Rowe and G. Tchobanoglous, Environmental Engineering: McGraw-Hill)

'	Moist: %	urė	re Density kg/m <sup>3</sup>		Low Calorific kcal/kg	Inert Residue After Combustion %				
	Range	Тур′1	Range	Typ'l	Range	Typ'l	Range	Тур'1		
Food Wastes	50-80	70	120-480	290	835-1670	1110	2-8	5		
Paper	4-10	6	30-130	85	2,770-4,450	4,000	4-8	6		
Cardboard	4-8	5	30-80	50	3,330-4,170	3,900	3-6	5		
Plastics	1-4	2	30-130	65	6,665-8,900	7,790	6-20	10		
Textiles	6-15	10	30-100	65	3,610-4,440	4,170	2-4	2.5		
Rubber	1-4	2	90-200	130	4,990-6,665	5,550	8-20	10		
Leather	8-12	10	90-260	160	3,610-4,730	4,170	8-20	10		
Garden Trimmings	30-80	60	60-225	105	550-4,440	1,550	2-6	4.5		
Wood	15-40	20	120-320	240	4,170-4,730	4,440	0.6	1.5		
Misc. organics	10-60	25	90-360	240	2,630-6,210	4,300	2-8	6		
Glass	1-4	2	160-480	195	24-60	36	96-99	98		
Tin cans	2-4	3	45-160	90	60-287	167	96-99	98		
Nonferrous metals	2-4	2	60-240	160			90-99	96		
Ferrous metals	2-6	3	120-1,200	320	60-287	167	94-99	98		
Dirt, ashes, brick	6-12	8	320-960	480	550-2,780	1,670	60-80	70		
Municipal Wastes (USA)	15-40	20			2,220-3,060	2,510				
Uncompacted			90-180	130						
In Compactor Truck			180-450	300						
In Landfill										
Normal Compaction			350-550	475						
Good Compaction			600-750	600						

Typical Compaction Ratios of Solid Wastes (Volume as Discarded over Volume in Landfill) (Source: G. Tchobanoglous, H. Theissen and R. Eliassen, Solid Wastes Engineering Principles and Management Issues: McGraw-Hill) Table 5.2.2-3

	oorly acted	Normally Compacted	Well- Compacted
Food wastes	2.0	2.8	3.0
Paper	2.5	5.0	6.7
Cardboard	2.5	4.0	5.8
Plastics	5.0	6.7	10.0
Textiles	2.5	5.8	6.7
Rubber,leather,wood	2.5	3.3	3.3
Garden trimmings	2.0	4.0	5.0
Glass	1.1	1.7	2.5
Nonferrous metal	3.3	5.6	6.7
Ferrous metal	1.7	2.9	3.3
Ashes, masonry	1.0	1.2	1.3

# 5.2.3 Working Table for Assessing the Solid Waste Loads

Data and Calculation Sheet for Solid Wastes (#  $\_$  of  $\_$ )

		SOURCE INORGANIC		VIC	011	_Y	ORGANIC			PUTRESI	CIBLE	LOW HAZARD		
SOURCE	UNIT (U)		Factor kg/U		Load tn/y	Factor kg/U	Load tn/y	Factor kg/V		Load tn/y	Factor kg/U	Load tn/y	Factor kg/U	Load tn/y
		,			. :	_	-							
					- •					- 1				
					-	-	- 3			- <u>†</u>	-	-		
				-	-		-	.				-		
1	.	-		.			-			-		_		-
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#### 5.2.4 Example Application

### The Problem:

Our study area comprises a city of 15,000 inhabitants, in which a wastewater treatment plant and a leather tannery operate. Determine the data requirements, collect the necessary information and assess the solid waste loads.

### Solution of the Problem:

- From Appendix II we find that Leather Tanneries are classified under the Standard Industrial Classification (SIC) Code # 3231. The Municipal Refuse Collection and the Wastewater Treatment activities are classified under the (SIC) Code # 92. The use of Appendix II facilitates the location of a particular activity in the model in Section 5.2.2.
- 2. From Section 5.2.2, inspection of the Leather Tanning, Municipal Refuse Collection and Wastewater Treatment segments of the solid wastes model yields the following input data requirements:
  - For the Leather Tannery
    - Type of Tannery (i)

Complete chromium tanning, Complete vegetable tanning, Only tanning, Only finishing, or Re-tanning and finishing.

- (ii) Type & Quantity of hides processed
- (iii) Type of wastewater treatment

None, Primary, or Secondary.

- For the Municipal Refuse collection (b)
  - (i) Standard of living in the study area

Very low income area, Area in a developing country, Area in an industrialized country, or Very high income area.

(ii) Presence of any significant refuse recycling at the source activity, which may affect the generated loads.

- (c) For the wastewater treatment plant
  - (i) Population served
  - (ii) Type of treatment

Primary only, Primary & activated sludge, Activated sludge only, Trickling filtration, or Chemical precipitation.

- (iii) Sludge digestion and dewatering
- 3. Assume that from the field survey work the following data were obtained in relation to the above questionnaire:
  - (a) For the Leather Tannery
    - (i) Type of Tannery:

Complete chromium tanning

(ii) Type & Quantity of hides processed:

Cow hides, 45,000/yr

(iii) Existence of a wastewater treatment plant:

Yes

- (b) For the Municipal Refuse collection
  - (i) Standard of living in the study area:

Typical of developing country

(ii) Presence of any significant refuse recycling at the source activity, which may affect the generated loads:

None

- (c) For the wastewater treatment plant
  - (i) Population served:

15,000 (the entire population of the city)

(ii) Type of treatment:

Primary & activated sludge,

# (iii) Sludge digestion and dewatering

### Sand beds

4. The above plant survey data, along with the necessary information from the solid wastes load model of Section 5.2.2, can be inserted in the working Table provided in Section 5.2.3. The latter can be used for computing the annual solid waste loads generated within the study area.

Table 5.2.4-1 shows how data and information can be entered and how the solid waste loads can be computed. It should be noted that in this Working Table the load factors are expressed as kg/Unit, while the activity of each source is entered in 1000 Units/Year. As a result, multiplication of each load factor by the source activity yields the solid waste load expressed in tons/year. For example, the factor for putrescible solid wastes from the Municipal refuse collection is 250 kg/(person\*yr) and the source activity is 15 thousand persons\*yr. Their multiplication yields 15\*250=3750 tons of putrescible solid wastes generated annually.

Table 5.2.4-1 Example use of the working table of Section 5.2.3 Data and Calculation Sheet for Solid Wastes (#  $_1$  of  $_1$ )

i			SOURCE INORGANIC		OILY		ORGANIC			PUTRESCIBLE		LOW HAZARD		
SOURCE	UNIT (U)	ĺ	Factor kg/U		Load tn/y	Factor kg/U	Load tn/y	Factor kg/U			Factor kg/U		Factor kg/U	Loa tn,
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Effluent Treat.	1000	0.045	300	С	13.5		_				(550)	(25)	_	-
2 Sanitary & Similar						<u> </u>				.		-		-
Refuse collectin	pers*y	15			-	.			}	- #	250-	-3750	- -	
Wastewater Treat	·			-	. #			. {	-	.   	-	-		
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CHAPTER 6

# STUDY IMPLEMENTATION ASPECTS

- 6.1 Resource and Time Requirements for Environmental Management Studies
  - 6.1.1 Personnel and Support Requirements
  - 6.1.2 Time Requirements
- 6.2 Definition of the Study and Sub-study Areas
  - 6.2.1 Definition of the Study Area
  - 6.2.2 Definition of the Sub-study Areas
- 6.3 Data Acquisition
  - 6.3.1 Authority for Data Access
  - 6.3.2 General Description of Information
  - 6.3.3 List of Possible Data Sources
  - 6.3.4 Verification of Data Reliability
- 6.4 Presentation of a Pollution Management Report
- 6.5 Bibliography

# 6.1 Resource and Time Requirements for Environmental Management Studies

As every study area is unique in some respects, it is difficult to make detailed step-by-step planning in advance. Hence, the study team should have the flexibility to collect whatever data and information they feel are suitable for their study and plan visits to data sources and industry. It is also important that both regulatory agency officials and survey team members understand the environmental management procedure, including its managerial and administrative support requirements. The following sections briefly describe the resource and time requirements, which have to be considered when planning a management study.

### 6.1.1 Personnel and Support Requirements

The environmental management approach described in this book allows the identification of environmental problems, assessment of their intensity, analysis of alternative mitigation options and the outline of effective environmental policies. Despite the fact that the material is organized so as to present a step-by-step guidance on most aspects, the nature and importance of environmental management studies makes it worthwhile to select the best qualified engineers and scientists as study members.

Usually, the study team will have to deal with air, water and land pollution problems in the study area and for this reason it should comprise personnel with management experience in each of the above three media. A team leader, with adequate managerial experience, as well as a broader understanding of the environmental management issues involved, should be designated and assigned overall responsibility.

The study team, depending on the complexity of the situation and the range of experience of the available personnel, may consist as few as two or three persons, including the project manager who may also participate in the analysis of one or more media, but probably not more than ten persons so as not to loose its coherence and flexibility. A model team for a complex study area will probably comprise seven persons working in very close cooperation, two per media and the project manager.

In addition to the study team personnel, several outside experts are likely to be invited to provide substantial input. Their involvement however, will depend on the analysis requirements, as various needs arise, and will be limited to the solution of the particular problems that emerge. For example, meteorologists from the local weather station may be requested to provide meteorological data and have them processed in a form that facilitates their subsequent use, (see section 8.2.2.1). Hydrogeologists from the ministry of mining and minerals may have to be requested to provide input in the selection of suitable landfill sites.

The study team should be selected from local or national environmental health staff, since the purpose of the study, in addition to assessing the pollution and waste sources and related problems, and developing an

appropriate control strategy, is to strengthen national and local proficiency in environmental management methodology. Also, since environmental management programmes are an on-going activity, it is important that national staff should be involved from the start. Thus, outside experts could be engaged only to give on-the-job training to local study personnel, who will later have the responsibility to take whatever follow-up action is necessary.

Proper authorization for access to data and information and for securing the technical input from outside experts should be obtained from all relevant government departments and industries. Such authorization could be obtained on the basis of existing government policy of allowing data collection and inter-departmental cooperation for environmental management issues.

Development of a spirit of cooperation between the survey team and those providing the data (government offices, industries, business groups, trade unions, etc) should be encouraged. Such cooperation will facilitate data collection, improve the completeness and accuracy of the study, and lay the ground work for future development of pollution control activities at national level.

Finally, administrative support, including transport, office space, telephone, fax, personal computers with appropriate software packages, photocopier, typing or printing facilities and a secretary will be required.

#### 6.1.2 Time Requirements

Environmental management studies should normally take only a couple of months to complete in areas where the problems are uncomplicated, and not much more than six months in the most complex metropolitan areas. If the time allocated is too short, it may not be possible to obtain all the required data and to complete the problem analysis and strategy synthesis phases. The end product under these circumstances cannot provide reliable guidance for the follow-up feasibility and detailed design studies. If on the other hand the time spent is too long, the chances are that the study has crossed the preliminary design limits and entered into the detailed analysis of particular measures. The latter should be deferred until the entire strategy has been formulated and clear targets have been set.

# 6.2 Definition of the Study and Sub-Study Areas

## 6.2.1 Definition of the Study Area

For national or regional environmental management studies the first step is to determine the number, types, and sizes of the study areas. Often the definition of the study area is influenced by prevalent pollution or public health problems in the region or country. However, it is advisable to consider the existing legal, institutional, or economic systems in the country in selecting boundaries. Usually the country or region is already divided into several districts that have particular socio-economic features: e.g. urban, industrial, rural, agricultural, mining, etc. These serve as a good basis for the definition of the study areas.

The major concern, however, is the selection of the appropriate boundaries. Sometimes there may be many possible choices of boundaries, but usually they fall into one or more of the following categories:

- Physical boundaries, such as drainage basins (surface or sewered), ridge-lines, rivers, coastlines, escarpments, express-ways, rail-roads, canals, etc.
- Political/legal boundaries, such as country, state or provincial borders, city limits, public health districts, census districts, air quality control regions, flood control/drainage districts, etc.
- Economic boundaries, such as industrial zones, mining districts, economic development areas, water/sewerage/refuse collection districts, etc.

Each category has its merits. Natural features usually facilitate the evaluation of the impact of pollution on air or water quality; political or legal boundaries facilitate data collection because the desired information, as well as the knowledgeable support staff are generally available in the corresponding government office in or near the study area; and, economic boundaries facilitate the assessment of the environmental impact of future growth. Thus, the person responsible for rapid pollution inventory studies must consider each of these categories in relation to other factors, such as known pollution or public health problems and available staff, in making the final decision on the definition of the study areas. A metropolitan city area along with the adjacent zones is a typical example of a suitable study area.

The study team should have the flexibility to modify the boundaries of the study area during the course of the study if the collected data indicate that this will enhance the completeness of the inventory, facilitate the assessment of emission impacts, or help in the formulation of better pollution and waste control strategies.

Finally, all of the study areas in a country or region should be ranked in order of priority. Among other factors, the severity of the pollution problems and the existence of any previous inventory studies could serve as the basis for setting such priorities.

#### 6.2.2 Definition of the Sub-study Areas

During the initial stages the study team, using area maps and other information obtained from the planning department or from other sources, should form a general idea about the geography or the area, the current and projected land usage, the location of industries and population centres, the boundaries of existing and planned sewerage systems, the prevailing meteorological and hydrological conditions, the various liquid waste receivers, the solid waste collection and disposal system, as well as the major pollution and public health problems and the existing pollution control authorities and legislation.

On the basis of this general information, the study team may find it desirable to subdivide the study area into smaller zones. It is useful to decide at an early stage whether or not the study area is to be subdivided, since this will affect the collection and organization of data. Generally, the complexity of the survey work increases with the number of subdivisions since separate pollution source activity data are required for each subregion. Experience so far indicates that the added difficulties are usually not so great as to preclude subdivision, but that the decision to subdivide should only be made when there are definite reasons for doing so.

With regard to air pollution, it is normally desirable to make separate assessments of the emissions from all major point sources, as well as separate inventories for the area sources (space heating and traffic) of each major population centre, since inventory data in this form are required as inputs to the air quality models for the analysis of the air pollution situation and the formulation of control strategies (see Chapter 8).

With regard to liquid wastes, area subdivisions that allow separate assessments to be made of effluent discharges into different receiving water bodies are often desirable. Such subdivisions facilitate the evaluation of the impact of discharges on receiving water bodies and help in the formulation of water pollution control strategies (see Sections 9.1 and Section 9.2). Also, subdivisions may be made in order to determine the type and capacity of pollution control facilities for the waste volumes and pollution loads discharged into the existing, planned, or proposed sewerage system.

With regard to solid wastes, area subdivisions sometimes have to be made along economic boundaries on the basis of the existing organization of waste collection and disposal systems.

Although separate reasons are given above for subdividing the study areas with regard to water, air, or land pollution problems, in practice all the above reasons have to be considered simultaneously so as to have the study area separated into a meaningful number of sub-areas in line with the overall analysis requirements.

## 6.3 Data Acquisition

Most of the input data required for the study are normally available in various government departments. In fact, the study procedure was designed with a view to making maximum use of existing information. To facilitate the organization of the survey data, the U.N. classification of industries and services is used (see Section 2.2 and Appendix II). This system should also facilitate the acquisition of data from government and industry since these commonly utilize the same or similar systems.

### 6.3.1 Authority for Data Access

In the course of the survey work the study team will have to contact many government agencies, local authorities, industrial associations, other institutions, as well as individual industries.

Written authorization to obtain access to both published and unpublished data is desirable, as it will enable government officials to disclose information without fearing any possible consequences. Industrial concerns may also demand such government authorization before they will disclose process and production data, or even permit site visits. The authorization should include references to the appropriate statutes and regulations and be issued by the appropriate minister or an equivalent high-level governmental official.

However, authorization alone may not be enough, since the most important element in this type of work is the establishment of a spirit of true cooperation between the study team and the agencies and industries involved. In places where competition exists among various government agencies for authority over pollution control work, it may be desirable to assign the inventory task to a team not directly associated with any of them, or to involve all the competing agencies in order to ensure cooperation between them.

# 6.3.2 General Description of Information

Before starting data collection, it is advisable to look up and list the type of data that is required for each of the industries identified in the study area. This can be done through the air, water and solid waste inventory models provided in Sections 3.2, 4.2, and 5.2 and the formulation of relevant survey questionnaires as discussed in Sections 3.2.4, 4.2.4 and 5.2.4.

In most cases important information can be found in government publications, such as statistical year books, industrial activity reports, master plans, or environmental impact statements. Useful data can also be

obtained from publications of international organizations such as UNDP, UNEP, UNIDO, WHO, and from any studies being undertaken in the area by United Nations Regional Economic Commissions or other Regional Intergovernmental Organizations. Also, reports produced by local authorities or industrial associations, trade unions, social security agencies, etc., may contain valuable information.

A sizeable portion of the required information available from various government agencies is often unpublished. These data are usually kept in a raw form and are not classified. Therefore, some effort has to be made to have the useful information extracted, processed, and classified. Examples of unclassified data include annual questionnaires completed by industries for government production statistics or economic studies and individual census forms.

The major difficulties with unpublished information are determining which data are required. Often there is a danger of leaving out important information if the screening is not done carefully, and, on the other hand, the complexity and the resource requirements increase considerably if relatively unimportant data are retrieved and processed. Previous experience in data collation will certainly be most helpful here in minimizing work, while ensuring the accuracy of the final results. If the study team has only limited experience of data handling, it is advisable to put in additional work in order to reduce the danger of major omissions.

During the inventory process all data collected have to be organized, critically assessed, and, whenever possible, cross-checked. This procedure will help identify areas for which data are lacking so that more emphasis can be placed on them. Clearly, not all of the data required can be obtained from government departments. Therefore, additional information will have to be sought either through experienced government employees or through direct contact with industry. Again this process is time-consuming and a balance has to be struck between the need for particular data and the effort required in obtaining them. Experience again helps to reduce the volume of this work without sacrificing much accuracy. Typical examples of additional information that can be obtained though industry surveys include detailed information on the processes, the air and water pollution control systems employed, the stack dimensions, the liquid waste receivers and the solid waste in-house storage and recycling/processing facilities. Section 2.3 provides guidance on how best to balance the information obtained from government and the detailed one from source survey visits.

The sources of all the data collected should be fully documented. For easy access during the survey, it is also recommended that files be set up in a systematic manner. Such a system would also be valuable when and if, at a later date, further verification and upgrading is carried out.

### 6.3.3 List of Possible Data Sources

A major task of the study team is to locate all major government information sources and to extract the required data from them. In order to facilitate this task, a list summarizing the most important types of information required and likely places from which such information can be obtained is provided in Table 6.3.3-1. The list is by no means exhaustive since data sources will vary in different countries depending upon the structure of government services.

# 6.3.4 Verification of Data Reliability

Background information on population, industrial establishments, and commercial facilities is most often available through national agencies dealing with population censuses, manufacturing and commerce. The accuracy of these data may vary considerably and, where data are likely to be less reliable, efforts should be made to verify and cross-check them to the maximum extent possible with information from other sources.

Cross-checking the data with information from other sources is often possible and highly desirable, since it is the best way of measuring the accuracy of the results. If important data from various sources of information are in significant disagreement, investigation of their original derivation often provides a good basis for the formulation of the most reasonable assumptions and provides guidance as how to proceed with the data collection so as to fill the gap. In any event, the reliability of the data along with major data deficiencies and disagreements should be clearly indicated in the final report. This will allow an overall assessment to be made of the accuracy of the results and the validity of the conclusions derived.

As an example of data cross-checking consider the case where for the inventory of traffic emissions the study team collects data about the total gasoline consumption in the study area from the ministry of energy and data about the number of gasoline powered cars, their age distribution and mean annual milage from the ministry of transport. From the latter through the model in Section 3.3 the anticipated gasoline consumption can be estimated and this can be compared with the actual gasoline consumption data from the ministry of energy. Obviously, major discrepancies will have to be carefully investigated.

List of Data Often Required in Environmental Management Studies, and Likely Sources for them (page 1 of 2) Table 6.3.3-1

Type of Data	Possible Source
Population	Statistical year-books Census reports Master plan studies National planning or development agencies
Health, mortality and morbidity data	Ministry of public health Local health services
Meteorological data	Meteorological services Airport authorities Universities
Hydrological data	Hydrological services River authorities Municipalities Water company
Agricultural activity	Ministry of agriculture National planning or economic development agencies Local governments
Mining Activity	Ministry of mining and energy National planning or economic development agencies Local governments Internal revenue agencies
Industrial activity	Ministry of industry and commerce National planning or economic development agencies
	Local governments Electric energy ministry, authority or
company	Internal revenue agencies Industry associations Ministry of animal production Air and water pollution control
authorities	All and water portation control
Road traffic	Ministry of transport
Length of streets, roads and highways	Ministry of public works Ministry of transport Municipalities

Table 6.3.3-1 Continued (page 2 of 2)

Type of Data	Possible Source
Airport activity	Airport authorities Ministry of transport
Port activity data	Port authorities Ministry of transport
Fuel consumption	Ministry of energy Ministry of industry Internal revenue agencies Refineries or oil distribution companies
Fuel quality	Refineries or oil distribution companies Ministry of energy Air pollution control authorities
Water supply	Ministry of public works Ministry of health Water company Municipalities
Sewage collection and disposal	Ministry of public works Ministry of health Sewerage organizations Municipalities
Solid waste	Local authorities Ministry of environment Private refuse disposal companies Area planning and development companies
Water quality and effluent loads	Oceanographic institute Ministry of health River authorities Water pollution control authorities Ministry of fisheries Area planning agencies Local health departments Universities
Air quality and air emissions	Ministry of environment Ministry of health Air pollution control authorities Universities

#### 6.4 Presentation of a Pollution Management Report

The following is a recommended outline, with brief description of the key elements for a report of an environmental management study.

### Introduction

The introduction should include the reasons for undertaking the study, its major objectives, a brief review of the methodology followed, some guidance on how the report material is organized, and a short statement about the uses and the limitations of the study results.

### Conclusions and Recommendations

The results from the source inventory work, the analysis of the existing pollution situation and the synthesis of a rational strategy should be briefly described for air, water and solid wastes separately. The highest priority measures and their anticipated impact should be separated from the rest so as to define a highly effective short term action programme. Follow-up activities must be defined, and the government departments responsible should be mentioned.

### General background

A description of the study area including a map should be provided. The geographical limits of the study area, prominent geographical and hydrological features and key characteristics of the area meteorology should be defined. For the urban regions within the study area some basic information about the population, and population trends, numbers of motor vehicles in use, fuel and water usage, as well as a brief description of the existing sewage collection, treatment and disposal, the refuse collection and disposal, and the nature and dimensions of the industrial activity should be presented. For industrial zones information such as, the zone size and location, the type of industrial establishments, the fuel and water supplies, the effluent treatment and receivers, should be given.

### Air Pollution

For each major point source in the study area the computed air emission loads and the critical impact analysis results (maximum credible concentrations on the critical and selected sensitive receivers) should be listed, see Table 8.1.2.2.2-2. Appropriate mitigation options (e.g. stack height modifications, fuel quality improvements, or control requirements) should also be included.

For each important type of area source (traffic emissions from passenger cars, taxis, buses, trucks, etc, space heating emission, etc) the computed emission loads and the long-term air quality impact analysis results (centre-maximum and spatial-average concentrations) should be listed. The air quality monitoring data that

may exist should be summarized and the air quality model predictions should be calibrated. The highest pollution contributors, as they emerge from the above analysis, should be clearly identified. The formulated air pollution control strategy in relation to area sources and its anticipated impact in the air emission loads and on the air urban air quality should be presented. The proposed measures should be screened and those with the highest priority (highest cost effectiveness, simplest implementation) identified, so as to formulate a high-priority action programme. The impact of the latter on the emissions and on the air quality should be assessed.

The longer term prospects in terms of population and urban growth, increase in traffic, fuel consumption, industrial production etc. should be analysed and the likely air quality problems, if no corrective action is taken, should be assessed. Alternative strategies for the solutions to these longer term problems should be defined.

### Water Pollution

Population and population trend data should be displayed. Existing sewage disposal systems (e.g. use of septic tanks, septage collection, treatment and disposal, or sewage collection, treatment and disposal systems) should be described in sufficient detail. Relevant computed waste volumes and loads and their distribution among the various receivers should be given.

The computed effluent volumes and loads from industrial sources, grouped and sub-totalled separately according to effluent receivers, should be listed. Separate lists of industries with toxic effluents should be provided and industries should be classified according to their type, size and their toxic waste problem.

The characteristics of the water bodies receiving the industrial and the domestic wastes should be provided, the critical parameters that define the controlling impact on such receivers should be identified, and the water pollution problems, as computed through the use of water quality models, should be defined.

The formulated water pollution control strategy should be described and the expected improvement after its implementation, defined. The proposed measures should be screened and those with the priority (highest cost effectiveness, implementation) should be identified, so as to formulate a high-priority action programme. The impact of the latter on the effluent loads and on the water quality should be assessed.

The longer term prospects in terms of population and urban growth, increases in water consumption and in the industrial production etc, should be analysed and the likely water quality problems, if no corrective action is taken, should be assessed. Alternative strategies for the solutions to these longer term problems should be defined.

#### Land Pollution

Current municipal waste management practices (recycling at the source, collection, transportation, processing and disposal) should be described and their effectiveness in terms of the level of service offered, cost, and protection of the environment should be defined. Formulated strategies in relation to the medium and longer term prospects should be described, and the associated capital investment requirements along with the economic and environmental merits should be defined. Intermediate, high priority, measures should be identified and their economic and operational impacts should be discussed. The implementation aspects, and especially the transition from the existing to the proposed system, should be adequately addressed.

The hazardous waste inventory results should be listed and the current management practices reviewed and assessed. The formulated relevant strategies in relation to the medium and longer term prospects should be described, and the associated economic and environmental merits should be defined. Intermediate, high priority measures, should be identified and their economic and operational impacts discussed.

Acknowledgements should be made where they are due, while detailed calculations and any additional information should be annexed.

Finally, the report should make frequent use of maps, photographs and graphic displays to support the text. In addition to tables, pie-, bar-, or line-charts should be used as they can provide a quick and clear understanding of relative load distributions and trends.

#### 6.5 Bibliography

- Economopoulos, A.P., (1989). Management and Control of the Environment, ed. H. W. de Koning. WHO/PEP/89.1. World Health Organization. Geneva.
- World Health Organization, (1982). Rapid Assessment of Air, Water and Land Pollution Sources, Publication No. 62. Geneva.

**APPENDIX** 

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# UN CLASSIFICATION OF INDUSTRIES AND SERVICES

#### APPENDIX OUTLINE

- II.1 Classification Table for Industries and Services
- II.2 Bibliography

#### II.1 Classification Table for Industries and Services

### 0 Activities not Adequately Defined

#### 1 Agriculture, Hunting, Forestry and Fishing

- 11 Agriculture and Hunting
  - 111 Agriculture and Livestock Production
  - 112 Agricultural Services
  - 113 Hunting, Trapping and Game Propagation
- 12 Forestry and Logging
  - 121 Forestry
  - 122 Logging
  - 130 Fishing

#### 2 Mining and Quarrying

- 21 Coal Mining
- 22 Crude Petroleum and Natural Gas Production
- 23 Metal Ore Mining
- 29 Other Mining

#### 3 Manufacturing

- 31 Manufacture of Food, Beverages and Tobacco
  - 311 Food Manufacturing
  - 313 Beverage Industries
  - 314 Tobacco Manufacturing
- 32 Textile, Wearing Apparel and Leather Industries
  - 321 Manufacture of Textiles
  - 322 Manufacture of Wearing Apparel, Except Footwear
  - 323 Manufacture of Leather and Products of Leather
  - 324 Manufacture of Footwear
- 33 Manufacture of Wood and Wood Products, Including Furniture
  - 331 Manufacture of Wood & Wood Products, Except Furniture
  - 332 Manufacture of Furniture and Fixtures
- 34 Manufacture of Paper and Paper Products, Printing & Publishing
  - 341 Manufacture of Paper and Paper Products
  - 342 Printing Publishing and Allied Industries
- 35 Manufacture of Chemicals, and Chemical, Petroleum, Coal, Rubber and Plastic Products
  - 351 Manufacture of Industrial Chemicals
  - 352 Manufacture of Other Chemical Products
  - 353 Petroleum Refineries
  - 354 Manufacture of Misc. Products of Petroleum and Coal

- 355 Manufacture of Rubber Products
- 356 Manufacture of Plastic Products not Elsewhere Classified
- Manufacture of Non-metallic Mineral Products, Except Products 36 of Petroleum and Coal
  - 361 Manufacture of Pottery, China and Earthenware
  - 362 Manufacture of Glass and Glass Products
  - 369 Manufacture of Other Non-Metallic Mineral Products
- Basic Metal Industries 37
  - 371 Iron and Steel Basic Industries
  - 372 Non-ferrous Metal Basic Industries
- Manufacture of Fabricated Metal Products, Machinery and Equip-38 ment
  - 381 Manufacture of Fabricated Metal Products, Except Machinery
  - 382 Manufacture of Machinery Except Electrical
  - 383 Manufacture of Electrical Machinery Apparatus & Appliances
  - 384 Manufacture of Transport Equipment
  - 385 Manufacture of ... Photographic and Optical Goods
- 39 Other Manufacturing Industries

#### Electricity Gas and Water

- 41 Electricity, Gas and Steam
- 42 Water Works and Supply
- Construction
- Wholesale and Retail Trade
  - Wholesale Trade 61
  - 62 Retail Trade
  - 63 Restaurants and Hotels
    - 631 Restaurants, Cafes, and other Eating & Drinking
    - 632 Hotels, Rooming Houses, Camps and Other Lodging

#### 7 Transport, Storage and Communication

- 71 Transport and Storage
  - 711 Land Transport
  - 712 Water Transport 713 Air Transport

  - 719 Services Allied to Transport
- 72 Communication
- Financing, Insurance, Real Estate and Business Services
- 9 Community, Social and Personal Services

- 91 Public Administration and Defence
- 92 Sanitary and Similar Services
- 93 Social and Related Community Services
  - 931 Educational Services
  - 932 Research and Scientific Institutes
  - 933 Medical, Dental, Other Health & Veterinary
  - 934 Welfare Institutions
- 94 Recreational and Cultural Services 941 Motion Pictures and Other Entertainment Services
- 95 Personal and Household Services
  - 951 Repair Services not Elsewhere Classified
  - 952 Laundries, Laundry Services and Cleaning
  - 953 Domestic Services
  - 959 Miscellaneous Personal Services

#### II.2 Bibliography

- 1. United Nations (1980). Year-book of Industrial Statistics. Department of Economic and Social Affairs, Statistical Office of the United Nations. New York.
- United Nations, (1989). Industrial Statistics Year-book. UN publication, Sales No. E/F.91.XVII.14.

APPENDIX III

# CONVERSION FACTORS AND SELECTED MATERIAL PROPERTIES

#### **APPENDIX OUTLINE**

- III.1 Conversion Factors
- III.2 Selected Material Properties

III.1 Conversion Factors

TO CONVERT	INTO	MULTIPLY BY
Gaseous Pollutant Concentrat	ions <sup>a</sup>	
O <sub>3</sub> , ppm volume NO <sub>2</sub> , ppm volume SO <sub>2</sub> , ppm volume H <sub>2</sub> S, ppm volume CO, ppm volume HC (as CH <sub>4</sub> ), ppm volume	O <sub>3</sub> , μg/m <sup>3</sup> NO <sub>2</sub> , μg/m <sup>3</sup> SO <sub>2</sub> , μg/m <sup>3</sup> H <sub>2</sub> S, μg/m <sup>3</sup> CO, μg/m <sup>3</sup> HC (as CH <sub>4</sub> ), μg/m <sup>3</sup>	1960. 1880. 2610. 1390. 1140. 654.
Fuel cons, mile/(US gal) Emission, gr/mile	Fuel cons, km/lt Emission, gr/km	0.426 0.6214
Length		
Millimeter (mm) Centimeter (cm) Meter (m) Kilometer (km) Inch (in) Foot (ft) Mile Yard (yd)	Inch (in) Inch (in) Foot (ft) Mile Millimeter (mm) Meter (m) Kilometer (km) Meter (m)	0.0394 0.3937 3.2808 0.6214 2.54 0.3048 1.6093 0.9144
Area		
Square centimeter (cm²) Square meter (m²) acre acre Hectare (ha) Hectare (ha) 1000 m² Square kilometer (km²) Square inch (in²) Square foot (ft²) Square mile Square yard (yd²)	Square inch (in²) Square foot (ft²) Square meter (m²) Hectare (ha) Square meter (m²) acre acre Square mile Square centimeter (cm²) Square meter (m²) Square meter (m²) Square kilometer (km²) Square meter (m²)	0.1550 10.7639 4046.8 0.405 10000. 2.471 0.2471 0.3861 6.4516 0.0929 2.5900 0.8361

TO CONVERT	INTO	MULTIPLY BY
Volume		
Liter Cubic centimeter (cm³) Cubic meter (m³) Cubic foot (ft³) Cubic foot (ft³) Bushel (bu) Bushel (bu) Barrel (US, dry) Cubic Yard (yd³)	Cubic foot (ft <sup>3</sup> ) Cubic inch (in <sup>3</sup> ) Cubic foot (ft <sup>3</sup> ) Liter (lt <sup>3</sup> ) Cubic meter (m <sup>3</sup> ) Liters (lt) Cubic foot (ft <sup>3</sup> ) Cubic inches (in <sup>3</sup> ) Cubic meter (m <sup>3</sup> )	0.03531 0.06102 35.31 28.317 0.0283 35.24 1.2445 7056. 0.7646
Liquid Capacity		
Liter (lt) Liter (lt) Liter (lt) Liter (lt) Quart (US) Gallon (US) (US gal) Quart (UK) Gallon (UK) (Imp. gal) Barrel Barrel Barrel Pint	Quart (US) Gallon (US) (US gal) Quart (UK) Gallon (UK) (Imp. gal) Liter (lt) Liter (lt) Liter (lt) Liter (lt) Liter (lt) Gallon (UK) (Imp. gal) Gallon (US) (US gal) Liter (lt)	1.0567 0.2642 0.8799 0.2200 0.9464 3.7854 1.1365 4.5461 158.984 34.9726 42.00 0.4732
Weight		
Gram (g or gr) Kilogram (kg) Metric ton (t or tn) Grain Once (oz) Once troy Pound (lb) Short ton (US)	Grain Pound (lb) Short ton (US) Gram (g or gr) Gram (g or gr) Gram (g or gr) Kilogram (kg) Kilogram (kg) Pounds (lb)	15.4323 2.2046 1.1023 0.0648 28.3495 31.1035 0.4536 907.2 2000.
Agricultural Products		
Corn, bu Corn, bu Milo, bu Milo, bu Oats, bu Oats, bu Barley, bu Barley, bu Wheat, bu	Corn, kg Corn, lb Milo, kg Milo, lb Oats, kg Oats, lb Barley, kg Barley, lb Wheat, kg	25.4 56. 25.4 56. 14.5 32. 21.8 48. 27.2

TO CONVERT	INTO	MULTIPLY BY
Agricultural Products (c	cont'd)	
Cotton, bale Cotton, bale	Cotton, kg Cotton, 1b	226. 500.
Miscellaneous Liquids		
Beer, bbl Paint, US gal Paint, US gal Varnish, US gal Varnish, US gal Whiskey, bbl Water, US gal Water, US gal	Beer, US gal Paint, kg Paint, 1b Varnish, kg Varnish, 1b Whiskey, 1t Whiskey, US gal Water, kg Water, 1b	31.5 4.5-6.8 10.0-15. 3.18 7.0 190. 50.2 3.81 8.3
Mineral Products		
Cement, bbl Cement, bbl Cement, yd <sup>3</sup> Cement, yd <sup>3</sup> Concrete, yd <sup>3</sup> Concrete, yd <sup>3</sup>	Cement, kg Cement, lb Cement, kg Cement, lb Concrete, kg Concrete, lb	170. 375. 1130. 2500. 1820. 4000.
1		1

 $<sup>^</sup>a\text{The conversion from ppm (volume) to }\mu g/m^3$  is based on the following Equation, which can be used for substances not listed in the table:

$$(C, \mu g/m^3) = (C, ppm volume)*40.87*(MW),$$

#### where:

C,  $\mu g/m^3$  = Concentration expressed in  $\mu g/m^3$  C, ppm = Concentration expressed in ppm volume = Molecular Weight (Use 16 for Hydrocarbons)

#### III.2 Selected Material Properties

Table III.2-1 Typical Densities of Selected Fuels, Woods and Mineral Products

	Density gr/lt
Liquid and Gaseous Fuels	
Asphalt	1030.
Butane (liquid at 15 <sup>0</sup> C)	. 579 <b>.</b>
Crude Oil	850-874.
Distillate Oil	845.
Gasoline	739.
Liquefied Natural Gas (LNG)	673.
Liquefied Petroleum Gas (LPG) <sup>a</sup>	521.
Natural Gas (at 15 <sup>0</sup> C)	0.78
Propane (liggid at 15 <sup>0</sup> C)	507.
Residual oil <sup>D</sup>	944.
Wood (Air dried)	
Elm	561.
Hem]ock	465.
Hickory	769.
Maple, sugar	689.
Maple, white	529.
Oak, red	673.
Oak, white	769.
Pine	641.
Mineral Products	
Cement	1483.
Concrete	2373.
Glass, common	2595.
Gravel, dry packed	1600-1920.
Gravel, wet	2020.
Gypsum, calcined	880-960.
Lime, pebble	850-1025.
Sand, Gravel (dry, loose)	1440-1680.

<sup>&</sup>lt;sup>a</sup>20% Butane, 80% Propane

 $<sup>^{\</sup>rm b}$  Typical densities for residual oil #4, #5, and #6 are 904, 933 and 966 g/lt respectively.

Table III.2-2 Typical Properties of Various Fuels

Type of Fuel	Heating Value kcal	Sulfur % by wt	Ash % by wt
Solid Fuels			
Bituminous coal Anthracite coal Lignite (@ 35% moisture) Wood (@ 40% moisture) Bagasse (@ 50% moisture) Bark (@ 50% moisture) Coke by-product	7,200/kg 6,810/kg 3,990/kg 2,880/kg 2,220/kg 2,492/kg 7,380/kg	0.6-5.4 0.5-1.0 0.5 neg1 neg1 0.5-1.0	4-20 7-16 6.2 1.0-3.0 1.0-2.0 1.0-3.0 0.5-5.0
Liquid Fuels			
Residual oil Distillate oil Diesel oil Gasoline Kerosene Liquid Petroleum Gas (LPG)	9,980/lt 9,300/lt 9,120/lt 8,620/lt 8,320/lt 6,250/lt	0.5-4.0 0.2-1.0 0.2-0.8 0.03-0.04 <sup>a</sup> 0.02-0.05 neg	0.05-0.1 negl negl negl negl
Gaseous Fuels			
Natural Gas Coke Oven Gas Blast Furnace Gas	9,341/Nm³ 5,249/Nm³ 890/Nm³	neg1 0.5-2.0 neg1	,

 $<sup>^{\</sup>text{a}}\textsc{Fuel}$  specifications often allow up to 0.1% and sometimes up to 0.15%

APPENDIX IV

LIST OF ABBREVIATIONS

APPENDIX OUTLINE

IV.1 List of Abbreviations

### IV.1 List of Abbreviations

AH Ampere-Hour

bbl Barrel

BOD Biochemical Oxygen Demand

BOD<sub>5</sub> 5-day Biochemical Oxygen Demand

BOD<sub>u</sub> Ultimate Biochemical Oxygen Demand

bu Bushel

COD Chemical Oxygen Demand

Conc Concentration

d day

ESP Electrostatic Precipitator

FF Fabric Filter (Baghouse)

g or gr Gram

gal US gallon

h or hr Hour

HC Hydrocarbons

l or lt Liter

km Kilometer

LDGP Light Duty Gasoline Powered

LWK Live Weight of animals Killed

m Meter

mg Milligram (10<sup>-3</sup> grams)

MWH Megawatt-Hour

Negl Negligible

ng Nanogram (10<sup>-9</sup> grams)

NM VOC Non-methane Volatile Organic Compounds

NTIS US National Technical Information Service

